Overview

The following describes compiled benchmark challenge measurement results which are used to judge submissions to the 2022 AM-Bench modeling challenges. The results presented here are summarized and formatted similar to how modelers were asked to submit their modeling results by July 15, 2022. Additional context, description, or measurement results may also be provided where necessary. Additional information may become available later so updated versions of these documents may be posted. Please check back occasionally.

Please note that the measurement results presented here are focused on the challenge problems and reflect only part of the validation measurement data which will be provided by AM Bench for each set of benchmarks.

AMB2022-03: Single laser tracks using different processing conditions and 2D arrays of laser tracks (Pads) on solid plates of IN718. Detailed descriptions of the experiment design, measurement methods, and data analysis are given here.

Challenges

- Track Solid Cooling Rate (CHAL-AMB2022-03-TSCR): Cooling rate immediately following complete solidification (below solidus) at the center of each track for all processing conditions.
- Track Liquid Cooling Rate (CHAL-AMB2022-03-TLCR): Liquid cooling rate immediately before start of solidification (above liquidus) at the center of each track for all processing conditions.
- Track Time Above Melt (CHAL-AMB2022-03-TTAM): Time above the midpoint between solidus and liquidus temperature (assumed to be 1 298 °C) for single laser-scanned tracks.
- Track Melt Pool Geometry (CHAL-AMB2022-03-TMPG): The laser track width and depth near the center of each track for all processing conditions.
- Pad Time Above Melting (CHAL-AMB2022-03-PTAM): Time above the midpoint between solidus and liquidus temperature (assumed to be 1 298 °C) for specified locations of the X-Pads and Y-Pads.
- Pad Solid Cooling Rate (CHAL-AMB2022-03-PSCR): Cooling rate immediately following complete solidification (below solidus) at the center of each track for all processing conditions.
- Pad Melt Pool Geometry (CHAL-AMB2022-03-PMPG): Laser track depth and geometrical measurements describing the overlapping laser tracks near the center and near the edge of both X-Pads and Y-Pads.

1. Description of Benchmark Challenge Problems

1.1 Single Laser Track Benchmarks

Seven combinations of spot size, scan speed, and laser power were tested with three repeats of each melt track. The process parameters for the thermography tests are summarized in Table 1.
Table 1: Summary of single-track thermography process parameter cases for quick reference

<table>
<thead>
<tr>
<th>Case Number</th>
<th>Laser Power [W]</th>
<th>Scan Speed [mm/s]</th>
<th>Spot size, D4σ [μm]</th>
</tr>
</thead>
<tbody>
<tr>
<td>Baseline</td>
<td>0</td>
<td>285</td>
<td>960</td>
</tr>
<tr>
<td>Change spot</td>
<td>1.1</td>
<td>285</td>
<td>960</td>
</tr>
<tr>
<td></td>
<td>1.2</td>
<td>285</td>
<td>960</td>
</tr>
<tr>
<td>Change Speed</td>
<td>2.1</td>
<td>285</td>
<td>1200</td>
</tr>
<tr>
<td></td>
<td>2.2</td>
<td>285</td>
<td>800</td>
</tr>
<tr>
<td>Change Power</td>
<td>3.1</td>
<td>325</td>
<td>960</td>
</tr>
<tr>
<td></td>
<td>3.2</td>
<td>245</td>
<td>960</td>
</tr>
</tbody>
</table>

The time above melt (TAM) and cooling rate (CR) values are determined based on 30 adjacent pixels at the track centerline at a nominally steady-state location along the track length. In order to determine the TAM and CRs, the apparent temperature at the solidification inflection is determined. It is assumed that no undercooling occurs, and the emissivity is used to convert the apparent temperature to ‘true’ temperature based on the midpoint of the solidus and liquidus table data for IN718. The apparent solidification temperature and corresponding emissivity values for each case (with three repeats) are shown in Figure 1.

As discussed in the measurements and challenge description documentation, the measurable TAM and CRs are based on the apparent temperature distribution, which includes any and all measurement error induced by the laser-matter interaction and byproducts thereof. It can be observed that, with decreasing volumetric energy density (VED) of each parameter, the apparent solidification temperature and emissivity increase. Although a change in undercooling may occur with differing cooling rates, it is also evident from the image data that the size, intensity, and position of the radiating process byproducts changes with VED, which also affects the measured temperature and associated TAM and CRs. It can be observed that the change in spot size had the most significant effect on the apparent solidification temperature.
Figure 1: Single track apparent solidification temperature and emissivity with three repeats of seven process parameter combinations.

The reported TAM and CRs are based on the average of three individual tracks, and the results are shown graphically in Figure 2. Increasing scan speed and decreasing power (both decreasing VED) causes the CRs to increase and the TAM to decrease approximately linearly. Increasing spot size shows a nonlinear decrease in TAM and a decreasing trend in SCR, which is converse of the other process parameters with respect to decreasing VED. These results combined with the substantial increase in apparent solidification temperature at the largest spot size suggest that the measurement error in TAM and SCR may be greatest at the largest spot size. The results should be interpreted accordingly.

Figure 2: Graphical summary of the measured TAM and CRs as a function of each process parameter. VED decreases from left to right in each graph, and so the power axis is decreases from left to right.

The results are tabulated in the following sections.
1.1.1 CHAL-AMB2022-03-TTAM, -TSCR, and -TLCR

Table 2 provides the summary results for the track time above melting (TTAM), track solid cooling rate (TSCR), and track liquid cooling rate (TLCR) results for the CHAL-AMB2022-03 set of modeling challenges:

<table>
<thead>
<tr>
<th>Case Number</th>
<th>Track Time Above Melting (TTAM) [s]</th>
<th>Track Solid Cooling Rate (TSCR) [°C/s]</th>
<th>Track Liquid Cooling Rate (TLCR) [°C/s]</th>
</tr>
</thead>
<tbody>
<tr>
<td>0</td>
<td>1.22E-03</td>
<td>6.99E+05</td>
<td>4.14E+05</td>
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<tr>
<td>1.1</td>
<td>1.30E-03</td>
<td>7.32E+05</td>
<td>4.06E+05</td>
</tr>
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<td>1.2</td>
<td>1.04E-03</td>
<td>5.11E+05</td>
<td>3.65E+05</td>
</tr>
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<td>2.1</td>
<td>8.96E-04</td>
<td>7.85E+05</td>
<td>5.06E+05</td>
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<td>3.1</td>
<td>1.38E-03</td>
<td>7.05E+05</td>
<td>3.81E+05</td>
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<tr>
<td>3.2</td>
<td>1.03E-03</td>
<td>7.49E+05</td>
<td>4.33E+05</td>
</tr>
</tbody>
</table>

1.1.2 Supplementary Data

The following measurements were also obtained during the AMB2022-03 set of tests, and described in the AMB2022-03 modeling challenge description. These were not part of the 2022 modeling challenge competition, but are provided here for future reference:

1.1.2.1 Track Transition Cooling Rate (TTCR)

<table>
<thead>
<tr>
<th>Case Number</th>
<th>Track Transition Cooling Rate (TTCR) [°C/s]</th>
</tr>
</thead>
<tbody>
<tr>
<td>0</td>
<td>1.93E+05</td>
</tr>
<tr>
<td>1.1</td>
<td>1.38E+05</td>
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<td>1.2</td>
<td>1.93E+05</td>
</tr>
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<td>2.1</td>
<td>3.01E+05</td>
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<td>2.2</td>
<td>1.46E+05</td>
</tr>
<tr>
<td>3.1</td>
<td>1.57E+05</td>
</tr>
<tr>
<td>3.2</td>
<td>2.32E+05</td>
</tr>
</tbody>
</table>
1.1.3 CHAL-AMB2022-03-TMPG

Dark field micrographs for single tracks are shown in Figure 3 for the track melt pool geometry (TMPG) challenge. The challenge measurements for melt pool depth and width are provided in Table 4. Trends with laser diameter, velocity, and power are plotted in Figure 4.

![Figure 3. Representative cross-sectional dark field optical micrographs of single tracks. Image labels include the part number-line condition-line number (e.g., P3-L1.2-1).](image)

<table>
<thead>
<tr>
<th>Sample ID and Case Number</th>
<th>Mean $d_t$ (µm)</th>
<th>Std. dev. $d_t$ (µm)</th>
<th>Mean $w_t$ (µm)</th>
<th>Std. dev. $w_t$ (µm)</th>
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</thead>
<tbody>
<tr>
<td>AMB2022-718-SH1-BP1-L0</td>
<td>139.7</td>
<td>1.9</td>
<td>136.3</td>
<td>2.9</td>
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<td>AMB2022-718-SH1-BP1-L1.1</td>
<td>227.2</td>
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<td>106.2</td>
<td>3.6</td>
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<tr>
<td>AMB2022-718-SH1-BP1-L1.2</td>
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<td>1.1</td>
<td>141.7</td>
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<td>AMB2022-718-SH1-BP1-L2.1</td>
<td>109.7</td>
<td>1.7</td>
<td>112.9</td>
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<tr>
<td>AMB2022-718-SH1-BP1-L2.2</td>
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<td>2.6</td>
<td>156.1</td>
<td>4.9</td>
</tr>
<tr>
<td>AMB2022-718-SH1-BP1-L3.1</td>
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<td>2.0</td>
<td>134.3</td>
<td>2.5</td>
</tr>
<tr>
<td>AMB2022-718-SH1-BP1-L3.2</td>
<td>116.9</td>
<td>1.2</td>
<td>129.4</td>
<td>1.6</td>
</tr>
</tbody>
</table>
Figure 4. Melt pool size (depth and width) trends with (a) laser spot diameter, (b) laser velocity, and (c) laser power for single track laser scans on BP1. Data are the mean ± 95% confidence interval (n = 6).

1.2 Laser Pad Benchmarks
1.2.1 CHAL-AMB2022-03-PTAM

The algorithm for analyzing the pad high speed thermal imaging is based on that described in the AMB2022-01 challenges for the 3D builds, as was mentioned in the AMB2022-03 challenge description.

Pre-processing was conducted in a slightly different order than the algorithm described in the AMB2022-03 challenge description for TAM and SCR. Here, spatter removal processing was first conducted on the
raw thermal video signal prior to conversion to temperature. However, this is inconsequential to the resulting PTAM and PSCR values.

The following algorithmic steps were taken to arrive at PTAM and PSCR results described in this document:

   a. Frame-by-frame spatter removal using threshold mask at 100 digital levels (approximately equivalent to $T = 1077$ °C at $\varepsilon = 0.5$).
   b. Masking of part boundaries using threshold of 760 digital levels (approximately equivalent to $T = 1260$ °C at $\varepsilon = 0.5$).
2. Convert the spatter-removed thermal images to temperature using the camera calibration and estimated emissivity of $\varepsilon = 0.5$.
3. Proceed with calculation of TAM and SCR for each pixel as described in the AMB2022-03 challenge description using transition temperature of $T_{\text{trans}} = 1298$ °C.

Further details on the exact algorithms will be clarified in a future publication. It should be noted that the selection of spatter-removal threshold parameters as well as the assumed emissivity affect the measured PTAM and PSCR results.

The choice in spatter-removal algorithm parameters, and emissivity value where chosen which provided similar results to the track time above melt (TTAM) along the centerline of the individual tracks.

1.2.1.1 PTAM Results

Figure 5 shows the PTAM results derived from the high-speed thermal imaging for the X-pads and Y-pads, including histograms of each pixel’s PTAM value. It should be noted that histograms showed dual peaks, and non-normal distributions. The left peaks constitute lower PTAM pixel values which largely stem from residual spatter, plume, or other spurious features which depend highly on the spatter-removal preprocessing. While these features are present in the thermographic measurement, it is recognized they may not be present in computational simulation.
X pad 1 and X pad 2 were measured separately resulting in separate thermographic videos, as were Y pad 1 and Y pad 2. The CHAL-AMB2022-03-PTAM modelling challenge requested summary statistics for each X pad and Y pad pairs combined. Table 5 provides statistical results for each separate pad, and X pad and Y pad pairs combined. Additional metrics, including mode, skew, and kurtosis results are provided for reference.

Table 5: PTAM statistical results. Results that were requested for the CHAL-AMB2022-03-PTAM challenge are in bold.

<table>
<thead>
<tr>
<th></th>
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<th></th>
<th></th>
<th></th>
<th></th>
</tr>
</thead>
<tbody>
<tr>
<td>X Pad 1</td>
<td>87020</td>
<td>4.83E-04</td>
<td>1.15E-04</td>
<td>1.01E-05</td>
<td>5.61E-04</td>
<td>0.72</td>
<td>1.72</td>
</tr>
<tr>
<td>X Pad 2</td>
<td>81042</td>
<td>5.06E-04</td>
<td>1.31E-04</td>
<td>1.01E-05</td>
<td>5.64E-04</td>
<td>0.61</td>
<td>1.56</td>
</tr>
<tr>
<td>X Pads combined</td>
<td><strong>168062</strong></td>
<td><strong>4.94E-04</strong></td>
<td><strong>1.22E-04</strong></td>
<td><strong>1.01E-05</strong></td>
<td><strong>5.63E-04</strong></td>
<td><strong>0.66</strong></td>
<td><strong>1.64</strong></td>
</tr>
<tr>
<td>Y Pad 1</td>
<td>39230</td>
<td>1.04E-03</td>
<td>1.24E-03</td>
<td>1.17E-03</td>
<td>5.02E-04</td>
<td>-0.80</td>
<td>2.27</td>
</tr>
<tr>
<td>Y Pad 2</td>
<td>39174</td>
<td>1.04E-03</td>
<td>1.24E-03</td>
<td>1.36E-03</td>
<td>5.04E-04</td>
<td>-0.82</td>
<td>2.27</td>
</tr>
<tr>
<td>Y Pads combined</td>
<td><strong>78404</strong></td>
<td><strong>1.04E-03</strong></td>
<td><strong>1.24E-03</strong></td>
<td><strong>1.30E-03</strong></td>
<td><strong>5.03E-04</strong></td>
<td><strong>-0.81</strong></td>
<td><strong>2.27</strong></td>
</tr>
</tbody>
</table>

1.2.1.2 PTAM Results, thresholded to > 0.5 ms.

Since spatter-removal parameters affect the prevalence of lower measured PTAM values, the left-most peaks in the histograms in Figure 5 were removed by removing PTAM values < 0.5 ms. Figure 6 gives examples of the resultant PTAM value histograms with values < 0.5 ms removed for X pad 1 and Y pad 2, and Table 6 gives summary statistics for the resultant distributions.
Figure 6: Example histograms of PTAM results which exclude values below 0.5 ms.

Table 6: PTAM statistical results for values above 0.5 ms. Results that were requested for the CHAL-AMB2022-03-PTAM challenge are in bold.

<table>
<thead>
<tr>
<th></th>
<th></th>
<th></th>
<th></th>
<th></th>
<th></th>
<th></th>
<th></th>
</tr>
</thead>
<tbody>
<tr>
<td>X Pad 1</td>
<td>31008</td>
<td>1.21E-03</td>
<td>1.25E-03</td>
<td>1.16E-03</td>
<td>2.27E-04</td>
<td>-0.80</td>
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<tr>
<td>X Pad 2</td>
<td>30985</td>
<td>1.20E-03</td>
<td>1.24E-03</td>
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<td>2.21E-04</td>
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<td>3.34</td>
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<tr>
<td>X Pads combined</td>
<td>61993</td>
<td><strong>1.20E-03</strong></td>
<td><strong>1.24E-03</strong></td>
<td><strong>1.22E-03</strong></td>
<td><strong>2.24E-04</strong></td>
<td>-0.81</td>
<td>3.32</td>
</tr>
<tr>
<td>Y Pad 1</td>
<td>30552</td>
<td>1.28E-03</td>
<td>1.31E-03</td>
<td>1.17E-03</td>
<td>2.46E-04</td>
<td>-0.61</td>
<td>3.73</td>
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<tr>
<td>Y Pad 2</td>
<td>30525</td>
<td>1.28E-03</td>
<td>1.32E-03</td>
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<td>2.45E-04</td>
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<tr>
<td>Y Pads combined</td>
<td><strong>61077</strong></td>
<td><strong>1.28E-03</strong></td>
<td><strong>1.31E-03</strong></td>
<td><strong>1.30E-03</strong></td>
<td><strong>2.46E-04</strong></td>
<td>-0.64</td>
<td>3.72</td>
</tr>
</tbody>
</table>

1.2.1.3 Note on modeling challenge evaluation

Measurement results were shown to depend on various parameters required for processing the thermal images. Additionally, residual features stemming from spatter or plume are not expected to be representative of the surface thermal history, and may skew summary statistics presented. Other thermal image processing parameters may provide improved relation to real surface thermal history, and more complex or locally variant quantitative metrics for comparing measurement and simulation results may be more appropriate. These issues will be considered when evaluating model challenge submission results.

1.2.2 CHAL-AMB2022-03-PSCR

The algorithm for analyzing the pad high speed thermal imaging is based on that described in the AMB2022-01 challenges for the 3D builds, as was mentioned in the AMB2022-03 challenge description. Similar thermal image pre-processing steps described above for pad time-above-melt challenge (CHAL-AMB2022-03-PTAM) were also used to evaluate pad solid cooling rate (PSCR). Figure 7 shows the PSCR results derived from the high-speed thermal imaging for the X-pads and Y-pads, including histograms of each pixel’s PSCR value. Similar to PTAM results, it should be noted that the selection of spatter-removal threshold parameters as well as the assumed emissivity affect the measured PTAM and PSCR results.
Figure 7: Pad solid cooling rate (PSCR) results for X pads and Y pads. Note that colorbar limits are selected for optimal image contrast, and values above $1 \times 10^6 \text{ °C/s}$ are removed from the histograms.

PSCR results were non-normally distributed and included a small number of spuriously high cooling rate values which skewed mean values. Values above $1 \times 10^6 \text{ °C/s}$ were removed prior to calculating statistical metrics in Table 7. Table 7 provides statistical results for each separate pad, and X pad and Y pad pairs combined. Additional metrics, including mode, skew, and kurtosis results are provided for reference.

<table>
<thead>
<tr>
<th>Pad Type</th>
<th>N [pixels]</th>
<th>Mean [°C/s]</th>
<th>Median [°C/s]</th>
<th>Mode [°C/s]</th>
<th>Std. Dev. [°C/s]</th>
<th>Skew [-]</th>
<th>Kurtosis [-]</th>
</tr>
</thead>
<tbody>
<tr>
<td>X Pad 1</td>
<td>47572</td>
<td>3.26E+05</td>
<td>2.65E+05</td>
<td>1.65E+05</td>
<td>1.73E+05</td>
<td>1.81</td>
<td>5.92</td>
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<tr>
<td>X Pad 2</td>
<td>45397</td>
<td>3.21E+05</td>
<td>2.61E+05</td>
<td>1.61E+05</td>
<td>1.70E+05</td>
<td>1.88</td>
<td>6.25</td>
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<tr>
<td>X Pads, combined</td>
<td>92969</td>
<td>3.24E+05</td>
<td>2.63E+05</td>
<td>1.61E+05</td>
<td>1.72E+05</td>
<td>1.84</td>
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<td>37269</td>
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<td>5.79</td>
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<td>37146</td>
<td>2.87E+05</td>
<td>2.35E+05</td>
<td>1.37E+05</td>
<td>1.56E+05</td>
<td>1.77</td>
<td>6.28</td>
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<td>Y Pads, combined</td>
<td>74415</td>
<td>2.91E+05</td>
<td>2.35E+05</td>
<td>1.35E+05</td>
<td>1.62E+05</td>
<td>1.74</td>
<td>6.04</td>
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</table>

1.2.2.1 Note on modeling challenge evaluation

Measurement results were shown to depend on various parameters required for processing the thermal images. Additionally, residual features stemming from spatter or plume are not expected to be representative of the surface thermal history, and may skew summary statistics presented. Other thermal image processing parameters may provide improved relation to real surface thermal history, and more complex or locally variant quantitative metrics for comparing measurement and simulation results may be more appropriate. These issues will be considered when evaluating model challenge submission results.
1.2.3 CHAL-AMB2022-03-PMPG

Pad scan results were analyzed in terms of track number and cross-section position within the pad. The X-pad (BP2) contained 47 tracks and two cross-section positions. The Y-pad (BP3) contained 23 tracks and four cross-section positions. Odd and Even refer to odd and even track numbers. Representative micrographs for the two pad types are shown in Figure 8. The challenge results for depths and widths are provided in Table 8. Melt pool depths and widths versus track number are plotted for each pad type at one cross-section position in Figure 9. Qualitatively, the first three tracks in each pad had smaller depths. These were included in the Odd and Even averages. The Y-pad had a significant difference in melt pool height for Odd and Even track numbers. We note that the Y-pad, Even track numbers correspond to a parallel laser scan direction and gas flow, whereas, the Y-pad, Odd track numbers correspond to an antiparallel configuration. The X-pad scan direction and gas flow direction are perpendicular for Odd and Even track numbers. The Even and Odd melt pool depth and width trends with cross-section position are plotted in Figure 10. A position of 0 mm corresponds to the starting side of the pad.

Figure 8. Representative cross-sectional dark field optical micrographs of pad scans: (a) X-pad, BP2-P2 and (b) Y-pad, BP3-P3. Track numbers are listed for the final five tracks in each pad/image. The terms Odd and Even correspond to odd and even track numbers.
Table 8. CHAL-AMB2022-03-PMPG Results: pad depth ($d_p$), pad width ($w_p$), overlap depth ($d_o$), and overlap width ($w_o$).

<table>
<thead>
<tr>
<th>Sample ID and Track Group</th>
<th>Mean $d_p$ (µm)</th>
<th>Std. dev. $d_p$ (µm)</th>
<th>Mean $d_o$ (µm)</th>
<th>Std. dev. $d_o$ (µm)</th>
<th>Mean $w_p$ (µm)</th>
<th>Std. dev. $w_p$ (µm)</th>
<th>Mean $w_o$ (µm)</th>
<th>Std. dev. $w_o$ (µm)</th>
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<tbody>
<tr>
<td>AMB-2022-718-SH1-BP2-P2-Odd</td>
<td>163.5</td>
<td>6.1</td>
<td>76.0</td>
<td>17.6</td>
<td>100.0</td>
<td>5.0</td>
<td>122.0</td>
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<td>155.8</td>
<td>4.7</td>
<td>91.8</td>
<td>7.8</td>
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<td>AMB-2022-718-SH1-BP2-P4-Odd</td>
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<td>7.0</td>
<td>79.2</td>
<td>18.3</td>
<td>95.1</td>
<td>6.6</td>
<td>113.3</td>
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Figure 9. Melt pool depths and widths versus track number for pad scans: (a-b) Y-Pad, BP3-P3 and (c-d) X-pad, BP2-P2. Each data point is a single measurement.
Figure 10. Melt pool depth and width trends for pad scan Even and Odd tracks versus position within the pad: (a, c) X-Pad, BP2 and (b,d) Y-Pad, BP3. Data are the mean ± 95% confidence interval. \( n = 23 \) and 24 for BP2 Even and Odd, respectively. \( n = 11 \) and 12 for BP3 Even and Odd, respectively.

2. Description and Links to Associated Data

Measurement results data associated with the AMB2022-03 challenges are provide in separate NIST Public Data Repository (PDR) datasets, accessible via the following DOI links to the PDR landing pages:

- AM Bench 2022 Measurement Results Data: In-situ Thermography and Scan Strategy for Laser-scanned Single Tracks and Pads on Bare In718 (AMB2022-03) – [https://doi.org/10.18434/mds2-2716](https://doi.org/10.18434/mds2-2716)
- AM Bench 2022 Measurement Results Data: Optical and Scanning Electron Microscopy of Laser-scanned Single Tracks and Pads (AMB2022-03) - [https://doi.org/10.18434/mds2-2718](https://doi.org/10.18434/mds2-2718)

New data files, updates, and/or changes to download URLs may be made periodically. Users should refer to the README text file in each dataset page which will record all updates. Additionally, the NIST Public Data Repository (PDR) undergoes frequent updates. If file downloads fail or are unavailable, users should wait several hours before contacting the technical support listed on the PDR dataset webpage.
References

Citations are provided throughout this document as hyperlinked URLs to the associated digital object identifier (DOI). Clicking these hyperlinked text should open the associated publication or cited source.

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Certain commercial equipment, instruments, or materials are identified in this paper in order to specify the experimental procedure adequately. Such identification is not intended to imply recommendation or endorsement by NIST, nor is it intended to imply that the materials or equipment identified are necessarily the best available for the purpose.