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May 20-23, 2018 Stamford, CT Assessing the Effect of Backcoatings and Fire Barrier Technologies on Upholstered Furniture Flammability

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> Recent Advances in Flame Retardancy of Polymeric Materials BCC Meeting on Flame Retardancy

#### Disclaimer

Some of the data in this presentation hasn't been through NIST review process and should be considered experimental / draft results. However, the data has been analyzed by subject matter experts within the research team and is believed to be scientifically sound and consistent with the integrity expected of NIST research



# Outline

- Residential-Upholstered-Furniture (RUF): moving away from Flame Retardants (FRs)
- Fire safe RUF without Flame Retardants
  NIST Silicone Backcoating
- Fire Barriers
- Testing (CUBE TEST)

composite cone-based-test for assessing Fire Barriers and Backcoatings



## **Residential Upholstered Furniture (RUF)**

#### RUF fires are the largest cause of civilian deaths in US home fires\*





How can we reduce RUF fire deaths?

- 1. Fire Prevention (ignition suppression)
- $\Rightarrow$  Reduce smoldering ignitions (most frequent ignition source 1<sup>st</sup> item)
- 2. Fire Mitigation (heat release rate reduction)

 $\Rightarrow$  >90 % of casualties from fires spreading beyond the initial burning object  $\Rightarrow$  >70 % from fires spreading outside the initial fire room\*\*

\*J.R. Hall Jr, Estimating Fires When a Product is the Primary Fuel But Not the First Fuel, With an Application to Uphol.Furn., NFPA, 2014. \*\*Ahrens, Home Fires that Began with Upholstered Furniture, NFPA, 2017



#### NFPA 277: Sudden Death of a Draft Standard Flaming test for RUF

- 2014: started development of NFPA 277
- April 2018: NFPA Standard Council voted to cease NFPA 277
- NFPA stated that [1]:

- The <u>concerns about the toxicity of flame</u> <u>retardant chemicals</u> raised by participants, including first responders, need to be answered.

[1] https://www.nfpa.org/News-and-Research/News-and-media/Press-Room/News-releases/2018/NFPA-Standards-Council-votes-to-cease-standards-development-of-NFPA-277



#### **Other Positions**

 Fire Fighters: It would appear that any proposed new fire test designed to resists ignition from a second item and/or designed to limit growth of Heat Release Rate will require much higher levels of FR than those required to pass TB117. Probably at similar levels or exceeding TB133 (15-30%)"

Why Do Fire Fighters Support the Banning of Flame Retardants? Joseph Fleming PFFM (Professional Fire Fighters of Massachusetts) http://greensciencepolicy.org/wp-content/uploads/2018/02/6-Fleming\_FRDPresentation\_2518.pdf

**CPSC** recommends to refrain from intentionally adding nonpolymeric, organohalogen FRs

[CPSC Docket No. CPSC-2015-0022, Sept'17]

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State of Maine first State banning all flame retardants in RUF
 Effective on Jan 1 2018 - https://www.mainelegislature.org/legis/bills/bills\_128th/billtexts/HP013801.asp

#### **Other Positions**

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CPSC Docket No. CPSC-2015-0022, Sept'17

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## What is NIST doing?

 NIST SP1220 Workshop Report: Research Roadmap for Reducing the Fire Hazard of Materials in the Future (2018):

https://www.nist.gov/publications/workshop-report-research-roadmap-reducing-fire-hazard-materials-future

identified RUF as the top priority application for fire safety research in terms of overall impact on the fire problem

NIST project - Low Heat Release Upholstered Furniture

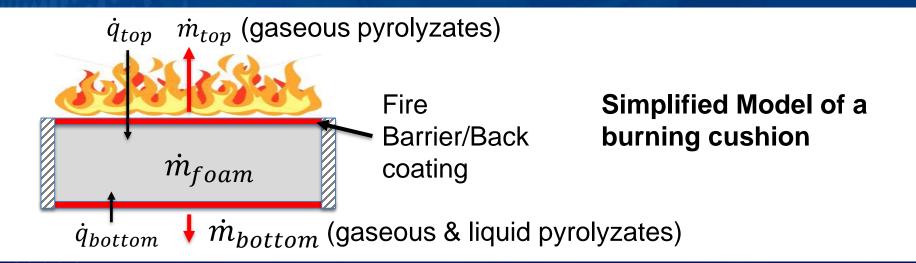
#### **Project Objectives:**

- low heat release rate RUF without the need for fire FR.
- bench-scale methodology for predicting the RUF flaming hazard.
- robust standard reference cigarettes for smoldering ignition testing
- bench-scale methodology for predicting the RUF smoldering hazard.

#### **Fire Barriers**

Reduce flammability without the use of chemical FRs by reducing

(1) Heat Transfer and (2) Mass Transfer (of pyrolyzates produced by foam decomposition)



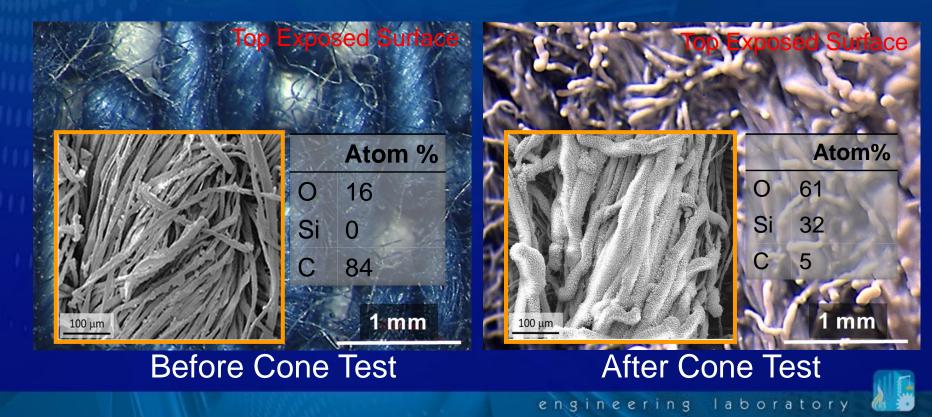


#### **NIST Silicone Backcoating**

Zammarano et al., Smoldering and Flame Resistant Textiles via Conformal Barrier Formation, Adv. Mat. Interf., Nov 2016

FORMULATION (Flexible Pre-ceramic):

- Vinyl terminated PDMS crosslinked by Pt-catalyzed hydrosilation.
- Vinyl-modified aluminum-hydroxide (65 % by mass)
- vinyl-modified nanosilica (13 % by mass)
- Ethyl acetate (solvent)



#### Silicone Backcoating – Large Scale

- Four cushion **mock-ups**:
- California TB 133 burner
  (18 kW square burner) 80 s
- Cover Fabric (Cotton velvet):
   Uncoated (UC) vs. Backcoated (BC)

| Sample     | Area<br>density<br>[g m <sup>-2</sup> ] | Thickness<br>[mm] |
|------------|---|-------------------|
| Uncoated   | 447±3                                   | 1.3 ±0.2          |
| Backcoated | 813±16                                  | 1.5 ±0.3          |



#### **Uncoated Mock-up**



## **Backcoated Mock-up**

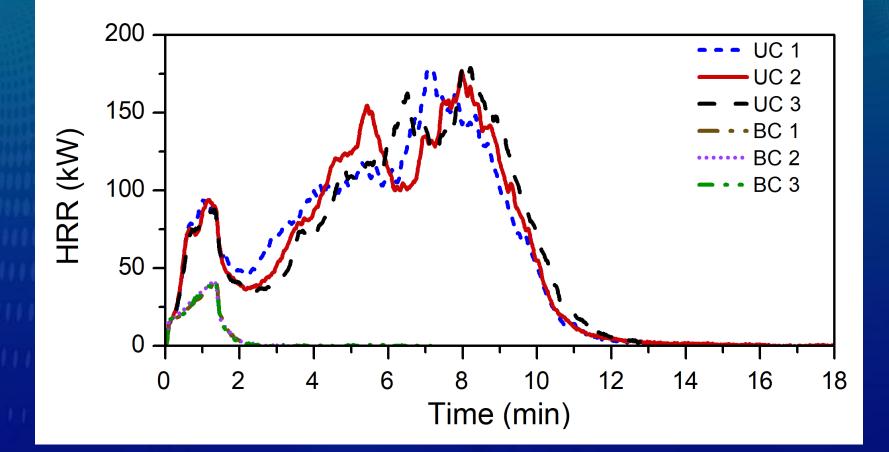


## **Seams are Critical**



- Backcoated fabric: no sign of failure
- Kevlar thread failure

#### HRR



Triplicate tests with high repeatability

#### **Data Summary**

|            | Peak HRR | Total Heat<br>Release | Mass Loss | EHC       |
|------------|----------|-----------------------|-----------|-----------|
|            | [kW]     | [MJ]                  | [%]       | [kJ/g]    |
| Uncoated   | 179±2    | 59.2 ±0.7             | 95.5 ±0.8 | 22.6 ±0.1 |
| Backcoated | 24±1     | 1.3 ±0.1              | 3.8 ±0.1  | 8.3 ±0.5  |



Backcoated sample after test



Backcoattencoatenpleamipheutteovestabric

## **Smoldering Ignition Resistance**

#### NIST Docket number: 15-026US1 **U.S. PATENT** filed on April 21, 2016



Playback Speed: 500 x On the Left

Filling: Cal TB 117-2013 Polyurethane Foam

Fabric: Backcoated Cotton Velvet

Heat source: SRM 1196 cigarette

On the Right

Filling: Cal TB 117-2013 Polyurethane Foam

Fabric: Uncoated Cotton Velvet (TB 117-2013, Type 2)

Heat source: SRM 1196 cigarette



#### Backcoated

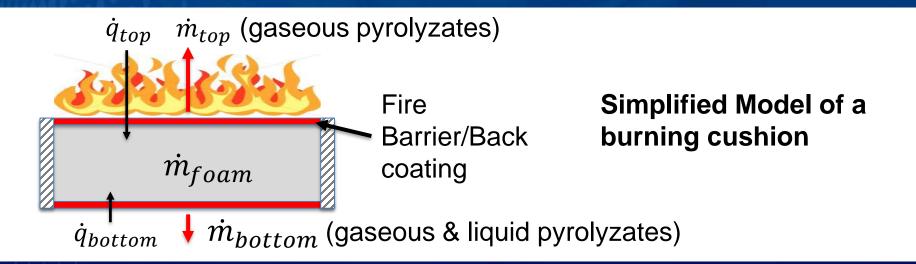
#### Uncoated



#### **Fire Barriers**

Reduce flammability without the use of chemical FRs by reducing

(1) Heat Transfer and (2) Mass Transfer (of pyrolyzates produced by foam decomposition)



**Challenge -** Design a bench-scale test capable of capturing the effect of Heat Transfer and Mass Transfer on HRR of RUF after ignition

# **Cone Calorimetry for RUF**

<u>CBUF Test</u> (*de-facto* standard)
 Foam Size: ≈ 4" × 4" × 2"
 ≈ (102 × 102 × 51) mm<sup>3</sup>

NIST Cube Test
 Foam Size: ≈ 41/4" × 41/4" × 41/4"
 ≈ (108 × 108 × 108) mm<sup>3</sup>





#### **Cube test: capturing mass transfer effects**



# POOL FIRE!





#### Combustion Efficiency $\downarrow$



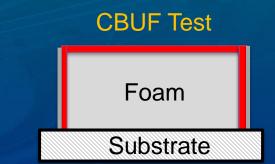
# **Fabric to Foam ratios**

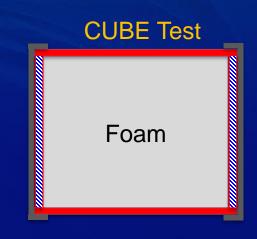
|              | Area <sub>fabric</sub> /Volume <sub>foam</sub><br>(m <sup>-1</sup> ) |  |  |  |
|--------------|--|--|--|--|
| RUF Cushion* | 19.1   |  |  |  |
| Cube         | 19.0   |  |  |  |
| CBUF         | 58.8   |  |  |  |

\*(610×737×152)cm<sup>3</sup>≈ (24×29×6)in.<sup>3</sup>

For  $\rho_{foam}$ =29 kg/m<sup>3</sup> and  $\rho_{fabric}$ = 0.4 kg/m<sup>2</sup>

|              | Mass <sub>foam</sub> /Mass <sub>fabric</sub> |  |  |  |
|--------------|--|--|--|--|
| RUF Cushion* | 3.8  |  |  |  |
| Cube         | 3.8  |  |  |  |
| CBUF         | 1.2  |  |  |  |





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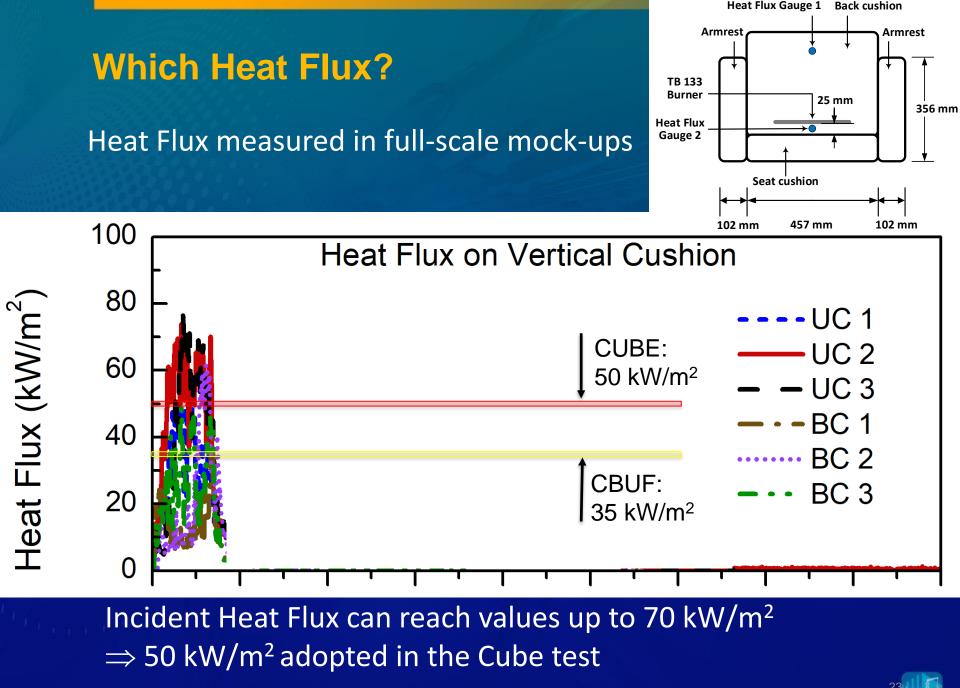
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## **CBUF Test: Sample Preparation** (~30 min+24h)



## **Cube Test: Sample Preparation**





#### **Correlation between CUBE and CBUF tests**

- 11 Commercial Barriers were tested in triplicate tests in the CUBE and CBUF test
  - Type barrier: woven, non-woven, knitted, backcoated
  - Thickness range: 0.5 mm to 10 mm
  - FRs: X, Sb, P, N, Si
- 1 Foam:
- No-FR, TB117-2013 foam





# **Edge Effects**

BF19 - External Heat Flux: 50 kW/m2

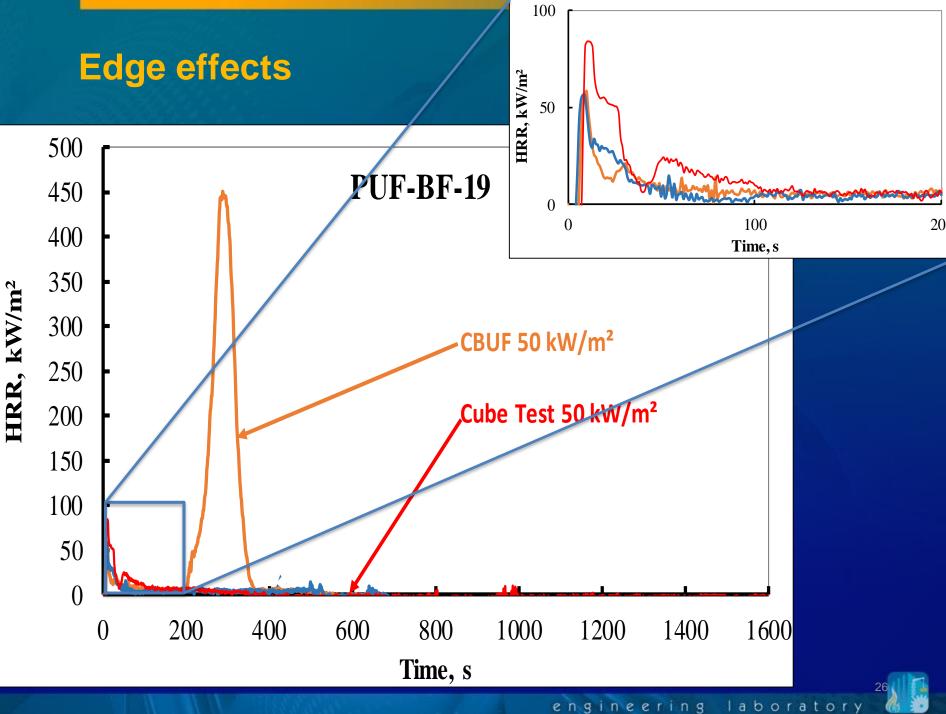
#### Playback Speed: 32x





#### Cube Test

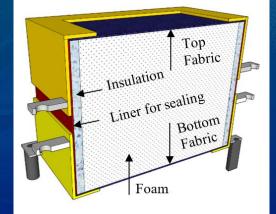




## Failure Induced by Barrier Shrinkage

#### Certain fire barriers tend to shrink (e.g., cellulosics)

CBUF: Barrier is not constrained Cube Test: Barrier is constrained by edge seal

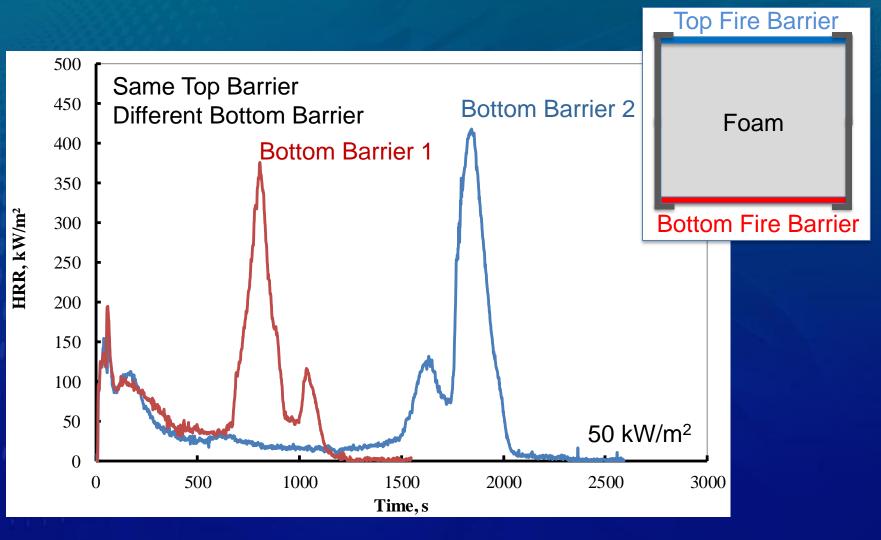


No stress induced failure

Shrinkage induces stress and possible failure



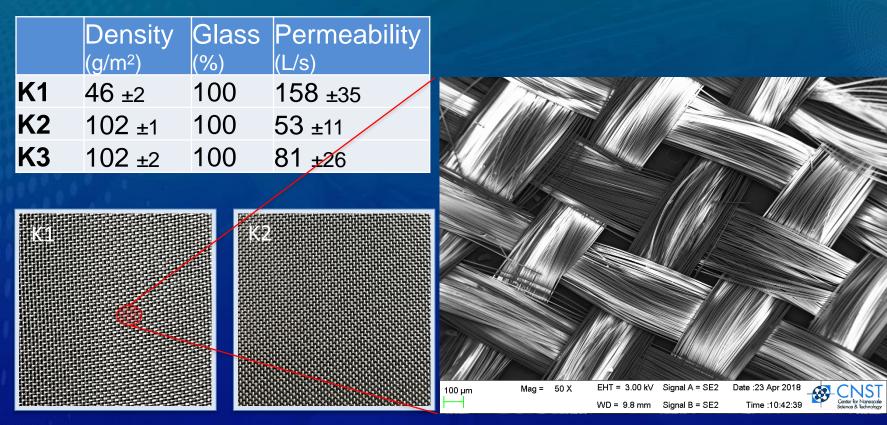
## **Cube Test: Effect of Bottom Upholstery Fabrics**



The cube test captures the effect of bottom fire barrier

#### **FR-free barriers: Glass Fabrics**

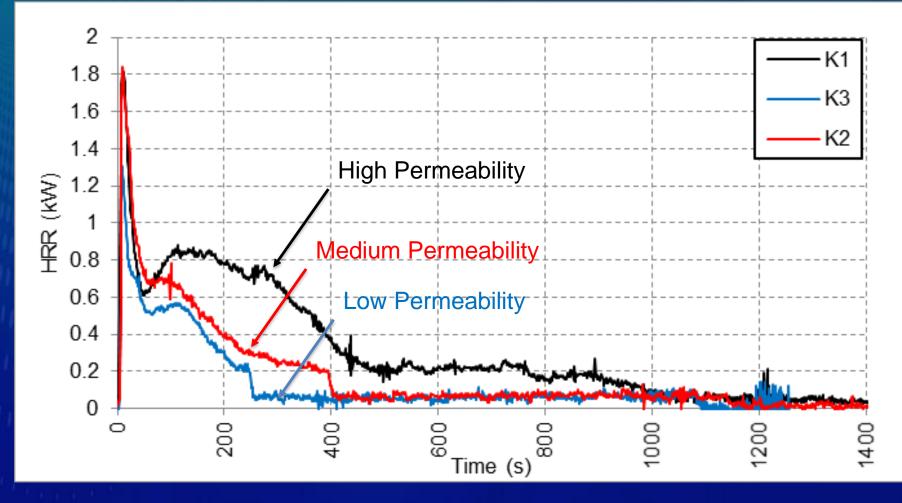
3 fabrics (K1, K2, K3), 100% Glass, no sizing



Pictures of the 3 glass fabrics (25 mm by 25 mm)

K1: Plain weave, nominally  $48.5 \text{ g/m}^2$  (1.43 oz/yd<sup>2</sup>) K2: Plain weave, nominally 107.1 g/m<sup>2</sup> (3.16 oz/yd<sup>2</sup>) K3: Satin weave, nominally 107.1 g/m<sup>2</sup> (3.16 oz/yd<sup>2</sup>)

#### **Glass Fabrics as Fire Barriers – Cube Performance**



Glass fabrics appear to be very effective even at a very low areal densities of 46 g/m<sup>2</sup> In a typical cushion the glass would account for less than 3 % of the mass of the cushion

#### **Glass Fabrics as Fire Barriers – Summary**

|         | ti<br>(s) |                 | AHR<br>(kW) |         | <b>EHC</b><br>(MJ/kg) | Foam ML<br>(%) |
|---------|-----------|-----------------|-------------|---------|-----------------------|----------------|
| Foam    | 2 ±1      | 10.2 ±0.3       | 4.6 ±0.2    | 938 ±15 | 27.0 ±0.3             | 97 ±2          |
| K1+Foam | 3 ±1      | <b>1.8</b> ±0.1 | 0.35 ±0.14  | 461 ±24 | 21.2 ±0.2             | 58 ±4          |
| K2+Foam | 5 ±1      | 1.4 ±0.1        | 0.17 ±0.03  | 238 ±71 | 13.9 ±0.7             | 47 ±11         |
| K3+Foam | 5 ±1      | 1.7 ±0.1        | 0.16 ±0.02  | 237 ±17 | 16.8 ±0.9             | 39 ±2          |

# The use of glass fabrics as fire barriers induces:

- 6- to 7-fold reduction in PHRR
- 1.3- to 2-fold reduction in EHC



Combustion Efficiency  $\downarrow$ 

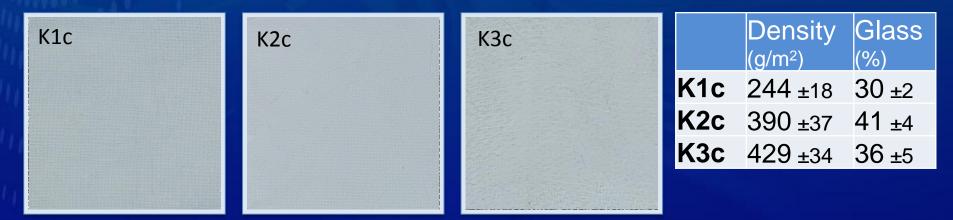


#### **Glass Fabrics + Silicone Coating**

SILICONE COATING FORMULATION:

Vinyl terminated PDMS crosslinked by Pt-catalyzed hydrosilation.

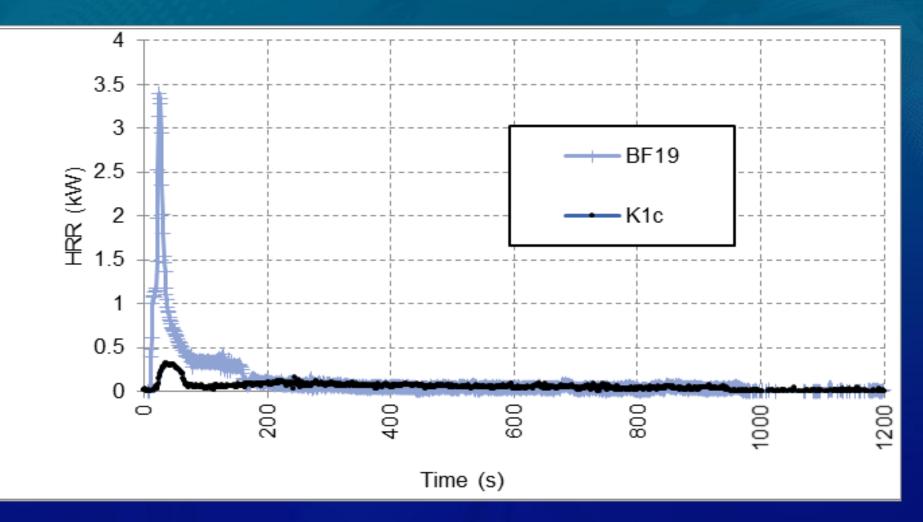
- □ Vinyl-modified aluminum-hydroxide (65 % by mass)
- vinyl-modified nanosilica (13 % by mass)
- Ethyl acetate (solvent)



Sample size shown (25 mm by 25 mm)

Case Western Reserve University: Kimberly DeGracia, PhD Candidate, Prof. David A Schiraldi

#### **Glass Fabrics + Silicone Coating – Cube**



#### **Glass Fabrics + Silicone Coating – Cube**

|          | Ignition time | Peak HRR        | AHR          | THR            | EHC       | Mass Loss  |
|----------|---------------|-----------------|--------------|----------------|-----------|------------|
|          | (S)           | (kW)            | (kW)         | (KJ)           | (MJ/kg)   | (%)        |
| Foam     | 2 ±1          | 10.2 ±0.3       | 4.6 ±0.2     | 938 ±15        | 27.0 ±0.3 | 97 ±2      |
| K1+Foam  | 3 ±1          | <b>1.8</b> ±0.1 | 0.35 ±0.14   | <b>461</b> ±24 | 21.2 ±0.2 | 55.4 ±3.7  |
| K2+Foam  | 5 ±1          | <b>1.4</b> ±0.1 | 0.17 ±0.03   | 238 ±71        | 13.9 ±0.7 | 42.6 ±10.3 |
| K3+Foam  | 5 ±1          | <b>1.7</b> ±0.1 | 0.16 ±0.02   | 237 ±17        | 16.8 ±0.9 | 35.1 ±1.5  |
| K1c+Foam | 25 ±4         | 0.3 ±0.02       | 0.051 ±0.003 | 55 ±7          | -         | 5.9 ±0.25  |
| K2c+Foam | 35            | 0.58            | 0.05         | 54             | -         | 2.33       |
| K3c+Foam | 31            | 0.62            | 0.04         | 51             | -         | 2.9        |

The addition of the coating to the glass fabrics induces:

- 7-fold increase in ignition time
- 2- to 8-fold reduction in Peak HRR
- 9- to 18-fold reduction in Mass Loss of the foam

# Conclusions

- NIST developed silicone backcoatings have proven to be an effective all-in-one solution for fire-safe RUF
- A bench-scale test for fire barriers has been developed at NIST
- Glass Fabrics appear to be effective Fire Barriers

**Ongoing NIST research (Real-scale tests):** 

- Feasibility of Low Heat Release Furniture without FRs
- Full-scale performance prediction by Cube test



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# **THANK YOU!**

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*Kimberly DeGracia, PhD Candidate, Prof. David A Schiraldi* 



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