



Update on Diffusion Mobilities in Oxide Systems

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Diffusion workshop
25-26 March 2009
NIST, USA



Aim of work

Predict oxidation:

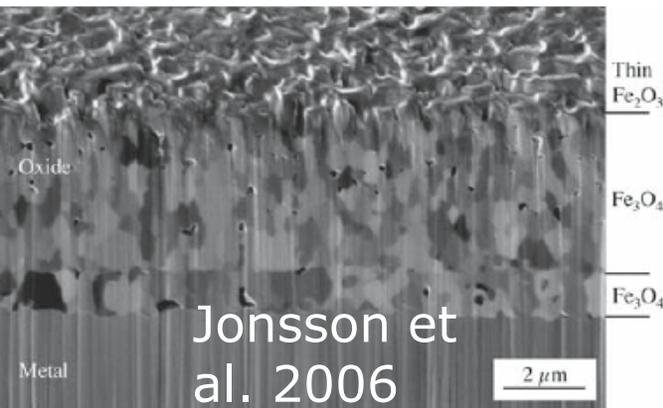
- Sharp-interface methods – DICTRA
- Diffuse-interface methods – phase-field

For example:

- Oxidation of steels
- Degradation of superalloy coatings

We need:

- Mathematical expressions for flux as function of gradients in composition or chemical potentials.
- Parameters that characterize a given material





Background

Ferritic 9-12 % Cr steels

The life-time of is limited by:

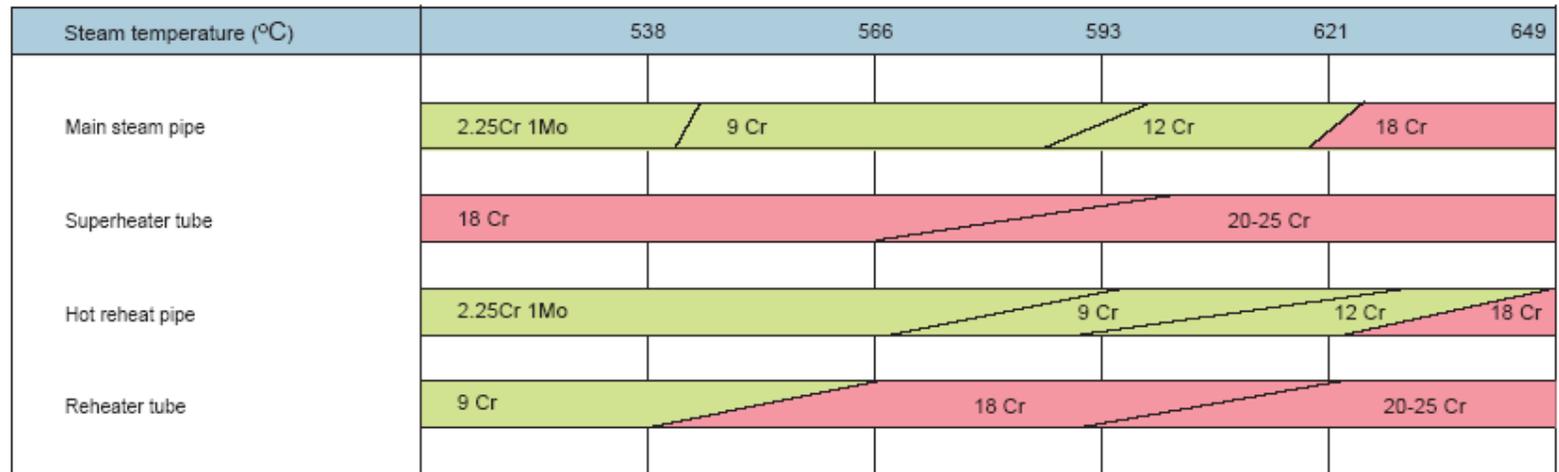
- Creep
- Oxidation.

Design requirement: at least 100 000 h at 100 MPa



Avedøre (Copenhagen)

Fig. 3 Steam conditions and high temperature materials



: Ferritic Material
 : Austenitic Material



Content

- Background
- Modelling of oxidation
- Bulk diffusion in oxides
- Grain boundary diffusion
- Kirkendall porosity
- Effect of water vapour



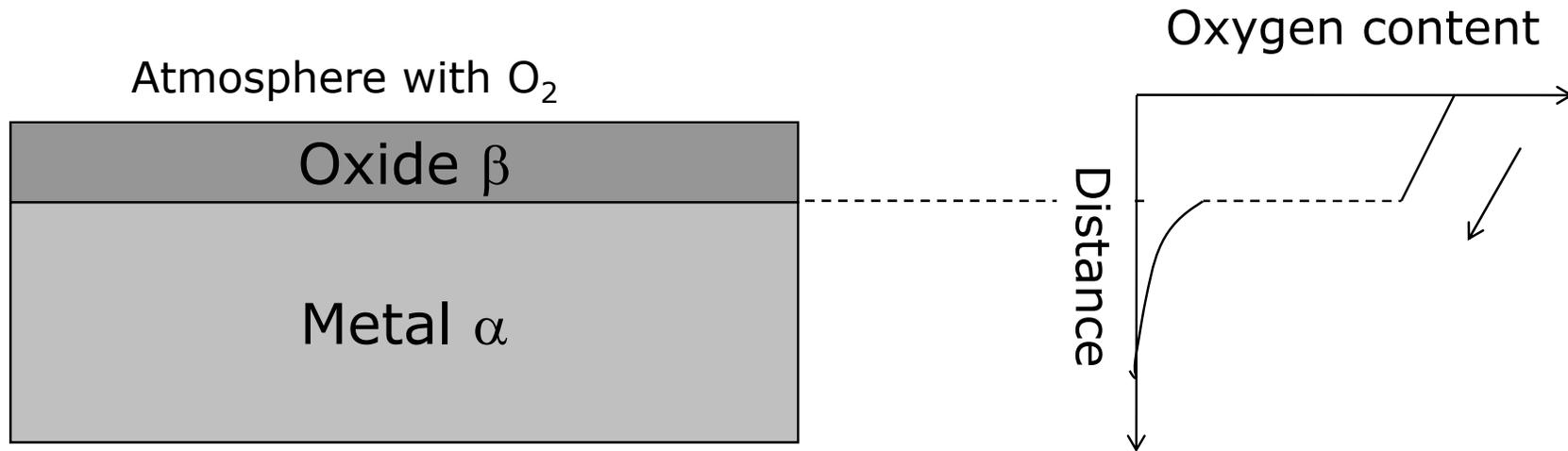
Modelling of oxidation - issues

Predict:

- Rate of oxidation
- What oxides form
- Porosity



Growth of oxide layers – how fast do the layers grow?



Flux balances in sharp-interface modelling!



General approach

Flux:

$$J = -L \frac{\partial \mu}{\partial x} = -L \frac{\partial \mu}{\partial c} \frac{\partial c}{\partial x} = -D \frac{\partial c}{\partial x}$$

$$D = L \frac{\partial \mu}{\partial c}$$

Kinetic parameters
from model.

Darken's thermodynamic factor,
e.g. from Calphad analysis.

Base models on a vacancy mechanism!



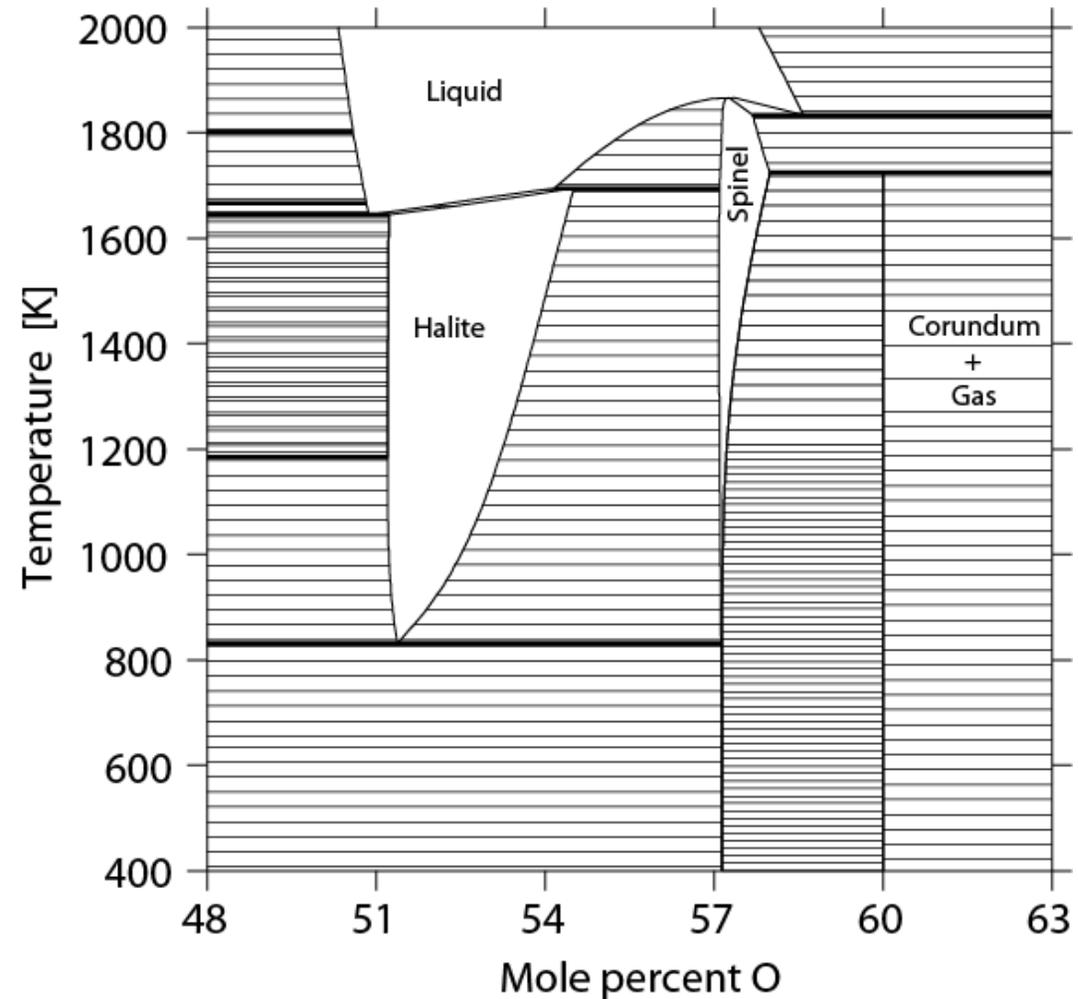
At present:

- Models included in DICTRA
Our data base now contains diffusional mobilities of
- Wustite
 - Fe
 - O missing but probably very small
- Magnetite (spinel)
 - Fe, Cr ongoing
 - O
- Hematite (Corundum)
 - Fe, Cr
 - O missing but similar to Fe



The Fe-O system

- Calculated from Sundman 1991.





Ionic systems – two extremes

- Electronic conduction compared to diffusion:
 - Much faster (charge does not need to be included)
 - Much slower (ions diffuse as species)

If electronic conduction and diffusion are about the same rate (electronic conduction needs to be accounted for)



Fe diffusion in spinel (lattice-fixed frame of reference)

Absolute reaction rate arguments:

$$J_{Fe}' = - \frac{1}{2} \left[y_{Va}'' y_{Fe}'' M_{FeVa}'' + y_{Fe}''' y_{Va}''' M_{FeVa}''' \right] \frac{1}{V_s} \frac{\partial \mu_{Fe}}{\partial z}$$

Normal octahedral sites

extra octahedral sites

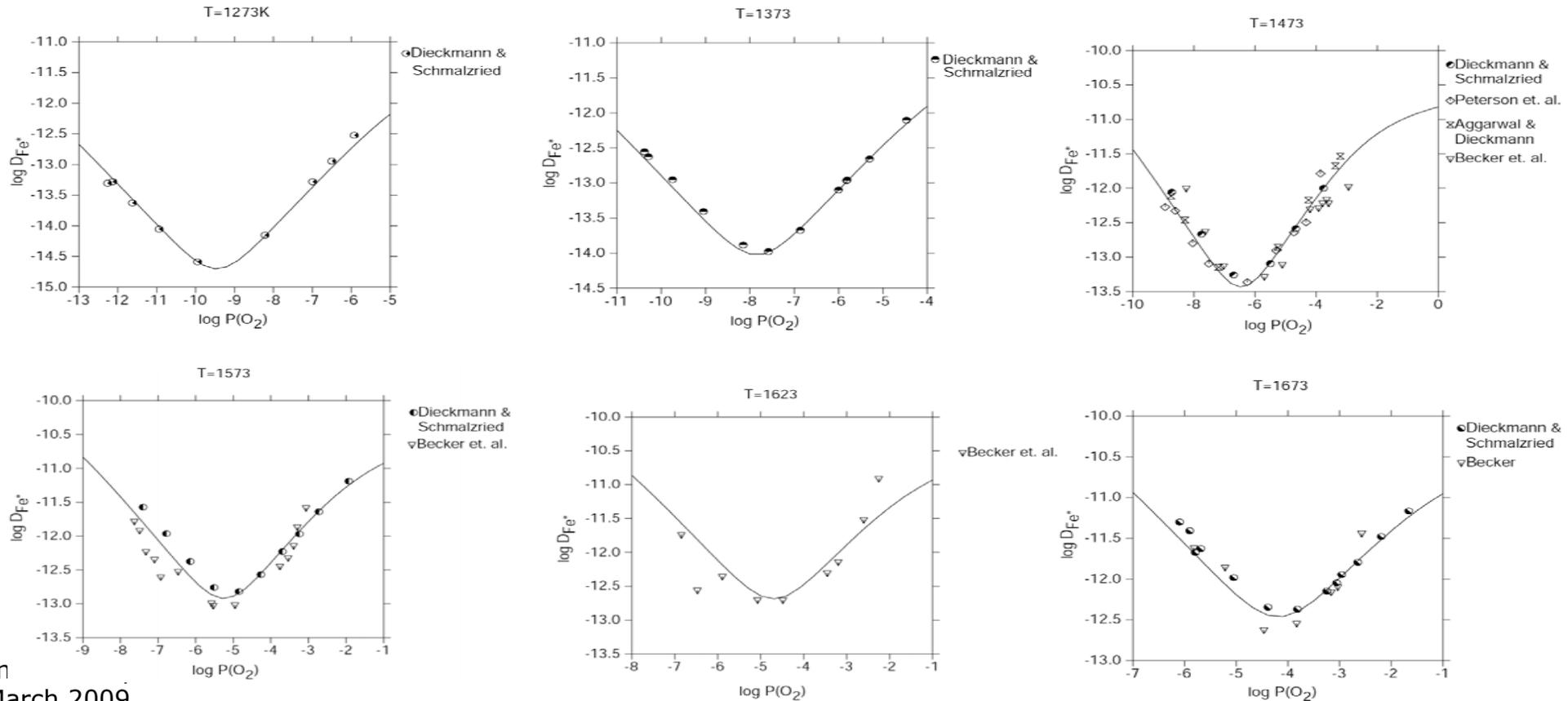
L_{Fe}

$$RTM_k = \delta^2 v \exp(-\Delta G_k / RT)$$

$$D_{Fe^*} \cong RT \frac{1}{2} \left[y_{Va}'' y_{Fe}'' M_{FeVa}'' + y_{Fe}''' y_{Va}''' M_{FeVa}''' \right] \frac{1}{u_{Fe}}$$



Experimental data on Fe tracer diffusion in spinel - Optimization of Fe mobilities (Hallström et al. 2008)

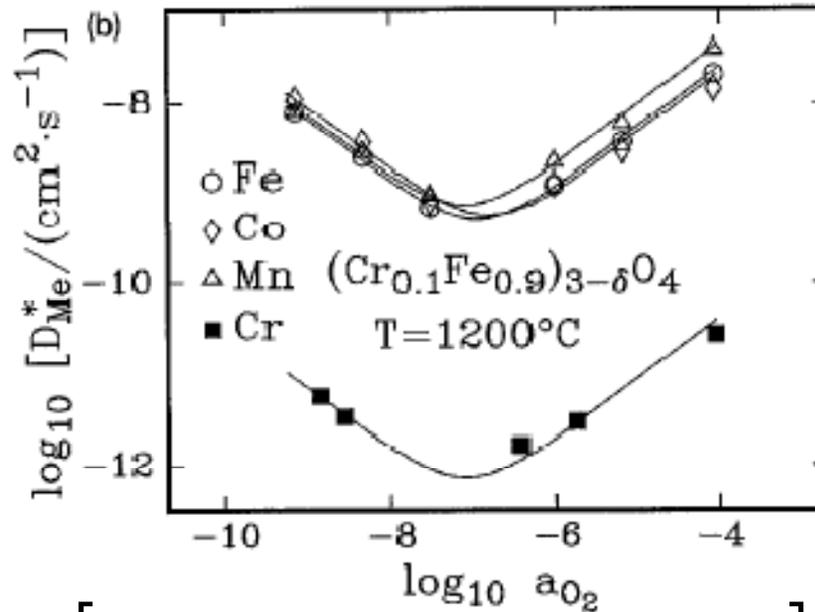


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Alloy elements in spinel (lattice fixed frame of reference)

Töpfer et.al. 1995



Cr content of inward growing spinel will inherit Cr content of alloy.

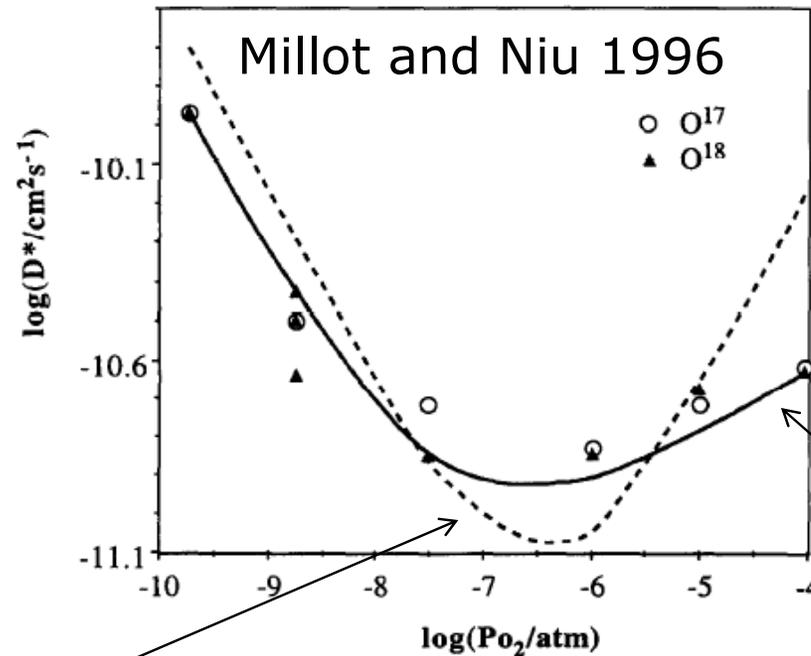
$$J_{Cr}' = - \left[y_{Va}'' y_{Cr}'' M_{CrVa}'' + y_{Cr}''' y_{Va}''' M_{CrVa}''' \right] \frac{1}{V_s} \frac{\partial \mu_{Cr}}{\partial z}$$

$$D_{Cr^*} = RT \left[y_{Va}'' y_{Cr}'' M_{CrVa}'' + y_{Cr}''' y_{Va}''' M_{CrVa}''' \right] / u_{Cr}$$



O tracer diffusion in spinel (lattice-fixed frame of reference)

T = 1150°C



$$J_O = - \left[y_{Va}^a y_O^a M_{OVa}^a + y_O^i y_{Va}^i M_{OVa}^i \right] \frac{1}{V_m} \frac{\partial \mu_O}{\partial z}$$

$$\text{or } J_O = - y_{Va}^a y_O^a M_{OVa}^a \frac{1}{V_m} \frac{\partial \mu_O}{\partial z} \quad y_{Va}^a = \left[y_{Va}'' y_{Fe}'' k_{FeVa}'' + y_{Va}''' y_{Fe}''' k_{FeVa}''' \right]$$

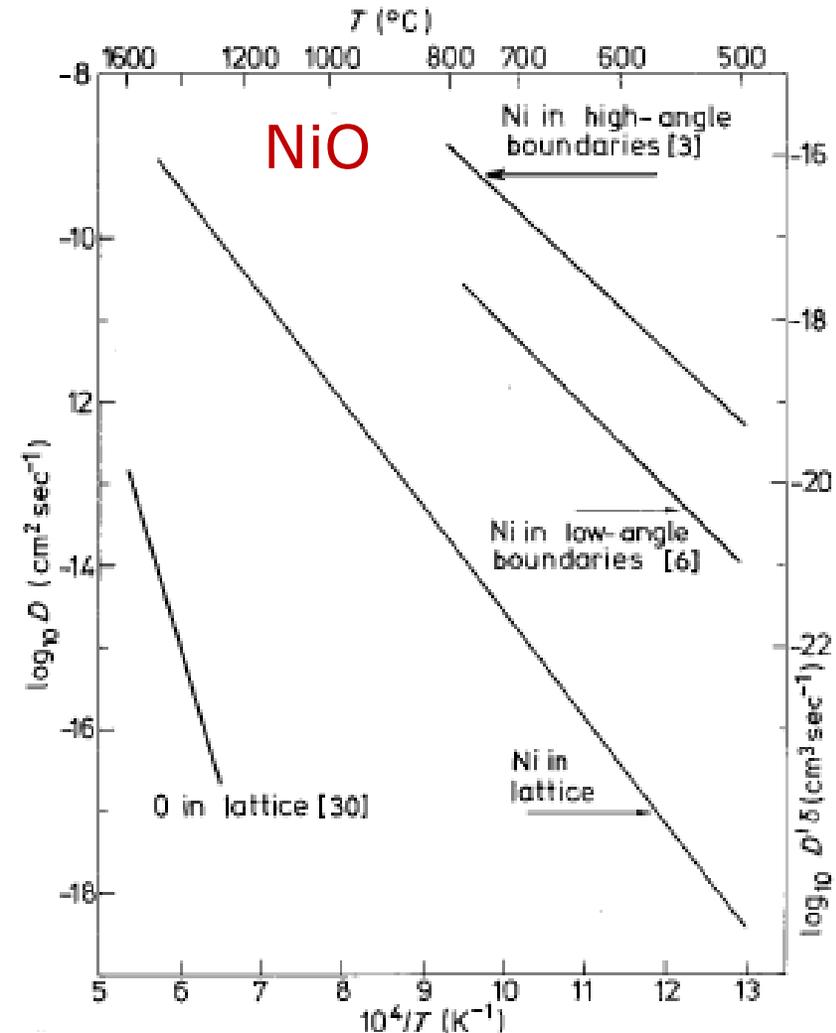


Effect of grain boundaries

Simplified approach:

$$D_{eff} = (1 - \delta / d) D_{bulk} + \delta / d D_{gb}$$

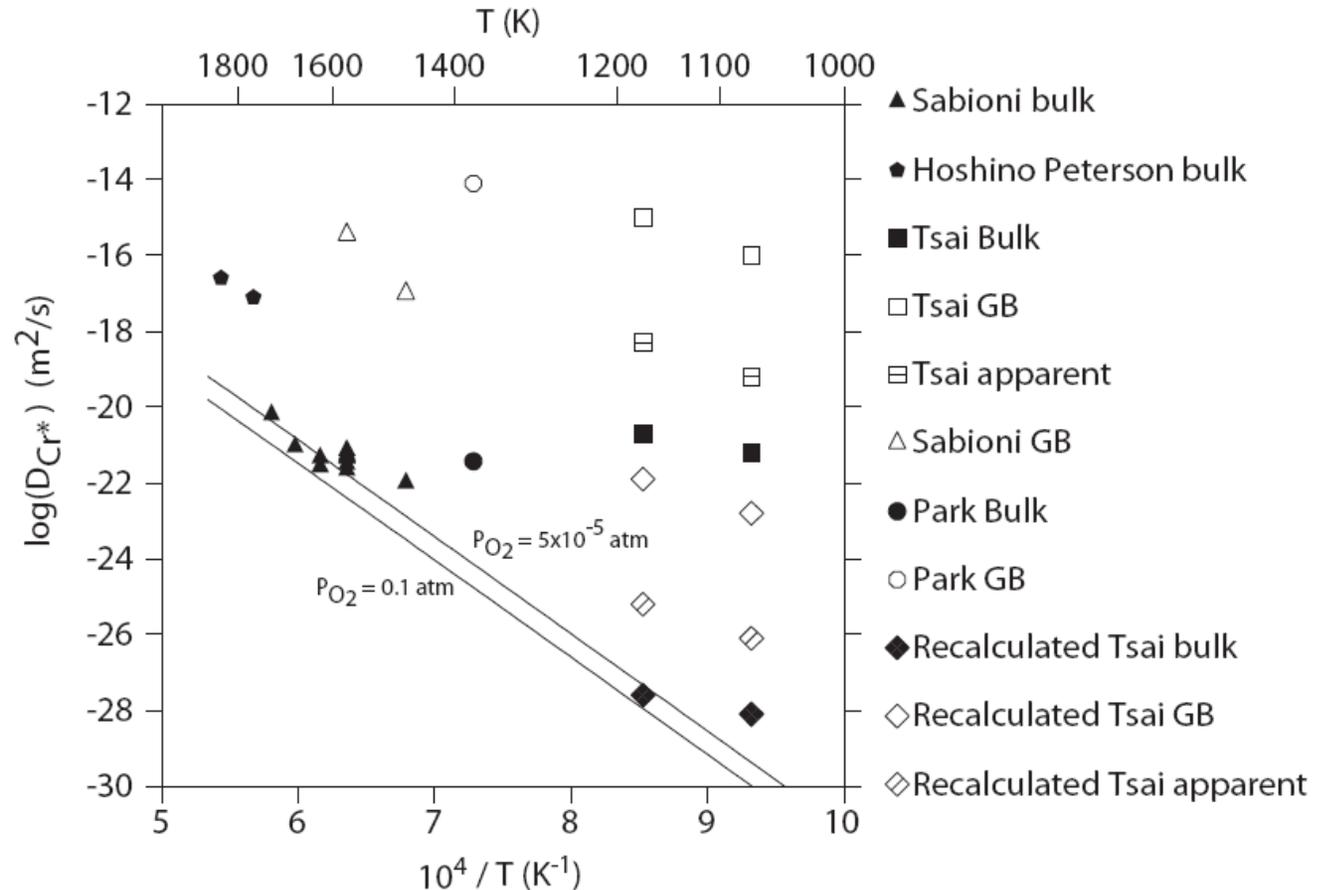
$$Q_{gb} \cong \alpha Q_{bulk} \quad 0.3 < \alpha < 0.5$$





Cr tracer in Cr_2O_3

- Q estimated from diffusion of Fe in hematite (isostructural).
- Lowest values should correspond to the most pure material.
- Values from Sabioni and Tsai (recalculated to tracer) used in optimization.





Simulations of oxidation of pure Fe at 600°C in dry atmosphere

- 600°C, $P_{O_2}=0.05$, 24h.
- $d^{\text{mag}} \approx 3\mu\text{m}$, $d^{\text{cor}} \approx 0.1\mu\text{m}$, $\delta=5$ nm
- Gb diffusion accounted for in magnetite and hematite.

$$D_{\text{eff}} = (1 - \delta / d) D_{\text{bulk}} + \delta / d D_{\text{gb}}$$

$$Q_{\text{gb}} \cong \alpha Q_{\text{bulk}} \quad 0.3 < \alpha < 0.5$$

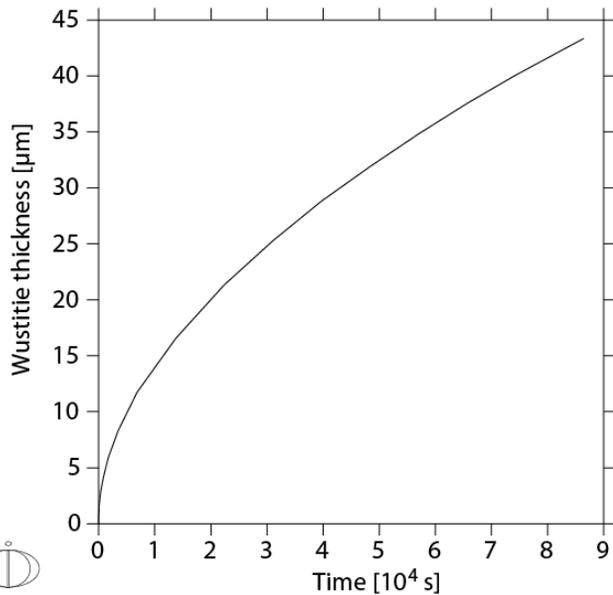
- Oxygen diffusion neglected



Simulation: $\alpha=0.33$ oxide thicknesses

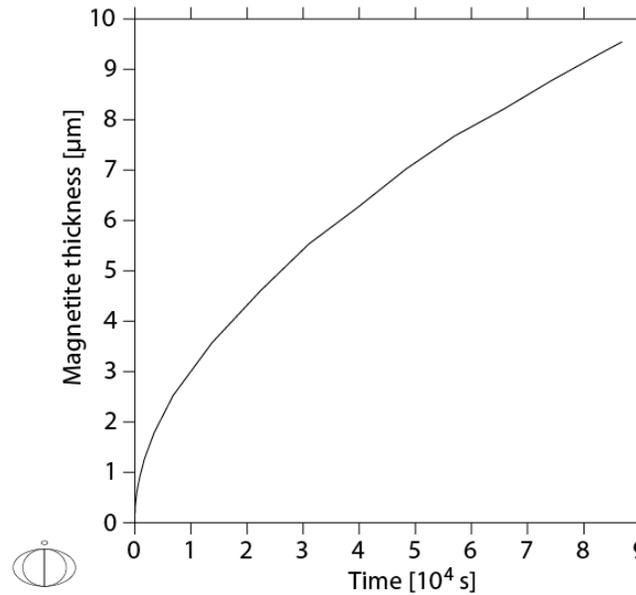


Wustite



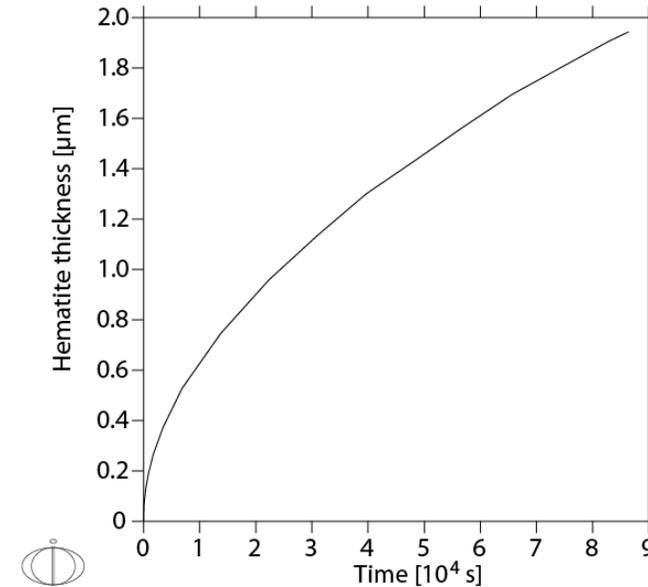
Calculated: 45 μm
Experimental: 21 μm

Magnetite



10 μm
11 μm

Hematite



2 μm
2 μm



Kirkendall effect - porosity

Oxygen is substitutional, divergence of oxygen flux gives Kirkendall effect:

$$\frac{v}{V_m} = -J = -J'_{O_2} / x_{O_2} \quad V_m = \text{molar volume/mole of atoms}$$

Rate of density ($\rho = 1/V_m$) change:

$$\frac{1}{V_m^2} \dot{V}_m = \mathbf{div}(J)$$

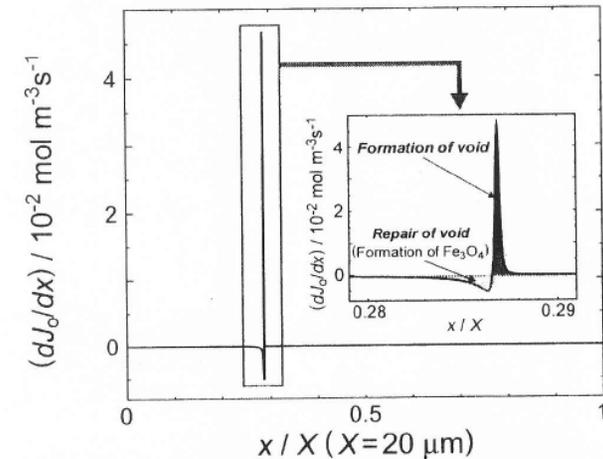
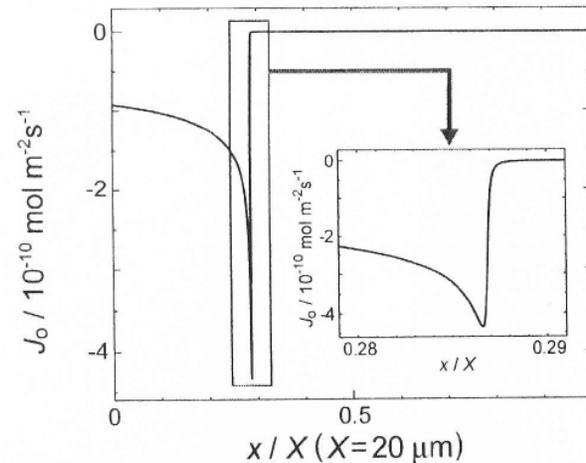
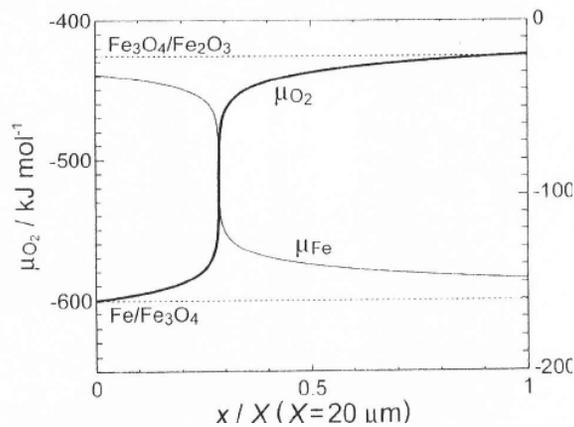
No porosity \Rightarrow Strain rate:

$$\dot{\epsilon}_{11} + \dot{\epsilon}_{22} + \dot{\epsilon}_{33} = \frac{1}{V_m} \dot{V}_m = V_m \mathbf{div}(J)$$

Only porosity (volume fraction f_p):

$$\frac{\dot{f}_p}{(1-f_p)^2} = -V_m \mathbf{div}(J)$$

Maruyama et al. 2004

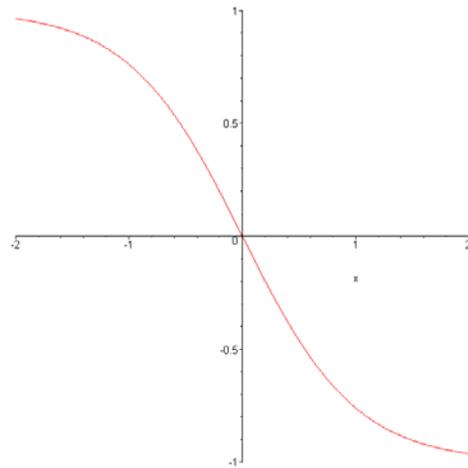


Voids form as a consequence of a divergence in the oxygen flux.



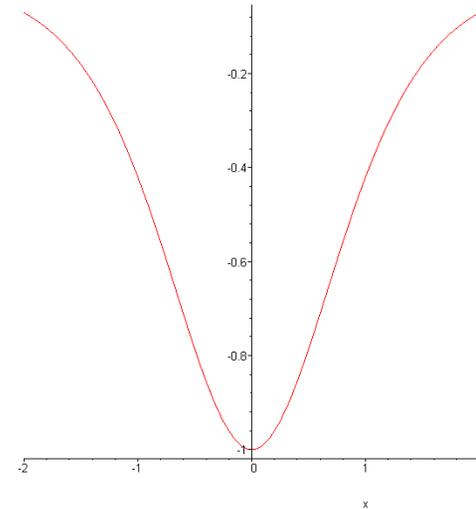
Schematics of Kirkendall effect in magnetite

μ_{Fe}



Distance

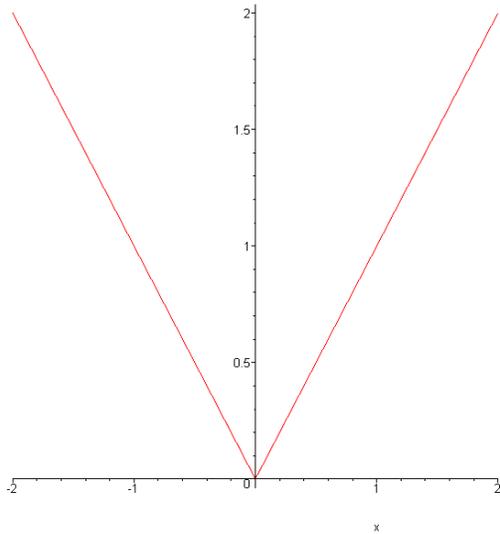
$$\frac{\partial \mu_{Fe}}{\partial z}$$



Distance

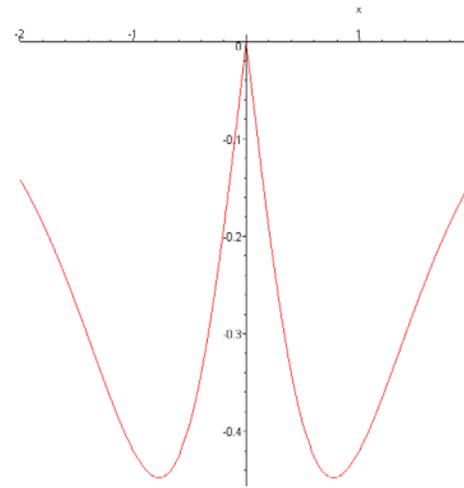


Oxygen mobility



Distance

Oxygen flux



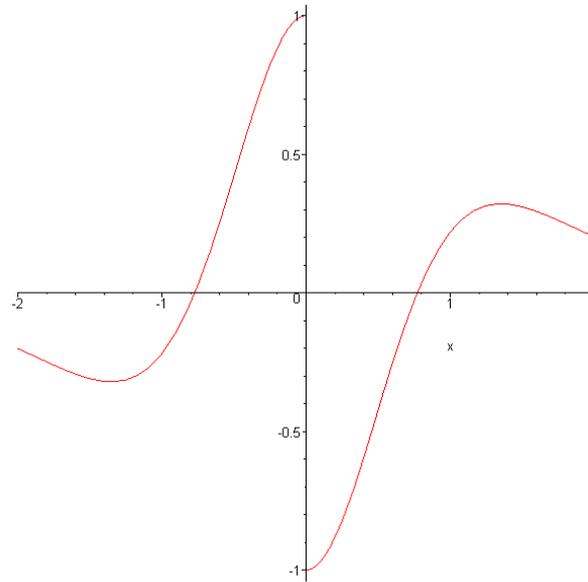
Distance



$$\partial y_{Va} / \partial t = \partial J_o / \partial z$$

Pores

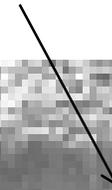
Pores



Distance

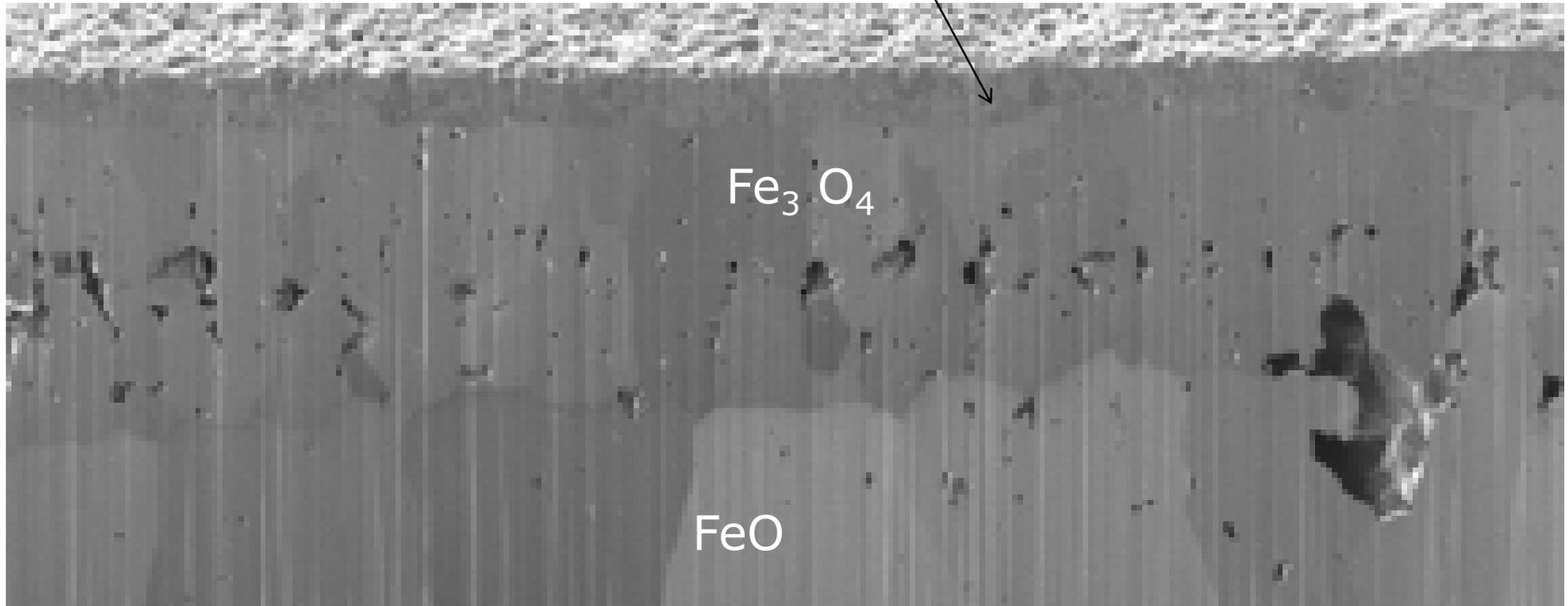


Fe_2O_3



Fe_3O_4

FeO



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T. Jonsson et al. 2008



Simulations of oxidation of pure Fe at 500°C in dry atmosphere

- 500°C, $P_{O_2}=1$ atm
- $d^{\text{mag}} \approx 3\mu\text{m}$, $d^{\text{cor}} \approx 0.1\mu\text{m}$, $\delta=5$ nm
- Gb diffusion accounted for in magnetite and hematite.

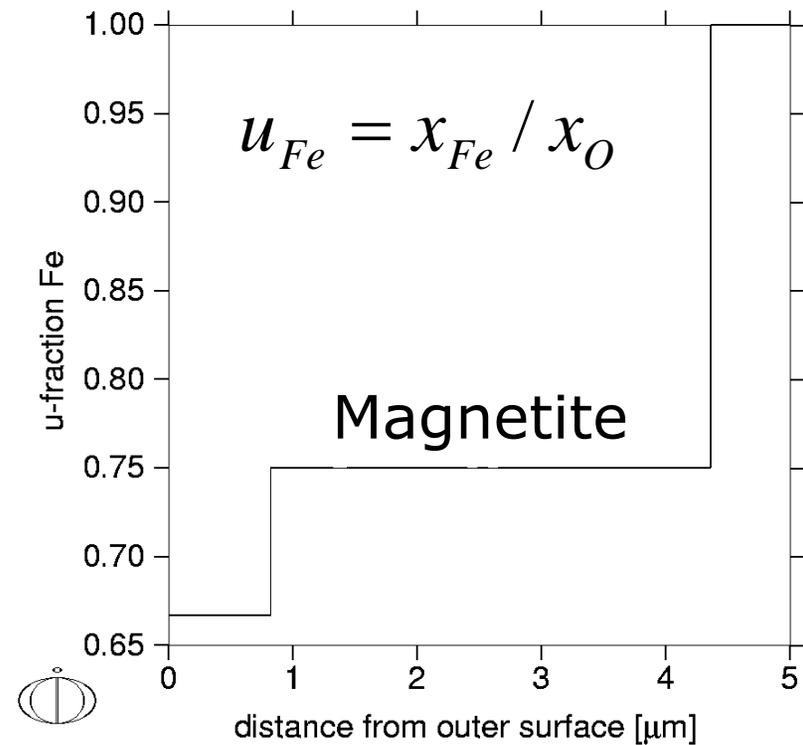
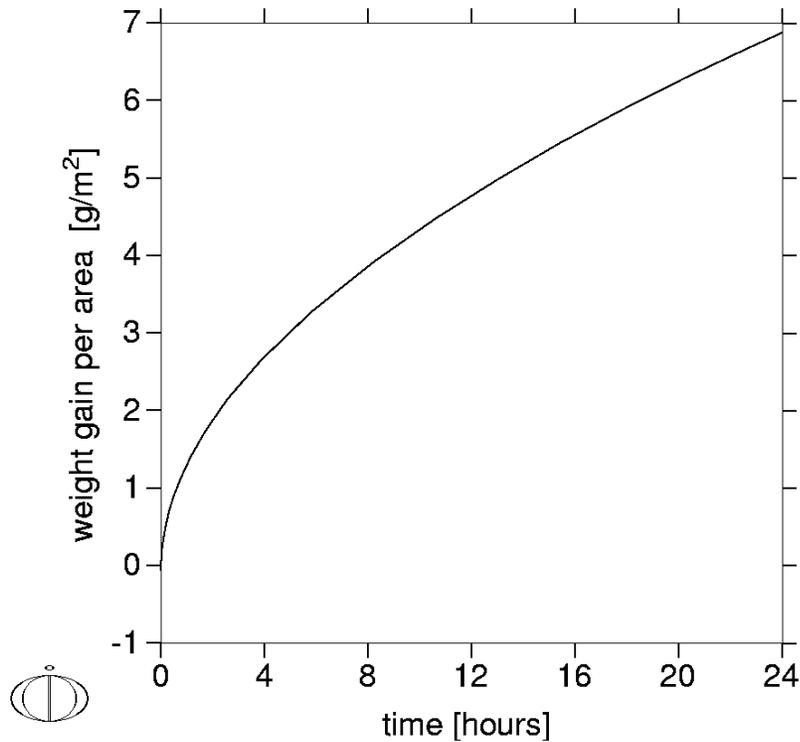
$$D_{\text{eff}} = (1 - \delta / d) D_{\text{bulk}} + \delta / d D_{\text{gb}}$$

$$Q_{\text{gb}} \cong \alpha Q_{\text{bulk}} \quad 0.3 < \alpha < 0.5$$

- Oxygen diffusion included



Fe-profile after 24 h

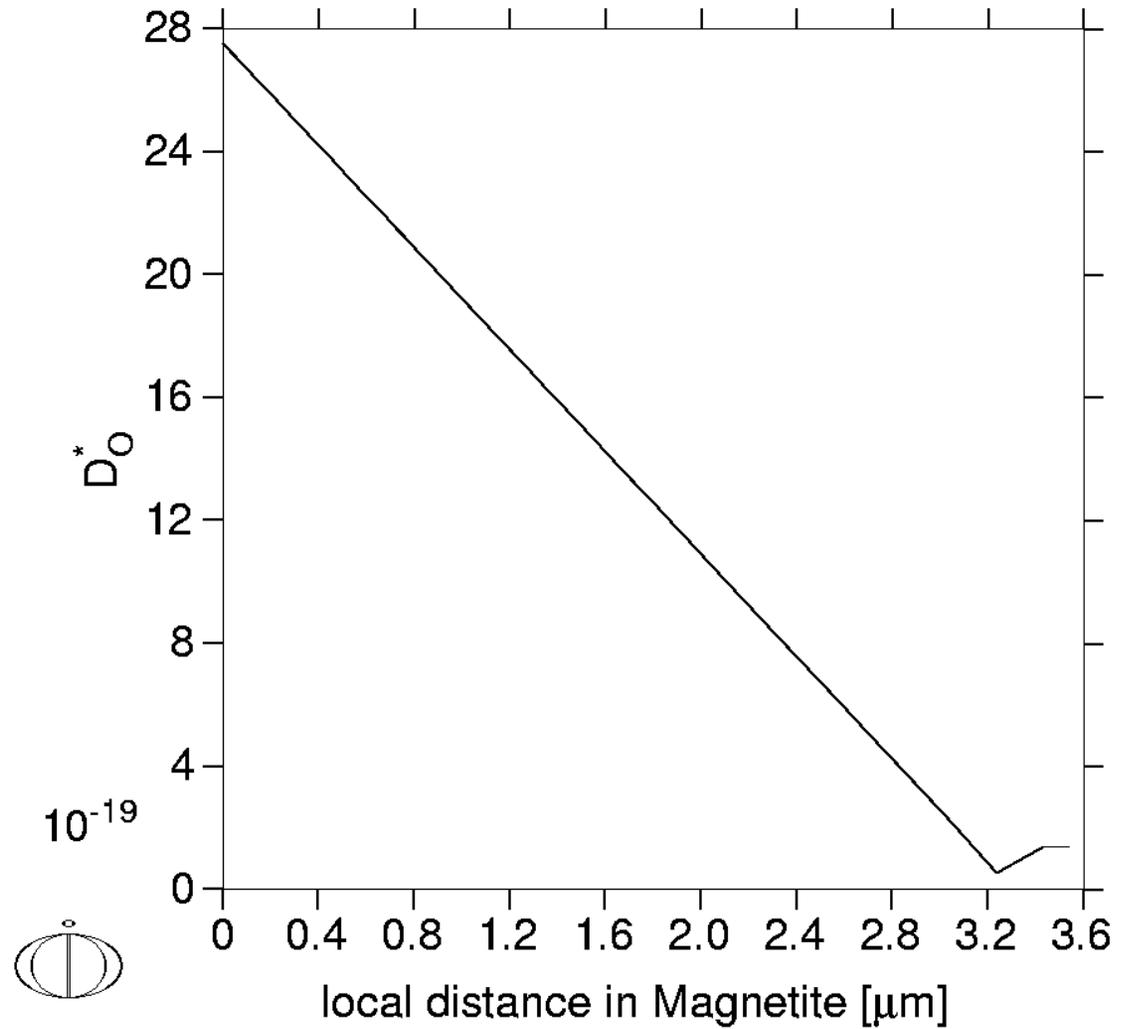


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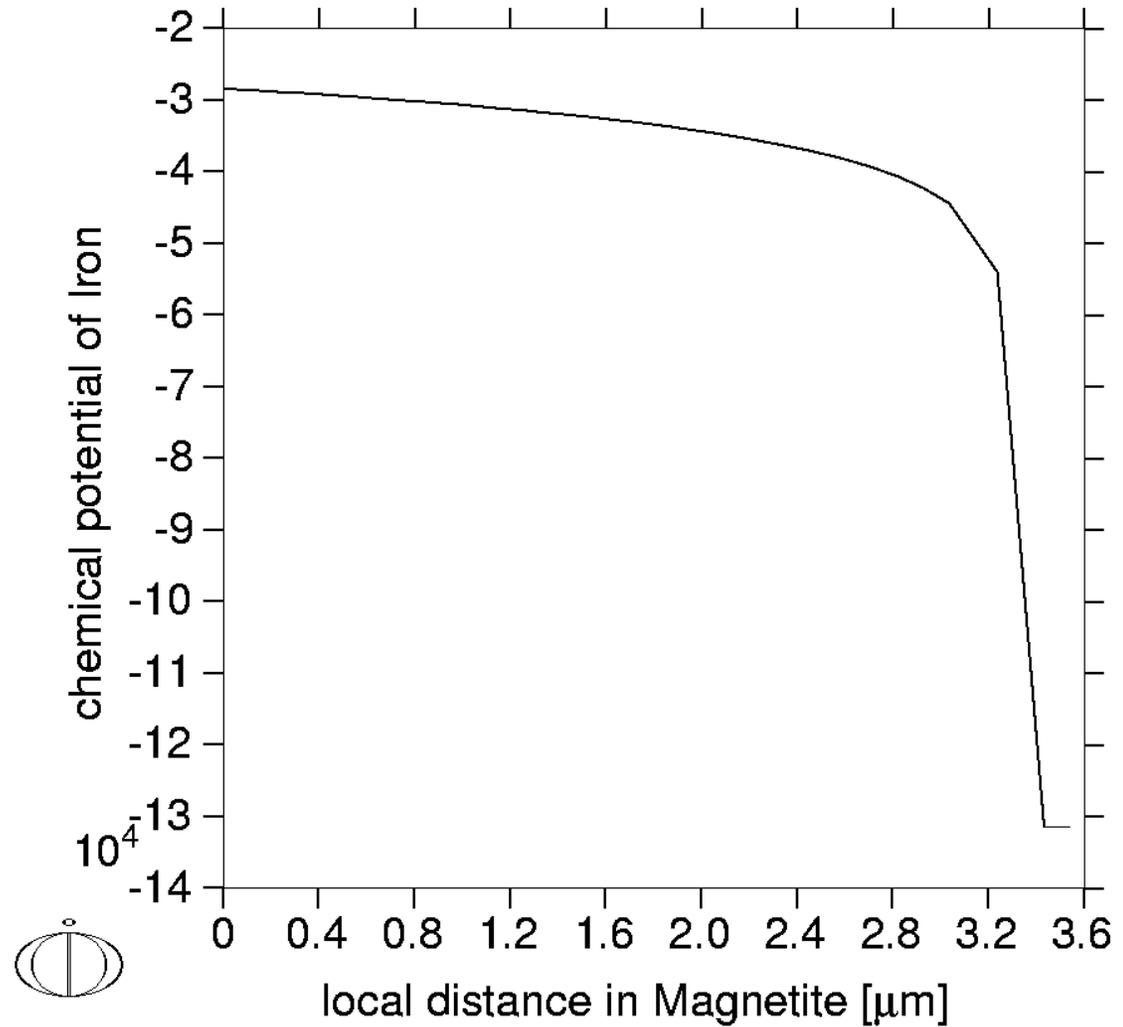


Interface Fe

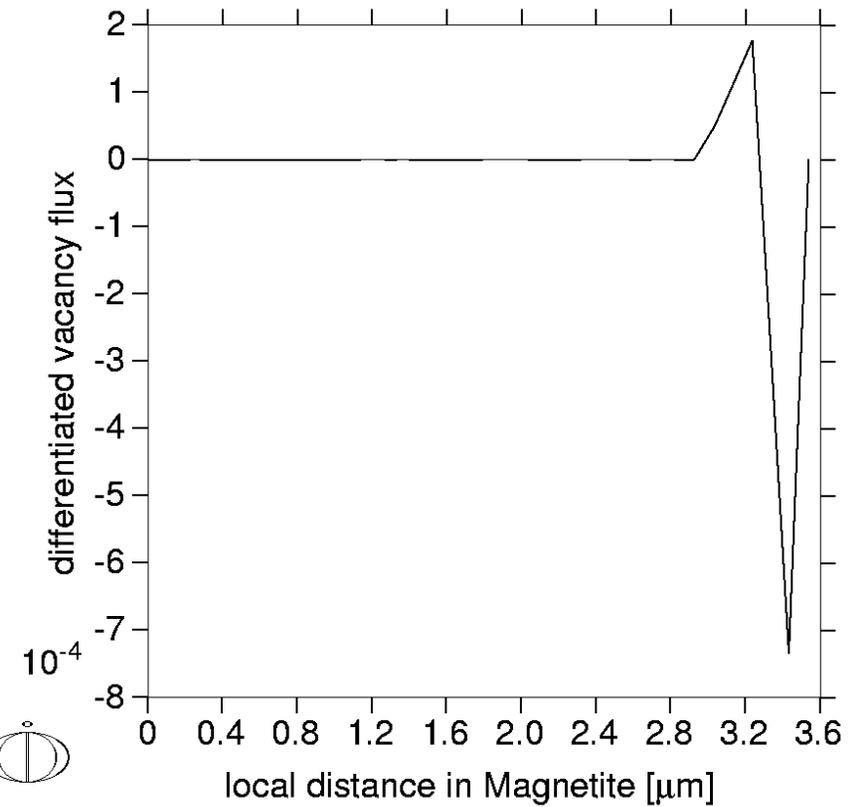
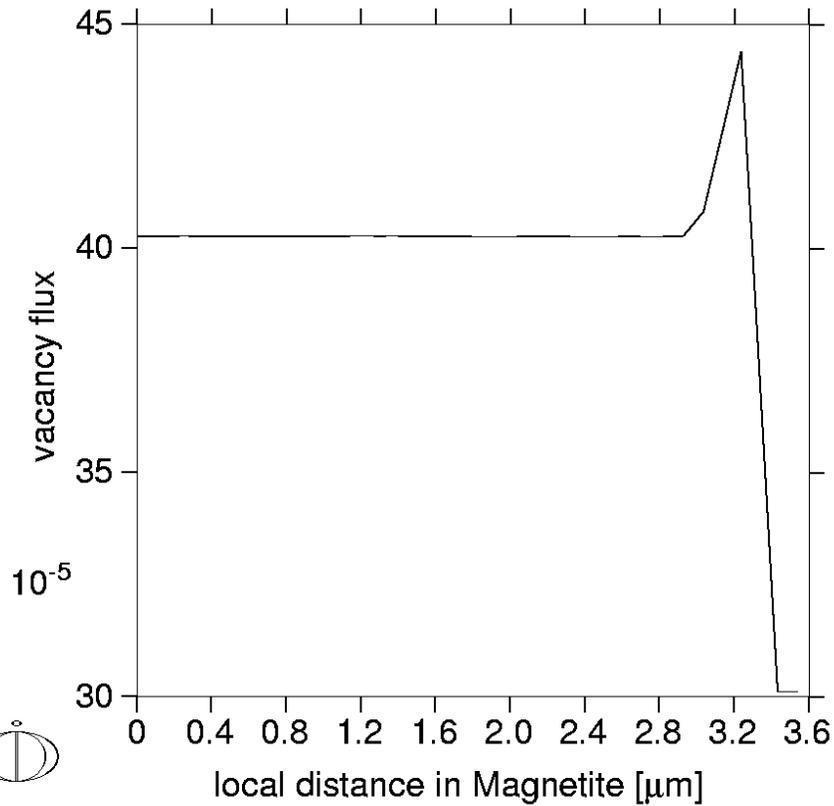
Interface hematite



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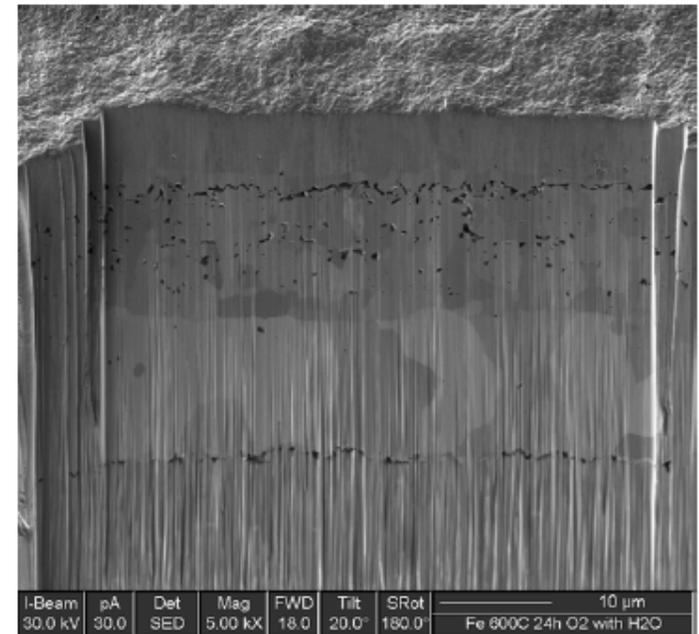
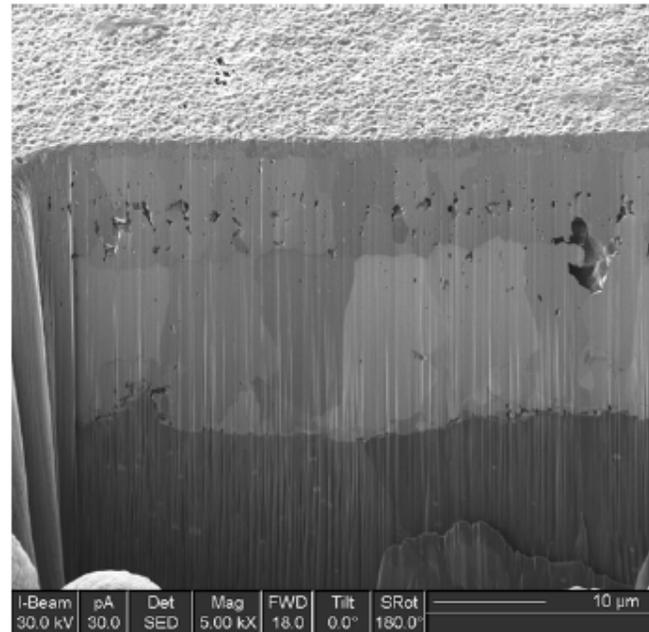
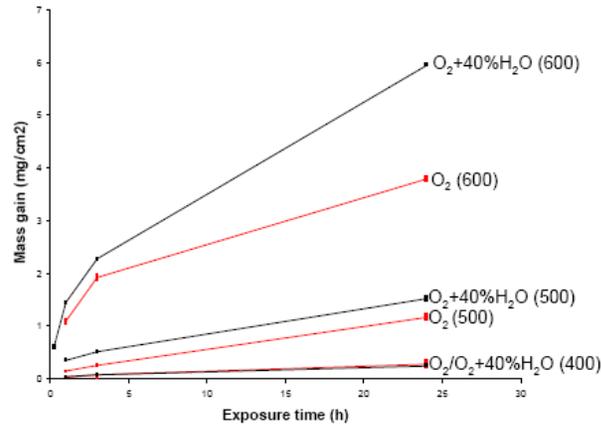


The steam effect in oxidation of Fe

600°C O₂ 24h

600°C O₂+H₂O 24h

Iron





- Dry atmosphere:
 - Inward growth of magnetite about 20-30 % of magnetite thickness.
 - Some porosity adjacent to the original steel surface
- Wet atmosphere:
 - Hematite layer much thicker due to much stronger outward growth (ca 50% of magnetite layer).
 - No porosity in hematite layer
 - High porosity in the inward growing magnetite layer.
 - Porosity at wustite/metal interface

The observations indicate that outward iron diffusion in hematite is accelerated by the steam.



Summary

- DICTRA can now handle diffusion in oxides allowing prediction of oxidation.
- Oxide mobilities in Fe-Cr oxides being assessed.
- Grain boundary diffusion is taken into account in a simplified manner.
- Oxygen diffusion may cause Kirkendall effect and porosity.