

Experimental Investigation on Geometric Parameters of S-type Pitot tube for GHGs Emission monitoring

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Contents

- I** **Korea GHGs Emission Monitoring**

- II** **S-type Pitot tube in Smokestack**
- III** **Research objective**
- IV** **Experimental results in KRISS**
- V** **Conclusion**

Korea GHG Inventory

- High proportion (90%) of greenhouse gas emissions arising from the energy and industrial fields such as heavy / petrochemical / semiconductor and power plant

Greenhouse Gas

CO₂

Carbon dioxide

- Industry, transportation,
use of energy
(coal and oil)

SF₆

Hexafluoride

- Insulators

PFC_s

Perfluorocarbon

- Semiconductors
(inert liquids for cleaning)

HFC_s

Hydrofluorocarbons

- Refrigerants used in air
conditioning systems

N₂O

Nitrogen dioxide

- Industrial processes
and use of fertilizers

CH₄

Methane

- Waste, agriculture
and livestock

KEPCO
E&C

SAMSUNG

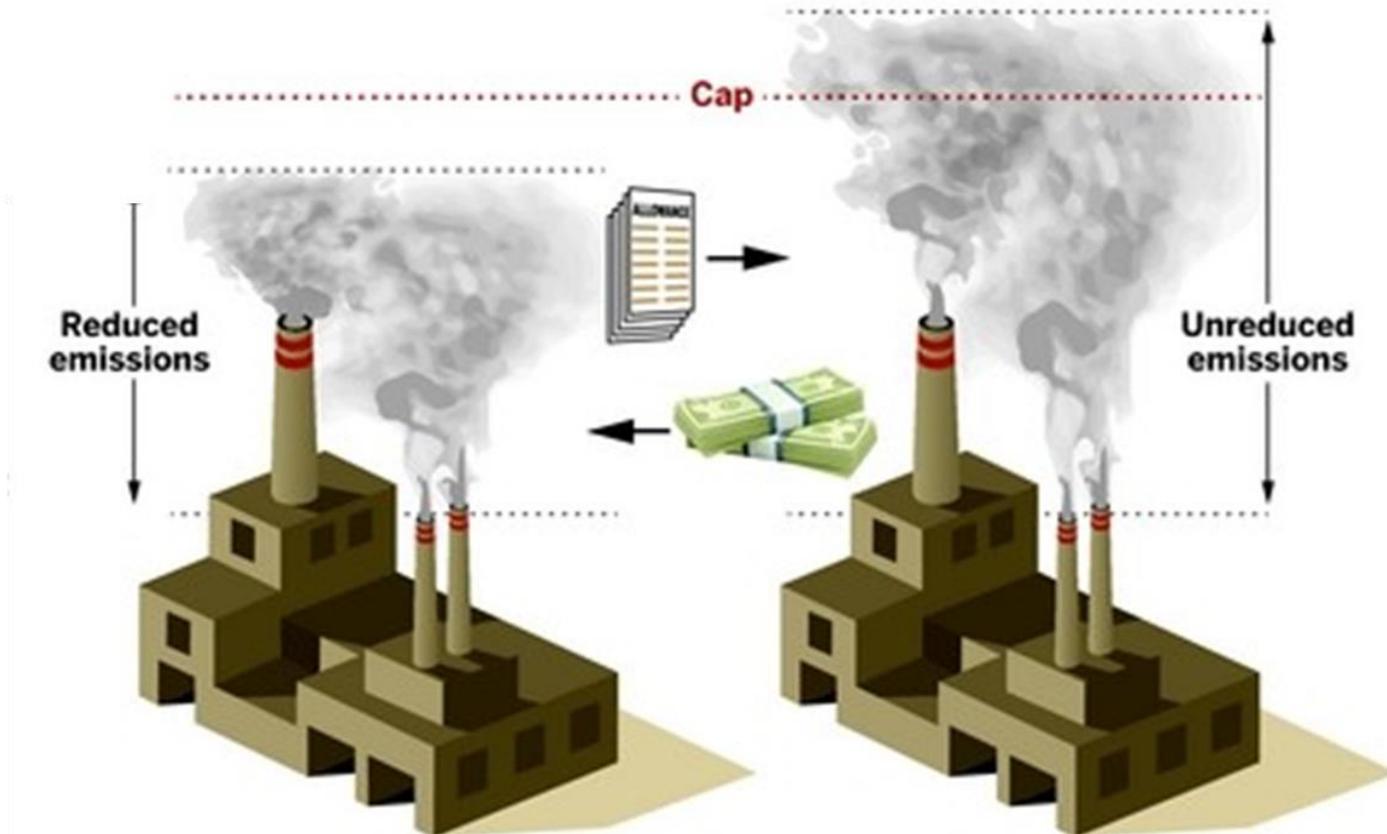
POSCO

HYUNDAI
STEEL

LG Display

Korea Emission Trading Scheme

- Implementation with allocation of emission cap for each company in 2015
- To meet the cap of emissions, company with increasing emissions should buy emission allowance from other emission-reduced company



Estimation method of GHG emissions in KOREA

Activity-based method

$$E = FC \times EF$$

E : estimated emission (kg)

FC : fuel consumption (TJ)

EF : emission factor (kg/TJ)

**Fuel consumption (Tier 1)
by IPCC guidelines**



$$E = FM \times CC \times \frac{M_{CO_2}}{M_C}$$

CC : fuel carbon content(kg/kg)

M_{CO_2} : molecular mass of carbon dioxide

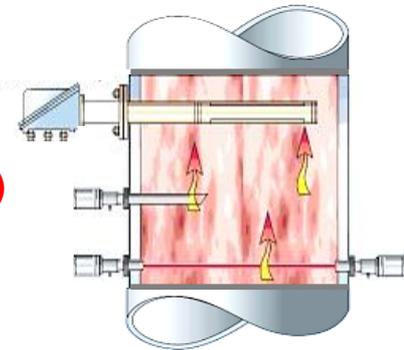
M_C : atomic mass of carbon

**Carbon content (Tier 3)
by IPCC guidelines**

Continuous emission measurement(CEM)

$$E_{CEM} = \sum_{i=1}^N E_{5min,i} = \sum_{i=1}^N \left(K \times \bar{C}_i \times Q_{5min,i} \times \frac{MW_{gas}}{22.4L} \right)$$

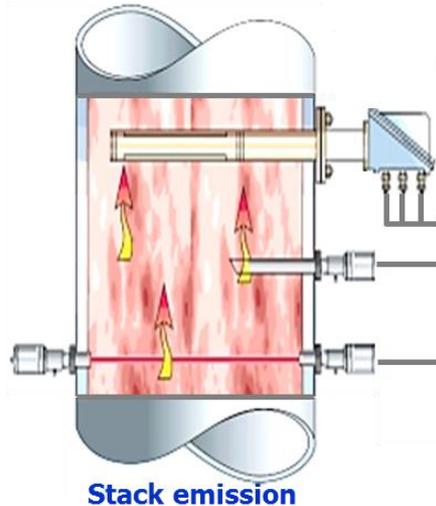
**CEMS (Tier 4)
by EPA**



- Depending on combustion source and unit size, facilities can select estimate methods, but CEMs is **not Mandatory** in the Environ. Law of Korea

Smoke Stack Tele-Monitoring System(TMS)

On-site Measurement



- Total Suspended Particle
- NO_x, SO₂, O₂ Concentration
- Flow rate
- Temperature

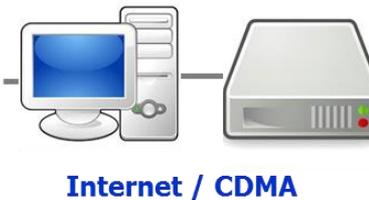
Analyzer Control Unit



Tele-metering system(TMS)



Local Area Network



- National Ambient Air Monitoring System operated by Ministry of S. Korea
- Measure and monitor the pollutant items(SOX, NOX,..)and non-pollutant item(Temp., Flow rate and O₂) from large-scale emission facilities

Contents

I Korea GHGs Emission Monitoring

II **S-type Pitot tube in Smokestack**

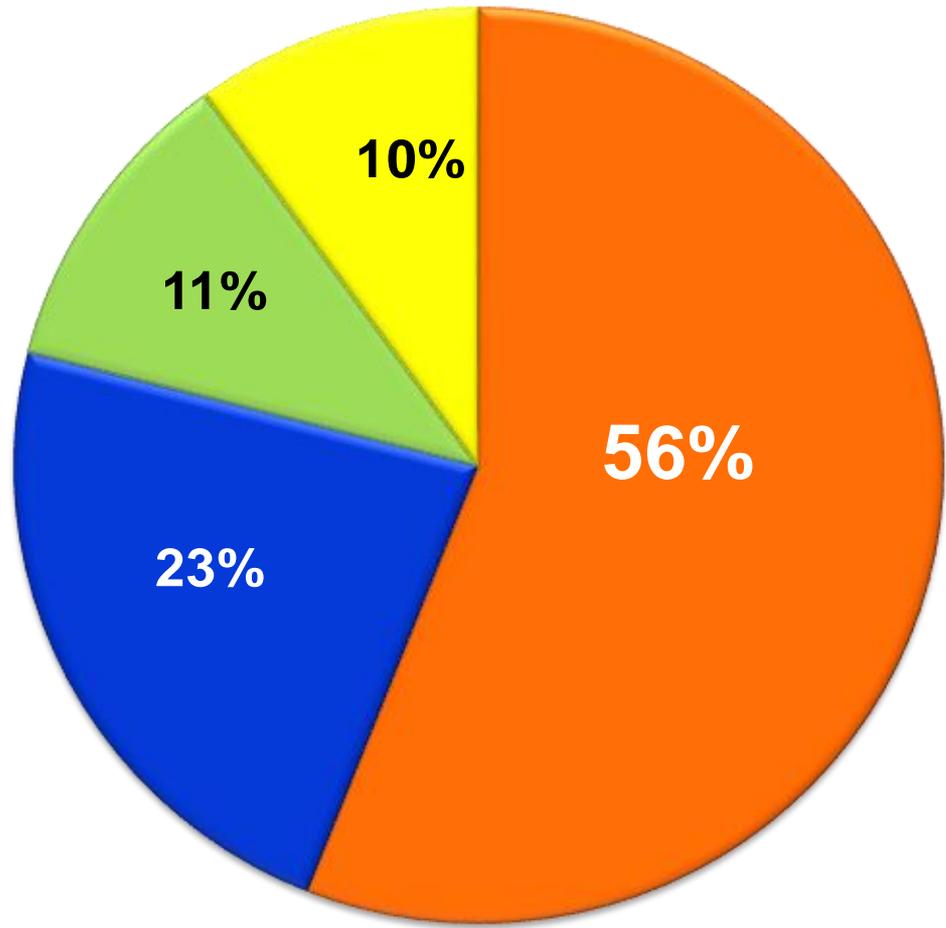


III Research Objective

IV Experimental results in KRISS

V Conclusion

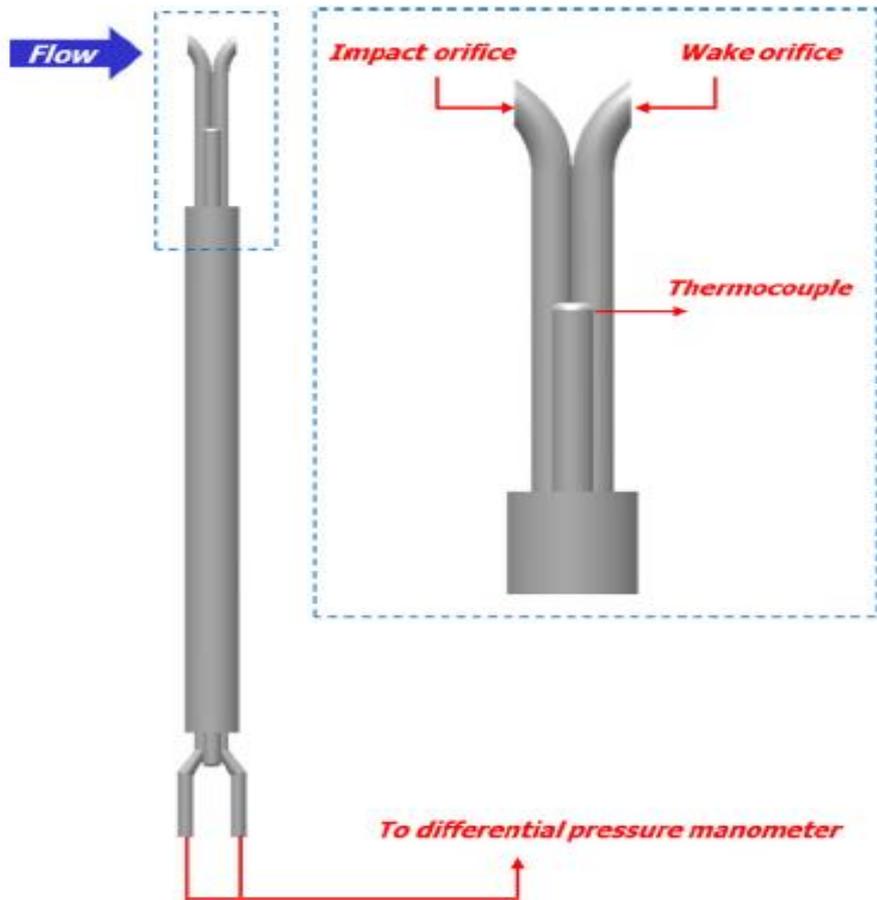
Instruments for Stack Flow Velocity in KOREA



- S-type Pitot tubes
- Thermal flowmeter
- Ultrasonic flowmeter
- Averaging Pitot tubes

S-Type Pitot tube

- Large pressure orifices($\Phi=5\sim 10\text{mm}$) & Strong tubes for high dust environments like industry stack (ISO 10780, KS M9429, EPA method2)
- Measurement differential pressure between an impact(total pressure) and wake orifice(static pressure) based on Bernoulli equation



$$V = C_{P,S} \sqrt{\frac{2\Delta P}{\rho}}$$

V : flow velocity in the stack gas(m/s)

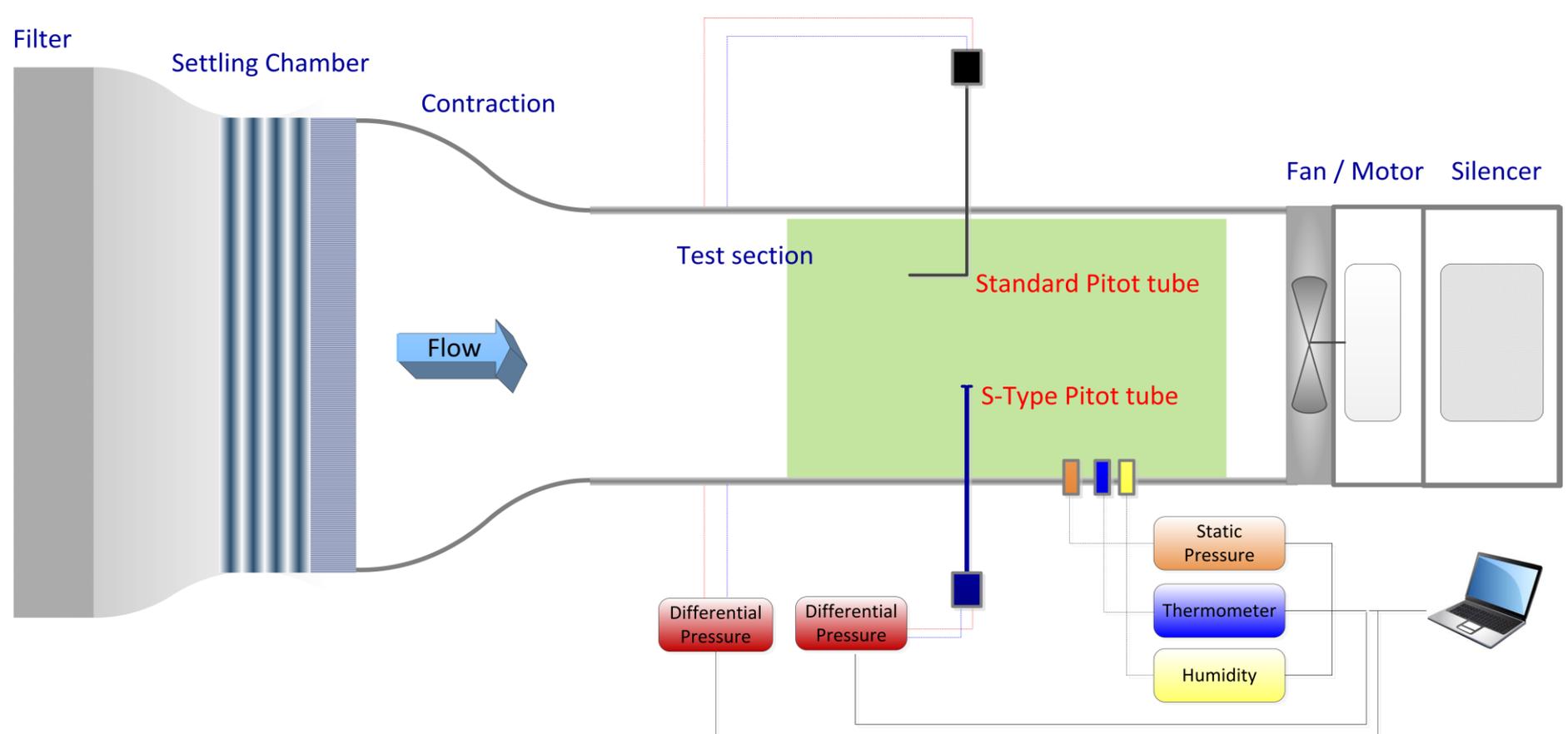
$C_{P,S}$: S type Pitot tube coefficient

ΔP : differential pressure between
impact and wake orifice (Pa)

ρ : density of the stack gas (kg/m^3)

Calibration for S Pitot Tube Coefficient (C_p)

- Calibration against L-type Pitot tube in the wind tunnel of the national metrology institute or the accredited calibration laboratories.



Calibration for S Pitot Tube Coefficient (C_p)

- Determination by comparing the differential pressure of standard pitot tube and S-type Pitot tube

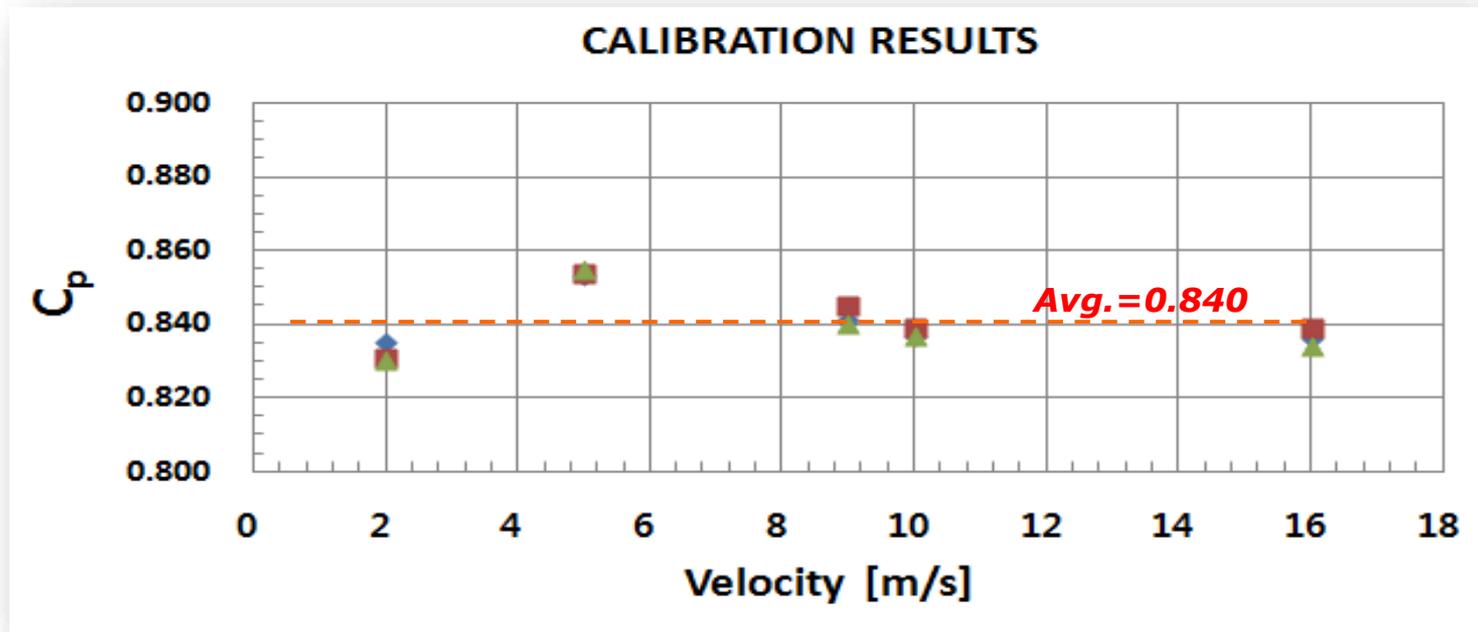
$$C_{P,S\text{-type}} = C_{P,Std} \left(\frac{\Delta P_{Std}}{\Delta P_{S\text{-type}}} \right)$$

$C_{p,s\text{-type}}$: S-type Pitot tube coefficient

$C_{p,std}$: Standard Pitot tube coefficient

$\Delta P_{s\text{-type}}$: differential pressure of S-type Pitot tube

ΔP_{std} : differential pressure of Standard tube



On-site Measurement

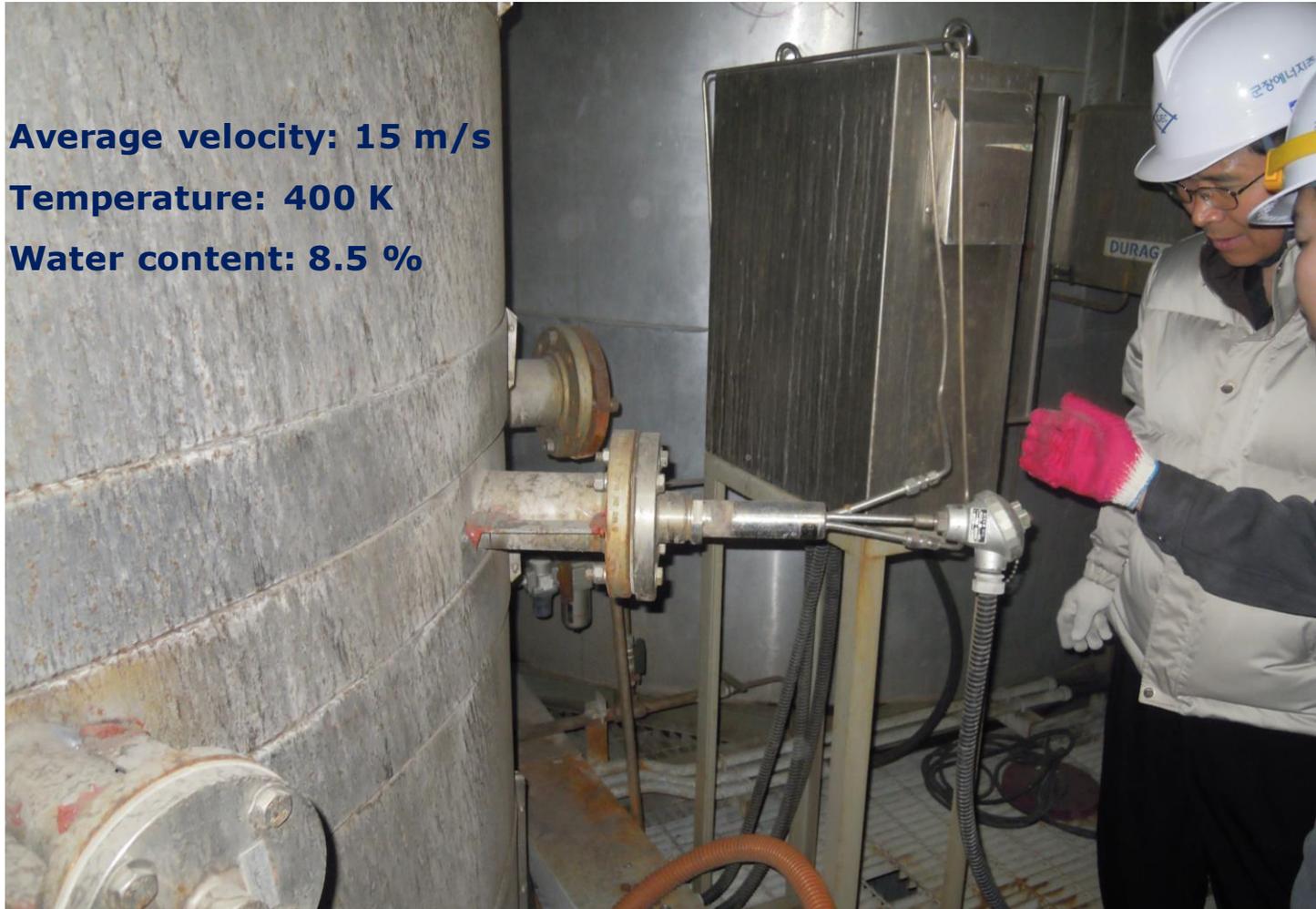


*Combined Heat and Power Plant
Guhjang Energy, KOREA*

On-site Measurement

- S-type Pitot tube is usually installed and inserted in harsh environment such as tall stack height and high gas temperature

Average velocity: 15 m/s
Temperature: 400 K
Water content: 8.5 %



On-site Measurement

- Difficult to observe the inside of the stack and verify the precise installation of the S-type Pitot tube

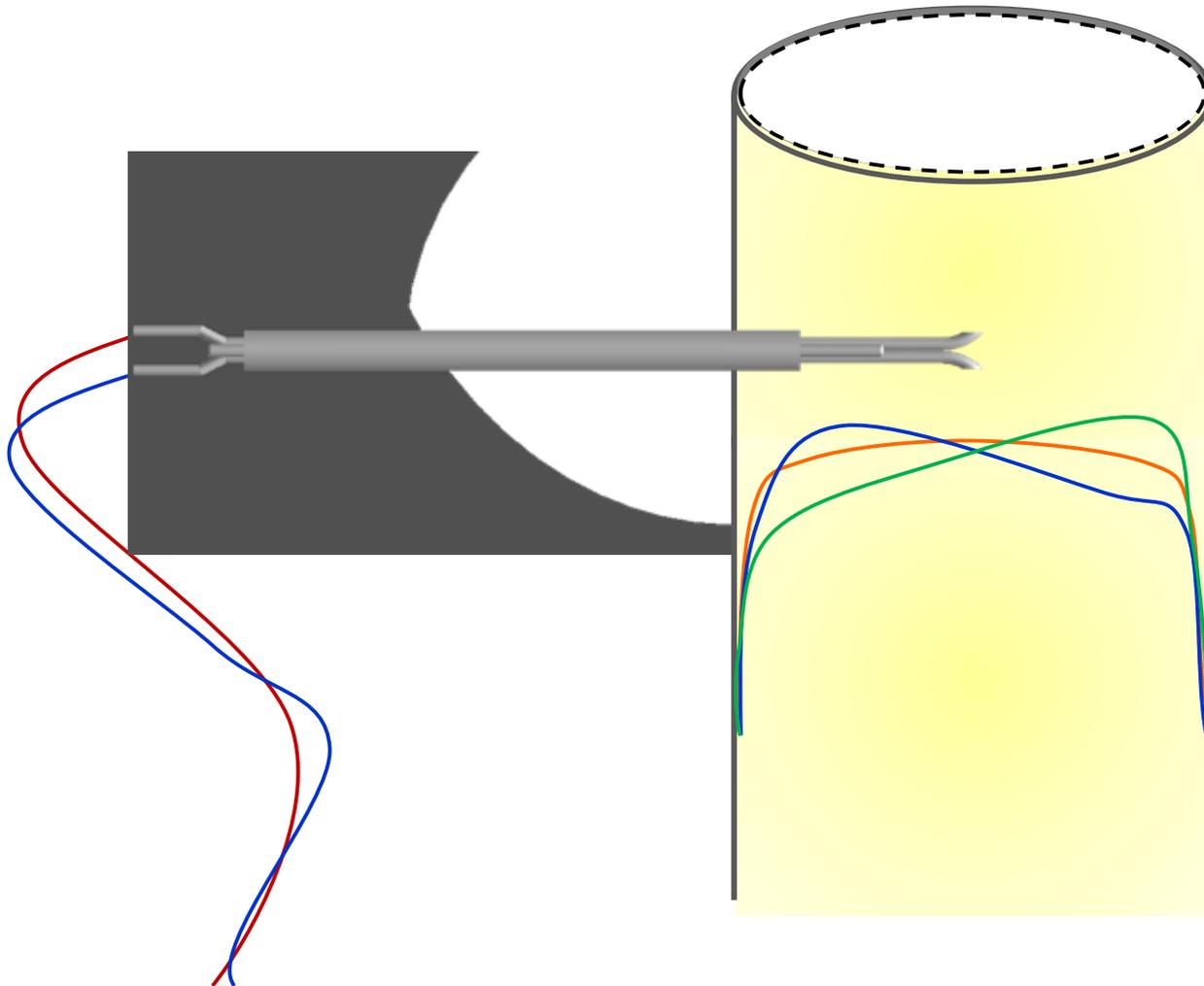


What Happens Inside the Stack?



What Happens Inside the Stack?

- Flow velocity of emission gas can be altered due to the unstable process in particular industrial condition of plant

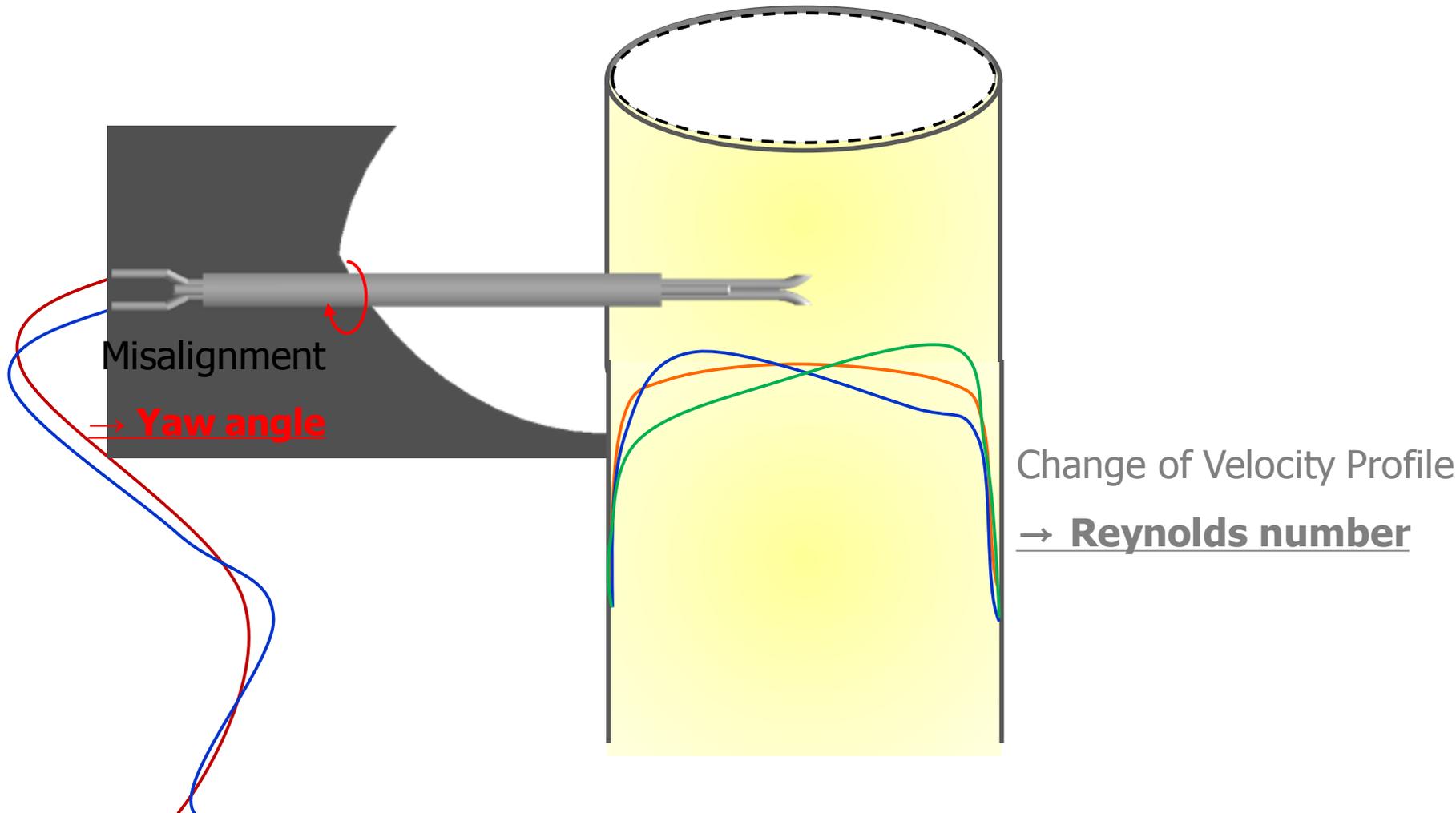


Change of Velocity Profile

→ **Reynolds number**

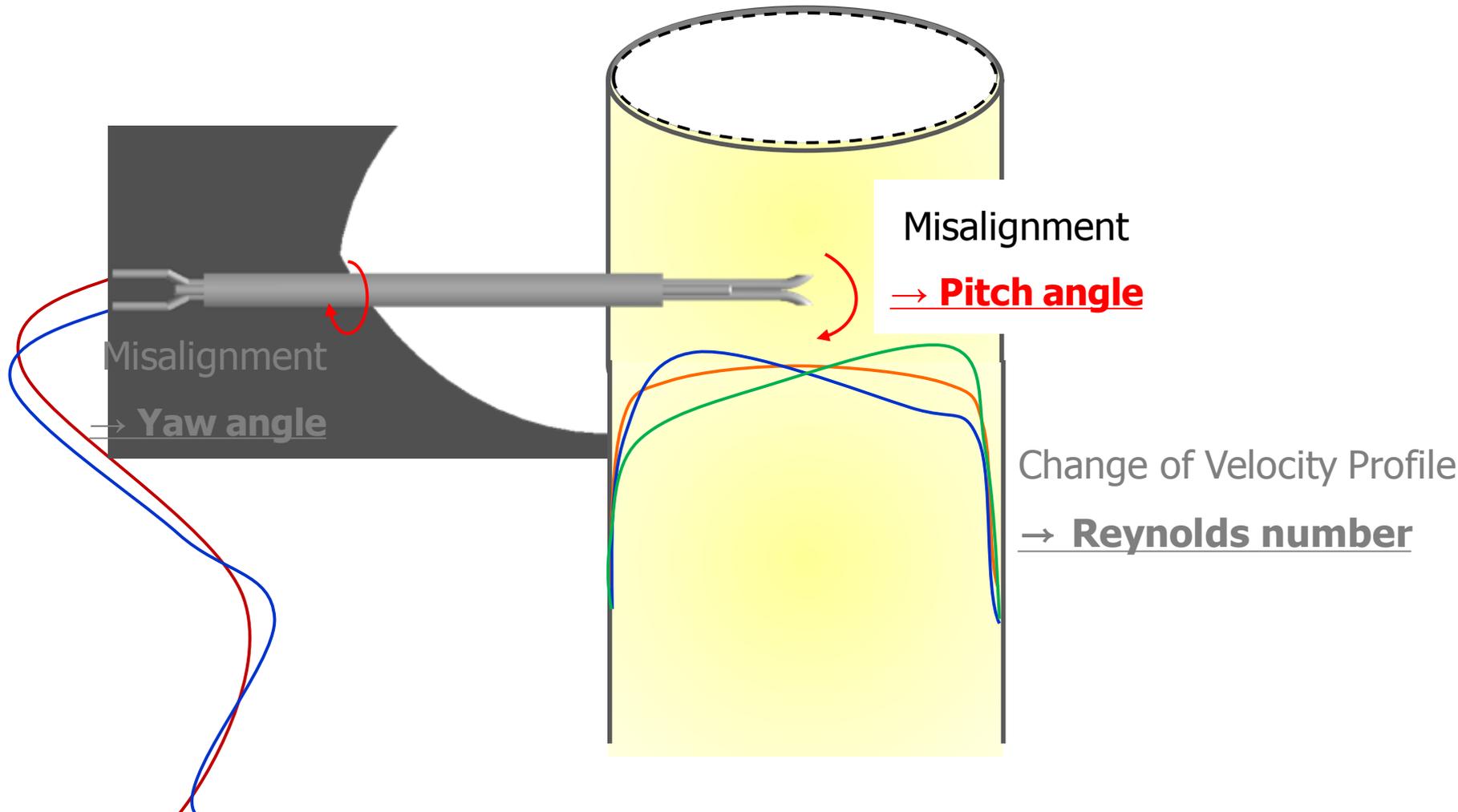
What Happens Inside the Stack?

- Yaw angle misalignment can occur during installation of S-type Pitot tube from outside of the stack due to the difficulty of observation



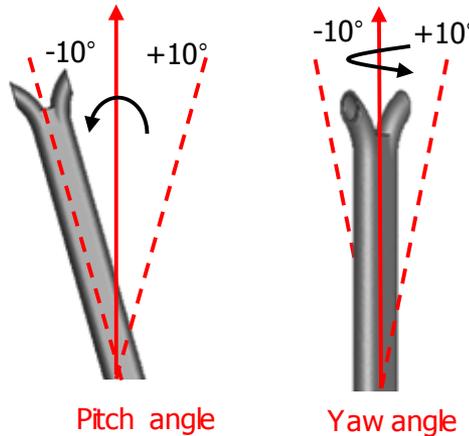
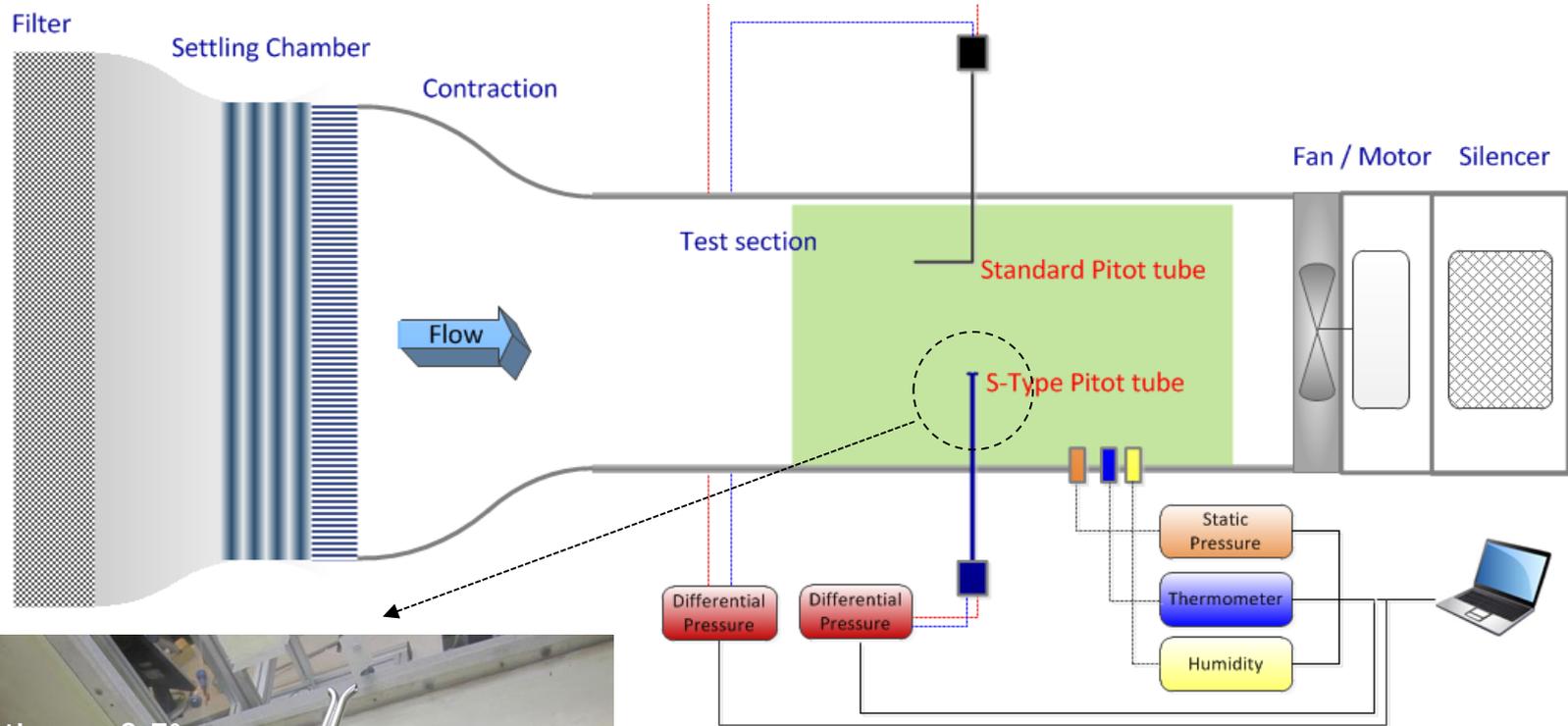
What Happens Inside the Stack?

- Pitch angle misalignment of S-type Pitot tube can result due to the deflection of the long S-type Pitot tube in large diameter stacks.



Experimental Studies (2015)

- Flow Measurement and Instrumentation, Kang et al. 2015

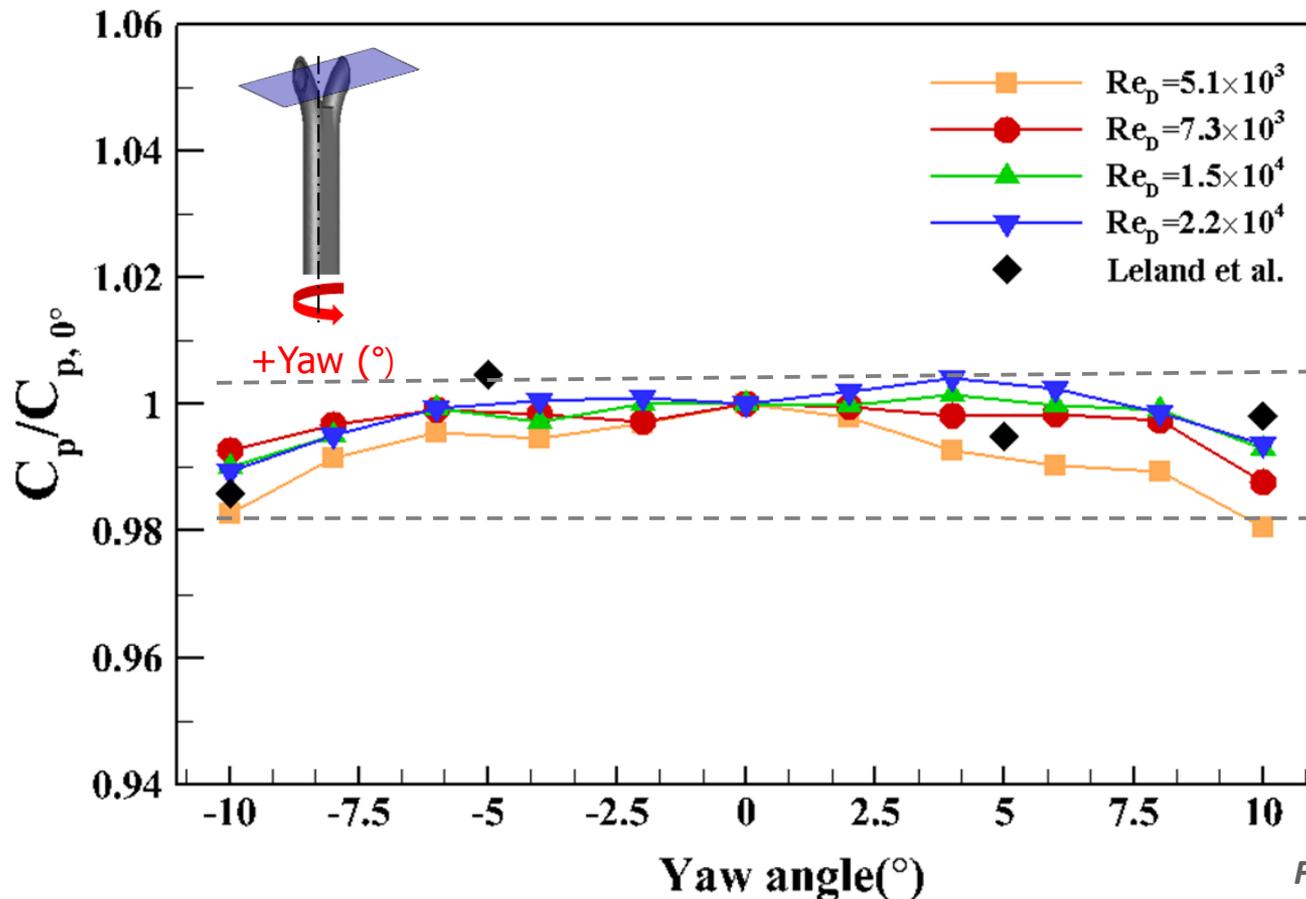


KRISS Subsonic Wind Tunnel	
Wind tunnel Type	Open-Suction type
Velocity range	2 m/s to 15 m/s
Test section area	0.9 m X 0.9 m
Uncertainty (%)	0.60 % to 1.1%

The effects of Yaw angle misalignment

The effects of Yaw angle misalignment

- S-type Pitot tube coefficients (C_p) at each yaw angle are normalized by S-type Pitot tube coefficients ($C_{p,0^\circ}$) at a yaw angle of 0°
- The normalized S-type Pitot tube coefficients decreased by up to -2% as the yaw angle increases to $\pm 10^\circ$ with symmetric tendency

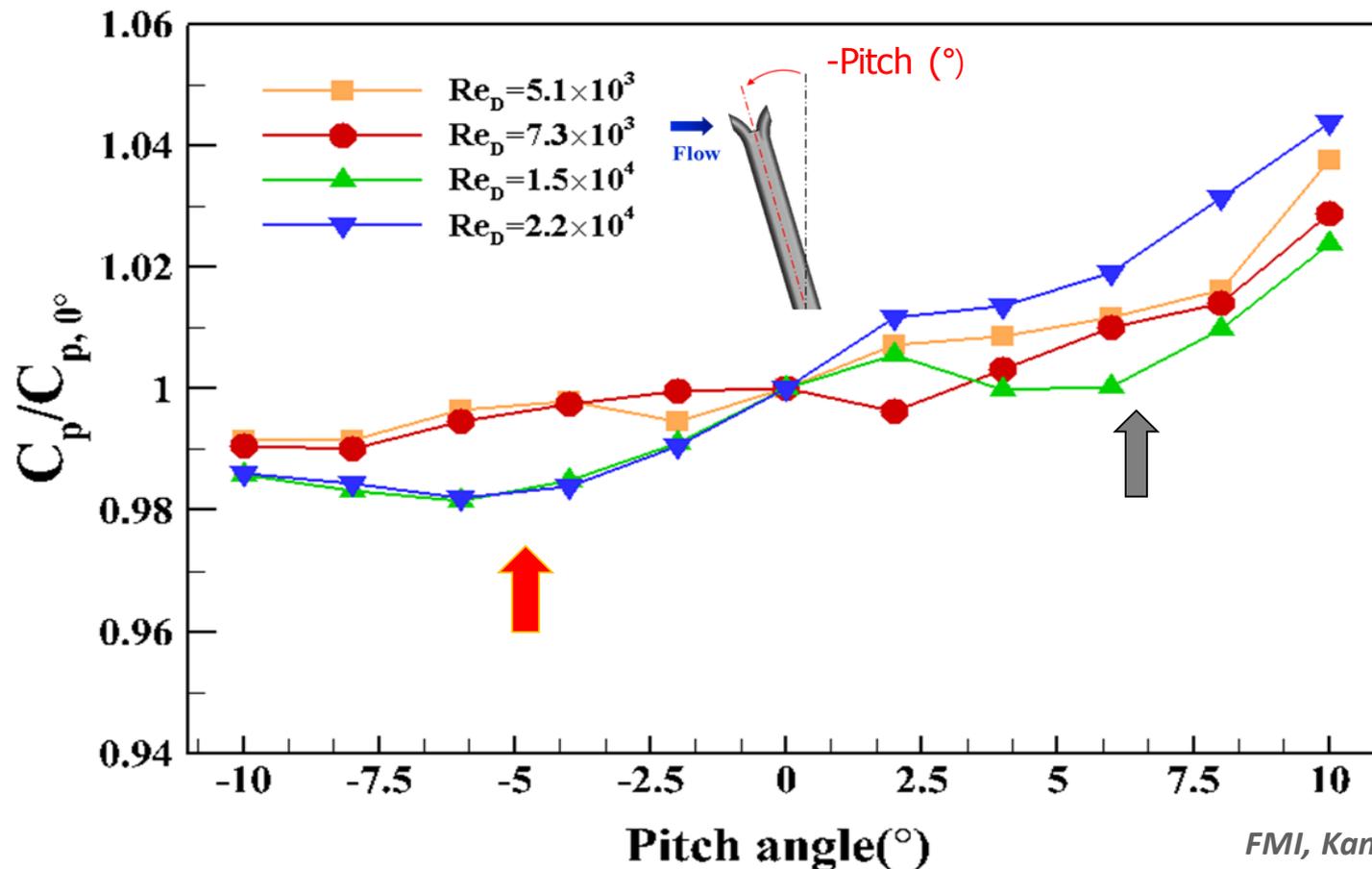


FMI, Kang et al. 2015

The effects of Pitch angle misalignment

The effects of Pitch angle misalignment

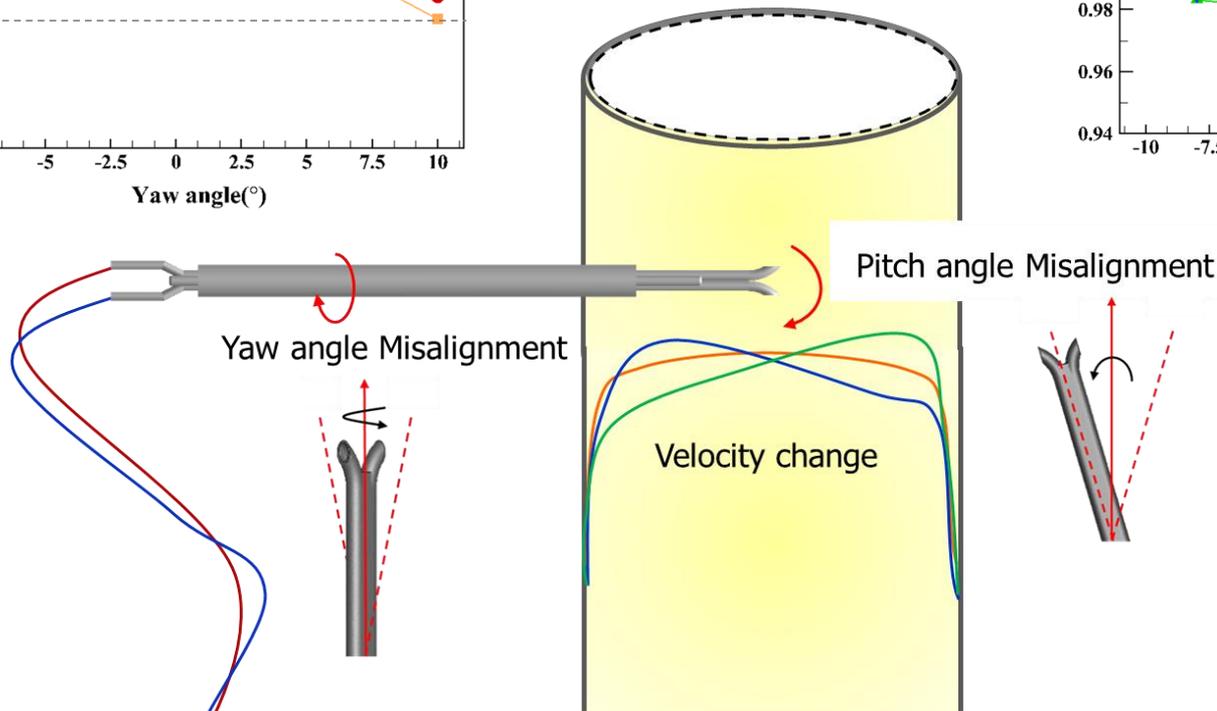
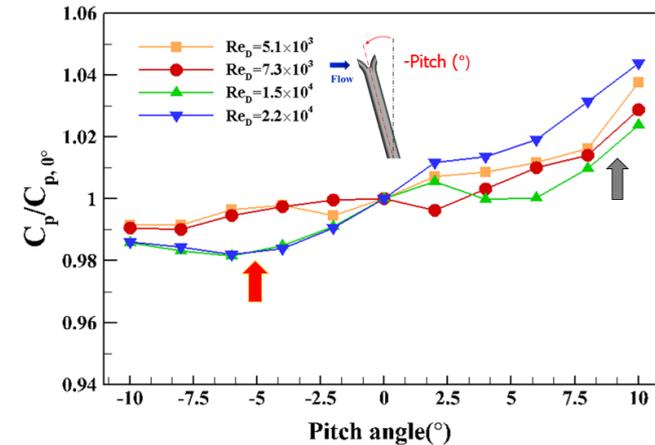
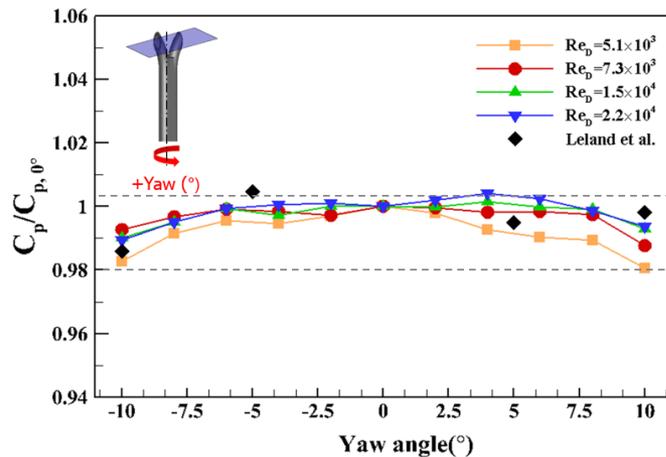
- The normalized S-type Pitot tube coefficients increase up to 4 % as the pitch angle increases to $+10^\circ$
- In negative Pitch angles, S-type Pitot coefficients decrease to -2% , which can occur in industry stacks due to deflection of long S type Pitot tube



FMI, Kang et al. 2015

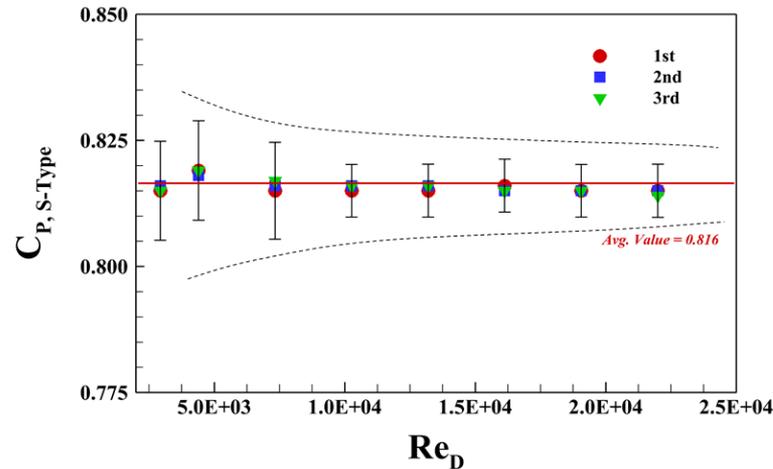
S-type Tube for Smokestack

- When S-type Pitot tube install in the stack, there could be yaw, pitch angle misalignment and velocity change.
- But, **one average calibration coefficient** of S-type Pitot tube was used.

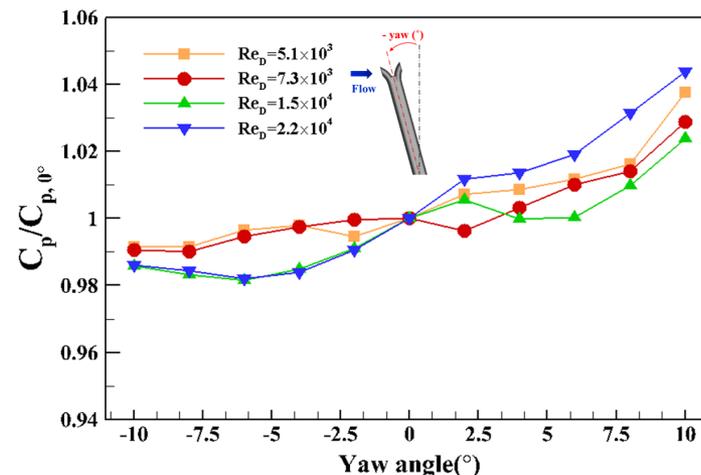
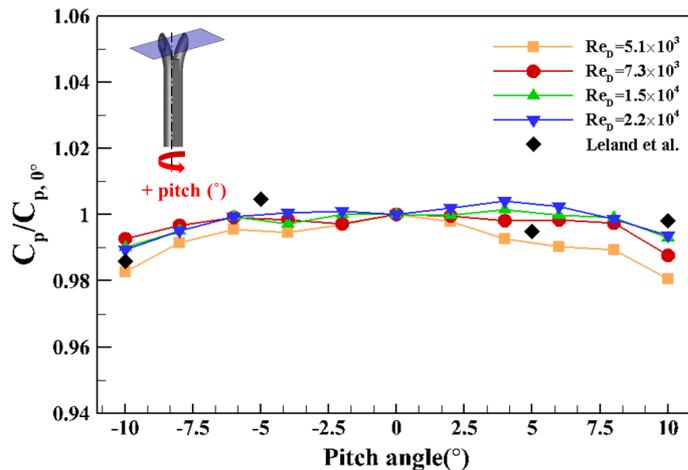


What is **Ideal** S-Type Pitot tube ?

- **Linearity, Repeatability** of S-type Pitot tube coefficient in the used range of Reynolds number



- **Less (more) sensitivity** to the effect of yaw and pitch angle misalignment



Standardization of S-Type Pitot tube

INTERNATIONAL
STANDARD

**ISO
10780**

First edition
1994-11-15

**Stationary source emissions —
Measurement of velocity and volume
flowrate of gas streams in ducts**

*Émissions de sources fixes — Mesurage de la vitesse et du débit-volume
des courants gazeux dans des conduites*



Designation: D3796 – 09

**Standard Practice for
Calibration of Type S Pitot Tubes¹**



Method 2—Determination of Stack Gas Velocity and Volumetric Flow Rate (Type S Pitot Tube)

Recommended Configuration of S Pitot tube



International
Organization for
Standardization



ISO 10780

External diameter of leg (D)
: 4 mm to 10 mm

Distance between the base of
each leg of the Pitot tube and
its face-opening plane
: $1.05D \leq L \leq 10D$

This distance shall be equal
for each leg

ASTM D3796(Ref. 1)

Bending a 45° angle on the
end of 0.95 cm stainless steel
tube

The Pitot tube's length
: $0.6 \text{ m} \leq PL \leq 3.0 \text{ m}$

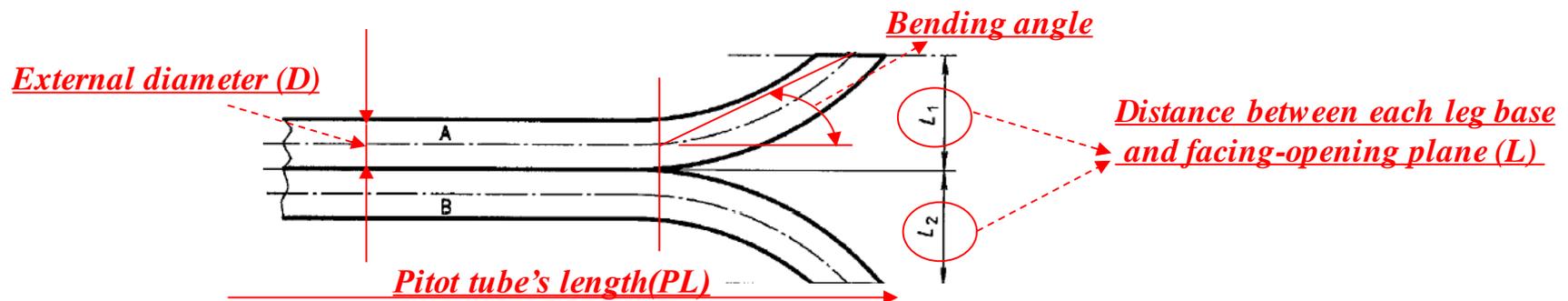
Cutting is parallel to the main
body of the tube

EPA

External diameter of leg (D)
: 4.8 mm to 9.5 mm

Distance between the base of
each leg of the Pitot tube and
its face-opening plane
: $1.05D \leq L \leq 1.50D$

This distance shall be equal
for each leg



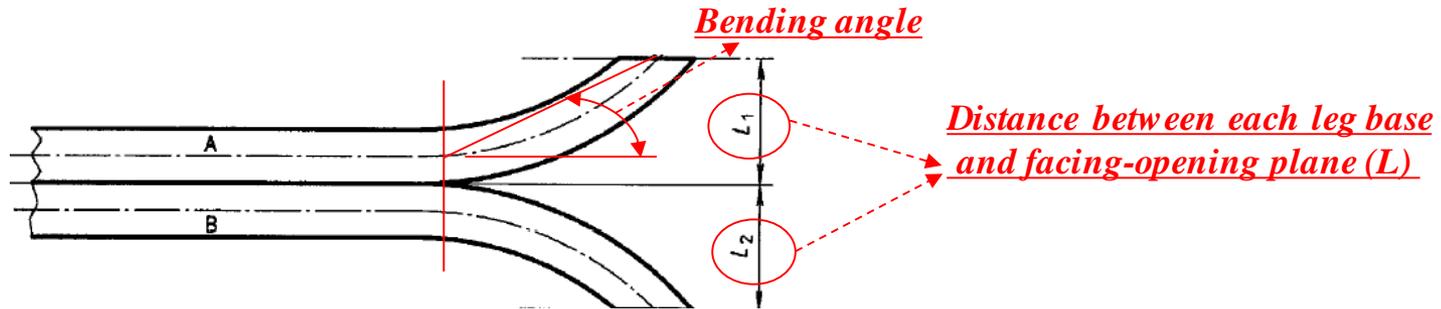
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Research objective

- Evaluate the effect of various geometries of S-type Pitot tube on the S-type Pitot tube coefficients including the sensitivity to velocity change, pitch and yaw angle misalignments



1. Distance between leg base and facing-opening plane (L)

- ISO: $1.05D \leq L \leq 10D$, EPA: $1.05D \leq L \leq 1.5D$

2. Bending Angle of opening parts (α)

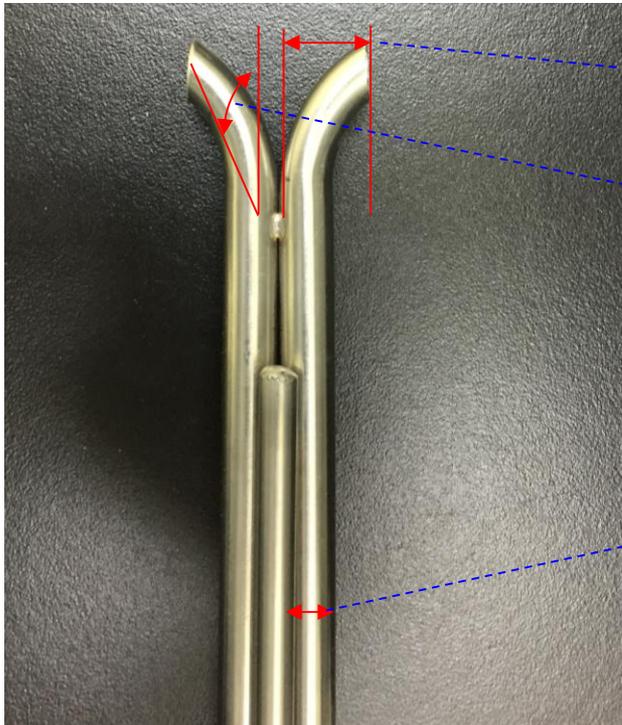
- ASTM: 45° (KRISS S Pitot tube = 30°)

3. Shape of opening parts

- Curved / Straight

Configuration of S-type Pitot tube

- S-type Pitot tube KRISS used



Distance between each leg base and facing-opening plane (L)

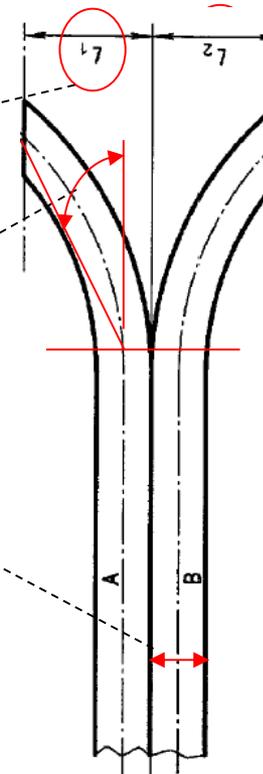
→ $L = 1.6D$

Bending angle

→ $\alpha = 30^\circ$

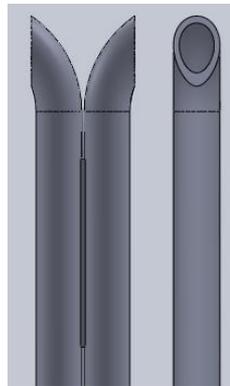
External diameter (D)

→ $D = 9.5 \text{ mm}$

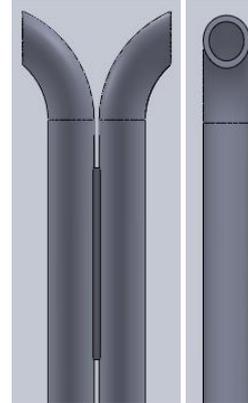


Configuration of S-type Pitot tube

- S-type Pitot tube KRISS used



$L = 1.05D, \alpha = 30^\circ$



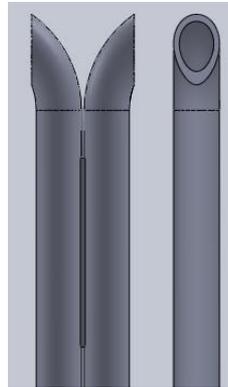
$L = 1.6D, \alpha = 30^\circ$



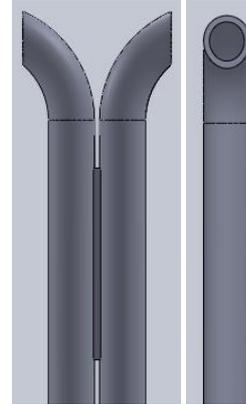
$L = 3D, \alpha = 30^\circ$

S-type Pitot tube Manufacturing

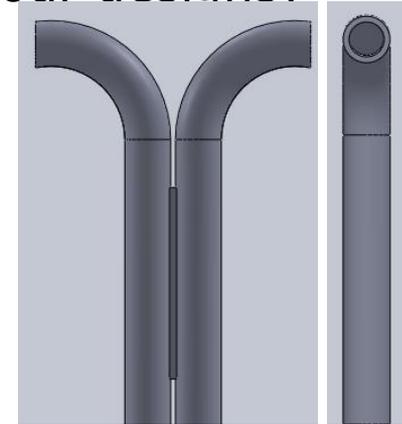
- How to manufacture S-type Pitot tube model for our designs?



$L = 1.05D, \alpha = 30^\circ$



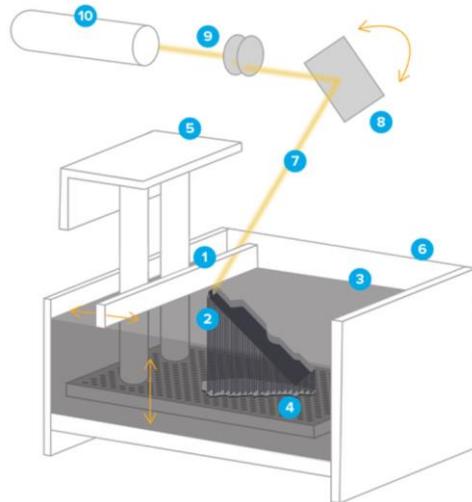
$L = 1.6D, \alpha = 30^\circ$



$L = 3D, \alpha = 30^\circ$

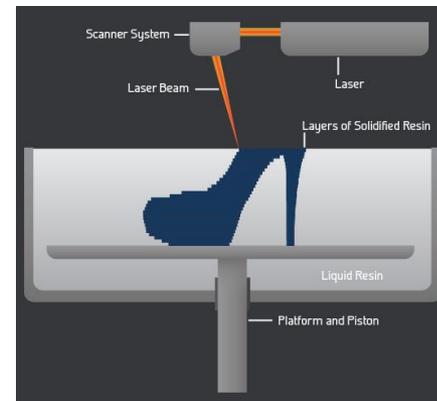
- 3D Printing (SLA, Stereolithography)

- focusing an ultraviolet (UV) laser on to a vat of photopolymer resin with elevator



Right-Side Up SLA

- 1 Sweeper
- 2 Printed Part
- 3 Resin
- 4 Build Platform
- 5 Elevator
- 6 Resin Tank
- 7 Laser Beam
- 8 X-Y Scanning Mirror
- 9 Lenses
- 10 UV Laser

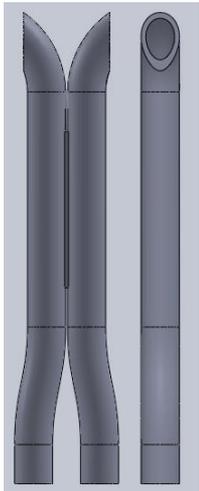
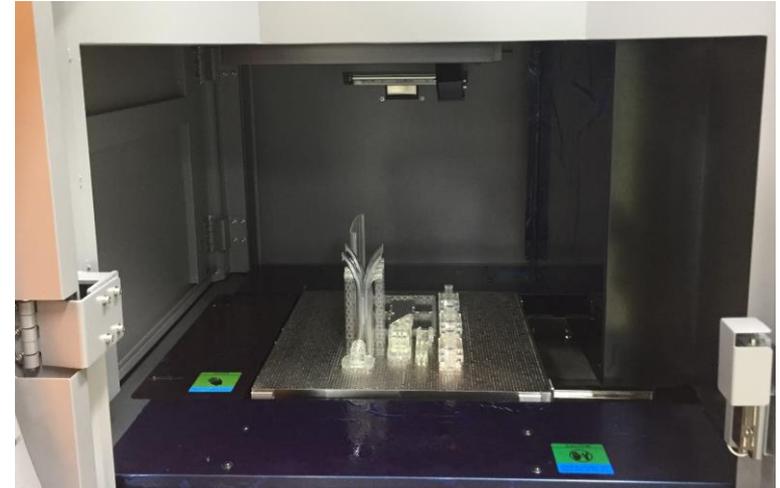


3D Printing for S-type Pitot tube

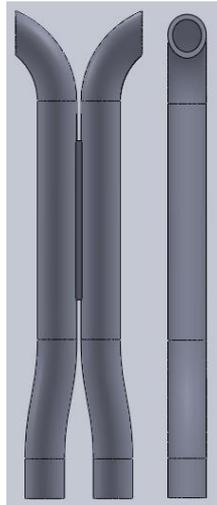
- 3D Printing S-type Pitot tube for our design(Daejeon Techno-park)



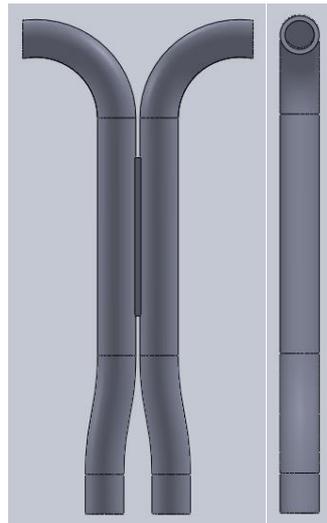
Model	ATOMm-4000
Equipped Laser	Solid state laser 400mW 40KHz
Scanning Method	Digital (TSS4)
Laser Warranty Period	1 year
Maximum Scanning Speed	30,000mm/sec
Laser Diameter	0.10 - 0.60mm (automatically changeable)
Maximum Model Size	400×400×300mm
Z Table	Minimum layer pitch 25μm *depends on the resin used
Recoater	Blade recoater
Resin Surface Control	Balloon
Power Supply	AC100V×1 Single phase 15A
Equipment Dimension	Approx.W1565×D1050×H1860mm
Equipment Weight	Approx.550kg (not including resin)
Software	C-Sirius
PC OS	Windows 7
Operation	English/ Japanese



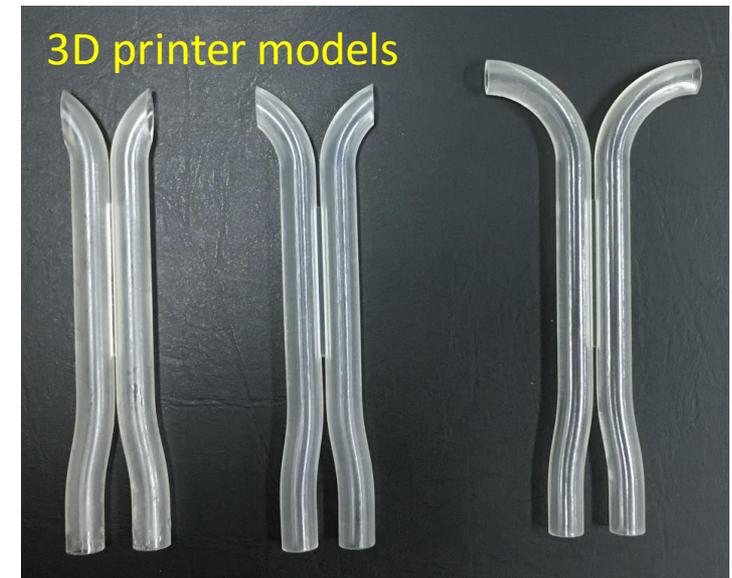
$L = 1.05D, \alpha = 30^\circ$



$L = 1.6D, \alpha = 30^\circ$



$L = 3D, \alpha = 30^\circ$



Research objective

- Evaluate the effect of **various geometries of S-type Pitot tube** on the S-type Pitot tube coefficients including the sensitivity to **velocity change, pitch and yaw angle misalignments**

1. Distance between leg base and facing-opening plane (L)

- ISO: $1.05D \leq L \leq 10D$, EPA: $1.05D \leq L \leq 1.5D$

→ **L = 1.05D, 1.6D, 3D**

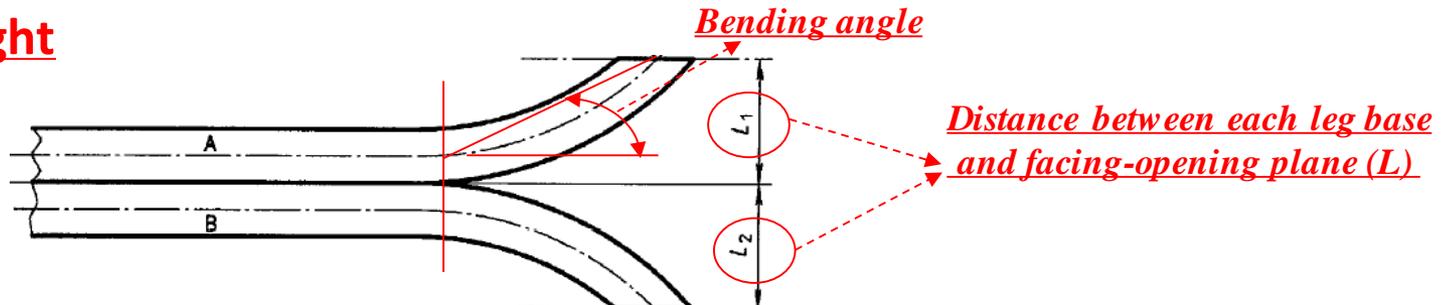
2. Bending Angle of opening parts

- ASTM: 45° (KRISS S Pitot = 30°)

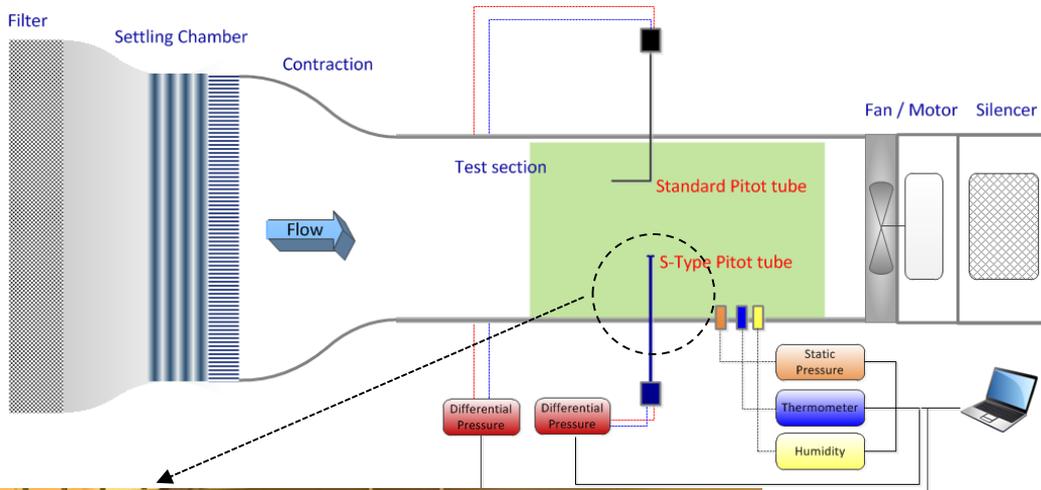
→ **$\alpha = 15^\circ, 30^\circ, 45^\circ$**

3. Shape of opening parts

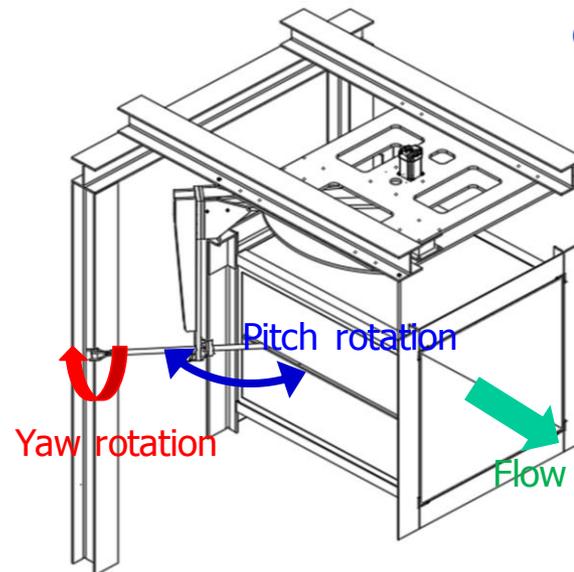
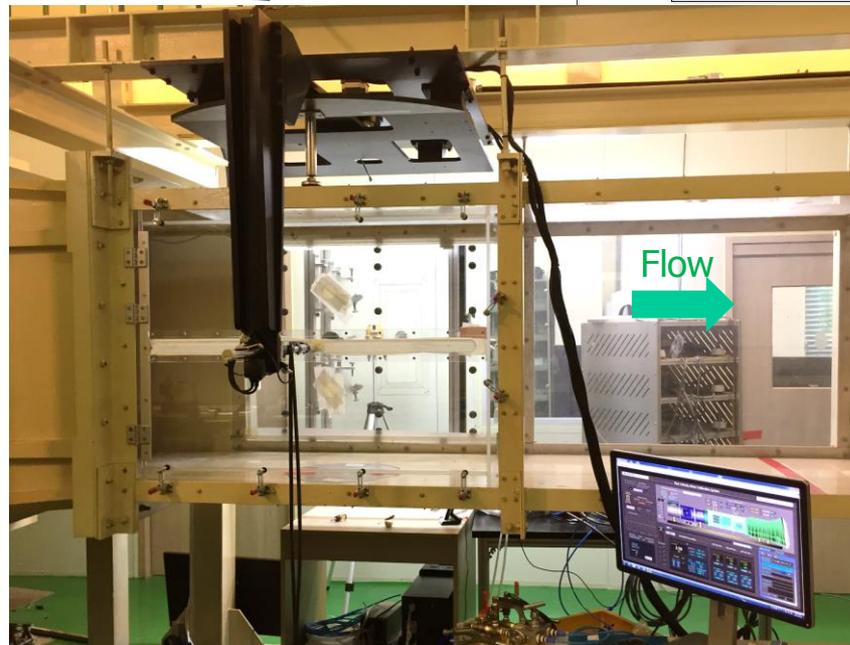
→ **Curved, Straight**



Windtunnel experiments



KRISS Subsonic Wind Tunnel	
Wind tunnel Type	Open-Suction type
Velocity range	2 m/s to 15 m/s
Test section area	0.9 m X 0.9 m
Uncertainty (%)	0.60 % to 1.1%

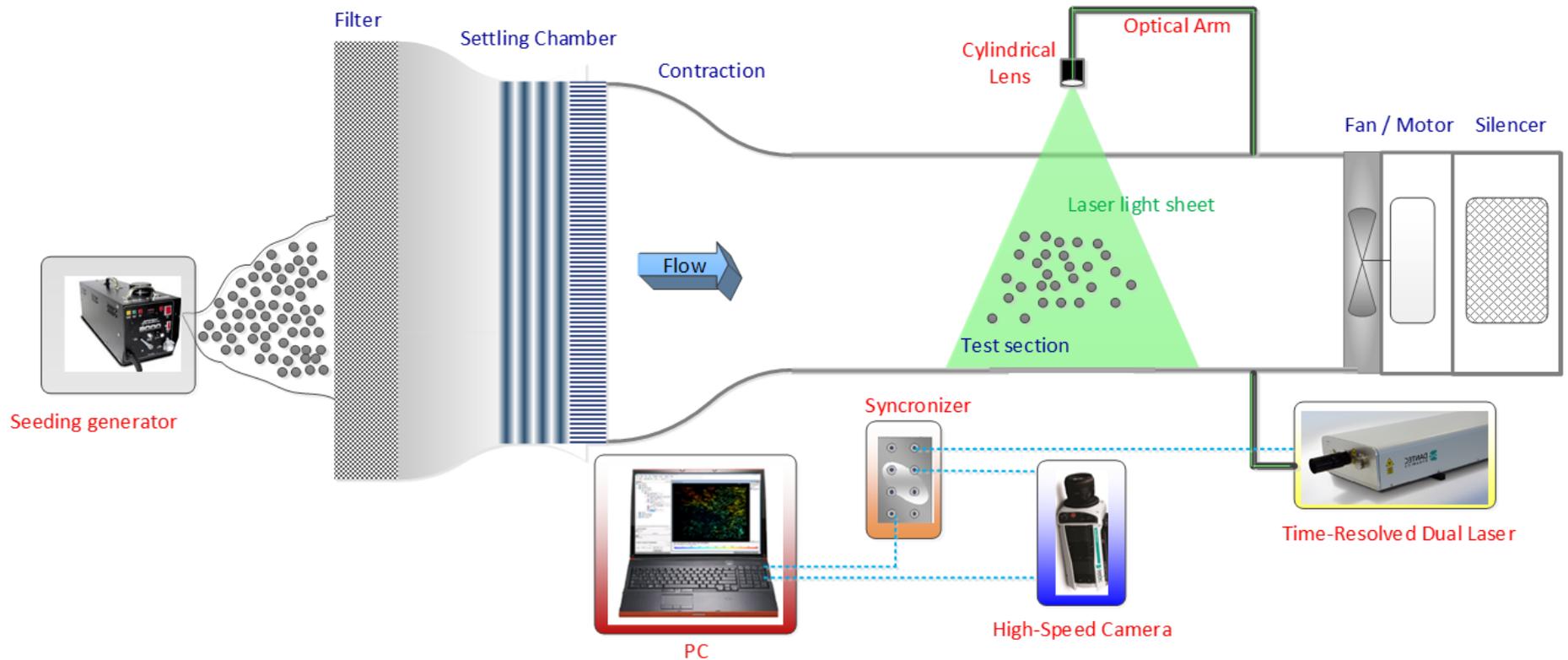


● New rotating device

- Pitch angle: $\pm 45^\circ$
- Yaw angle: $\pm 180^\circ$
- Interval: 1°

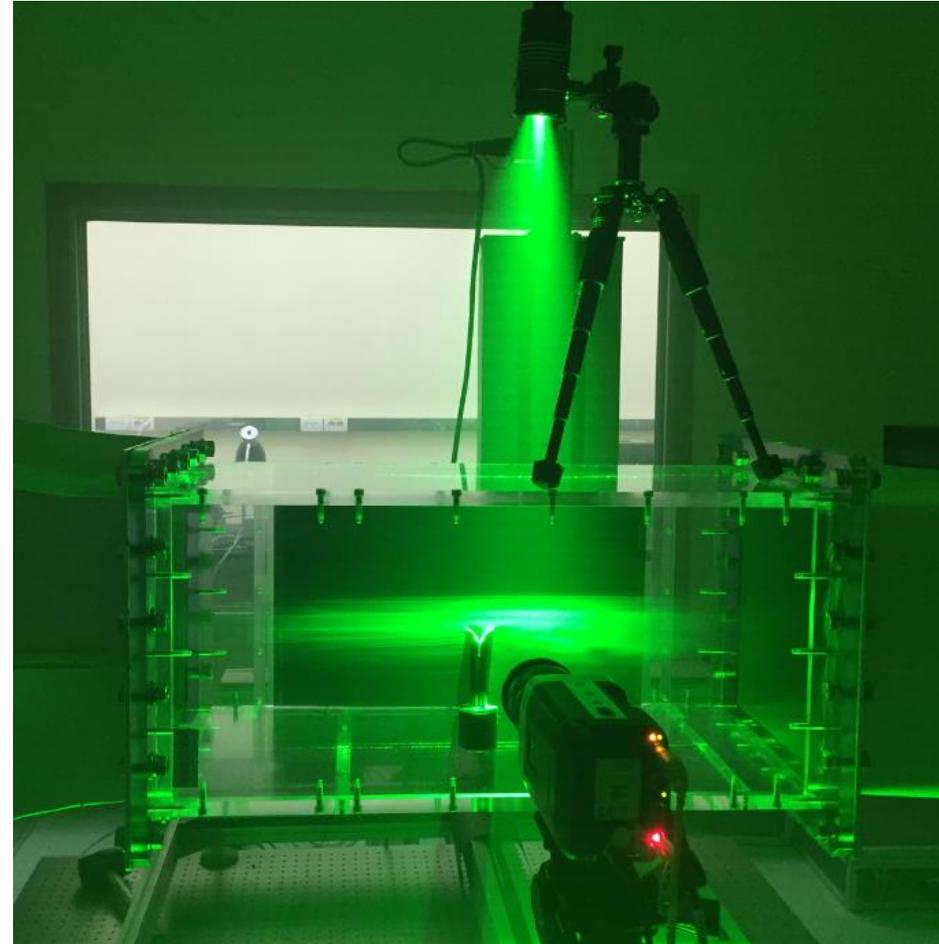
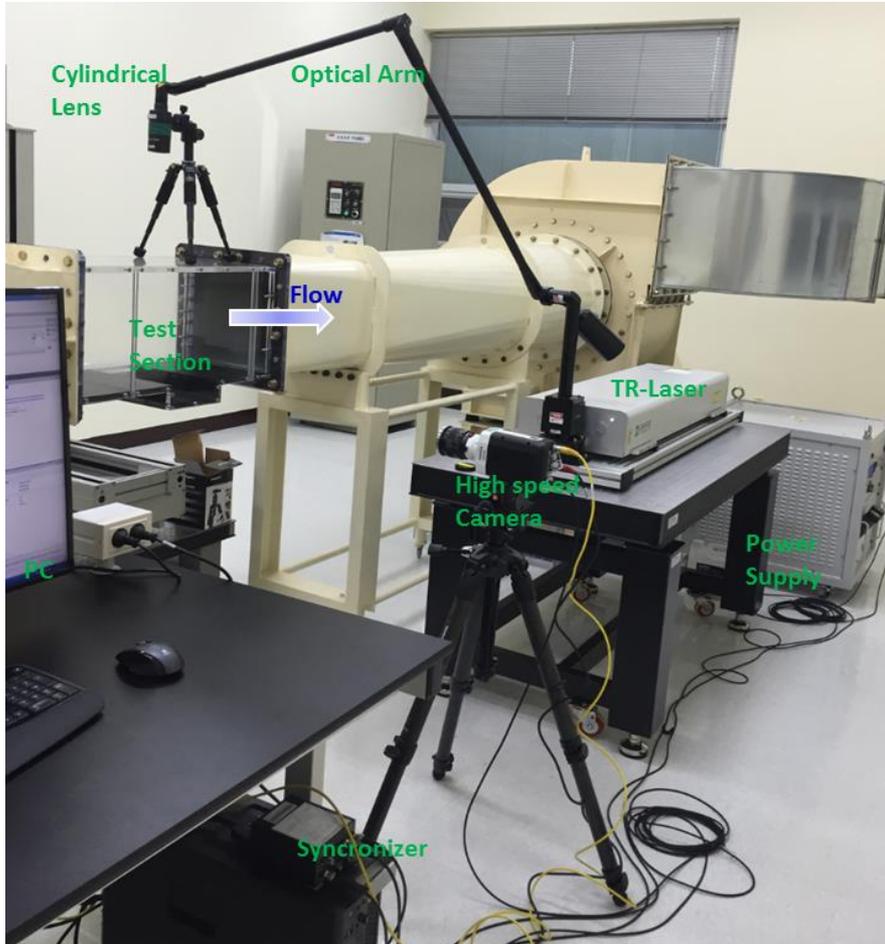
Particle Image Velocimetry(PIV)

- Quantitative visualization of flow phenomenon around S-type Pitot tube
- Time-resolved laser (20mJ), High-speed camera(3200 fps), Time interval = 1ms between two-consequent velocity image



Particle Image Velocimetry(PIV)

- Quantitative visualization of flow phenomenon around S-type Pitot tube
- Time-resolved laser (20mJ), High-speed camera(3200 fps), Time interval = 1ms between two-consequent velocity image



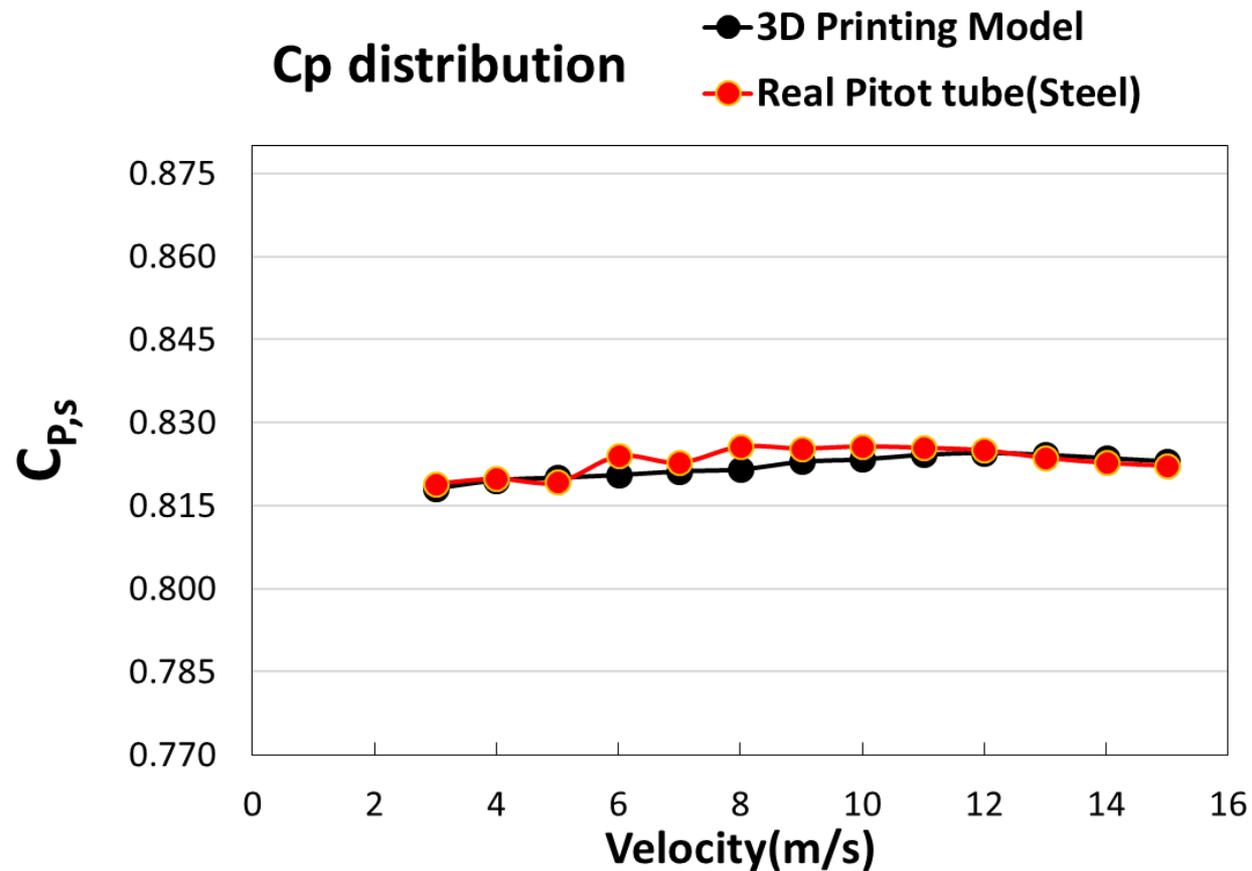
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Verification of 3D Printing model

- Compare C_p distribution according to velocity change

$L=1.6D$, 30 Deg.



- Two pitot tubes show almost similar results in yaw and pitch angle change

Experiments for the effect of S pitot geometry I

1. Distance between leg base and facing-opening plane (L)

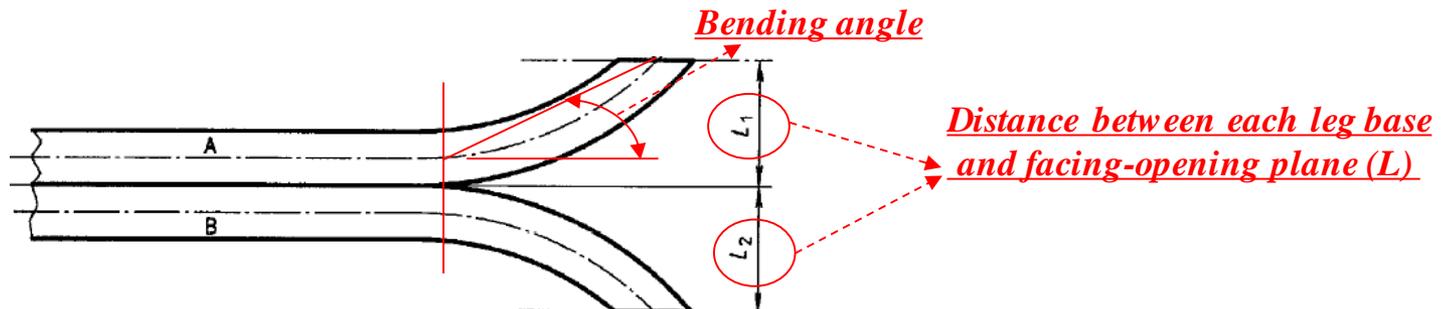
→ $L = 1.05D, 1.6D, 3D$

2. Bending Angle of opening parts

→ $\alpha = 15^\circ, 30^\circ, 45^\circ$

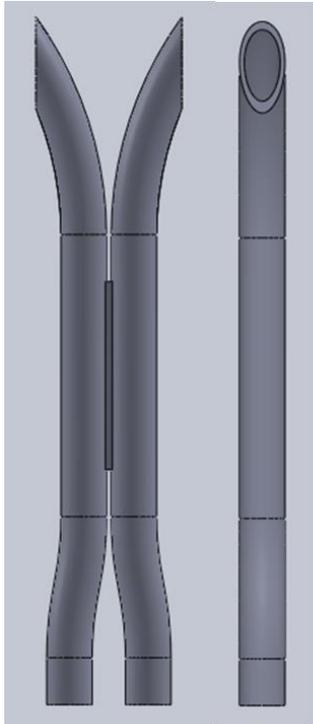
3. Shape of opening parts

→ **Curved**, Straight

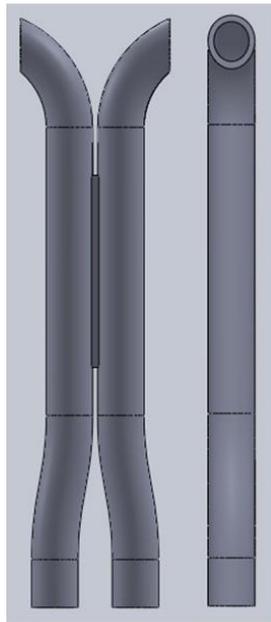


L=1.6D Models

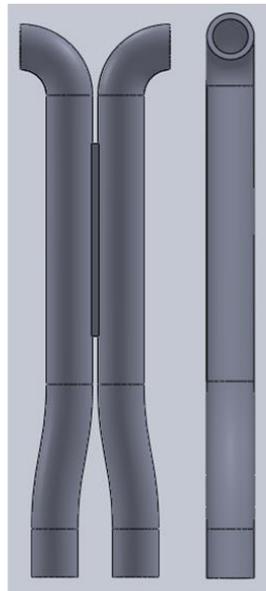
- Compare L=1.6D models ($\alpha = 15$ Deg., 30 Deg. and 45 Deg.)



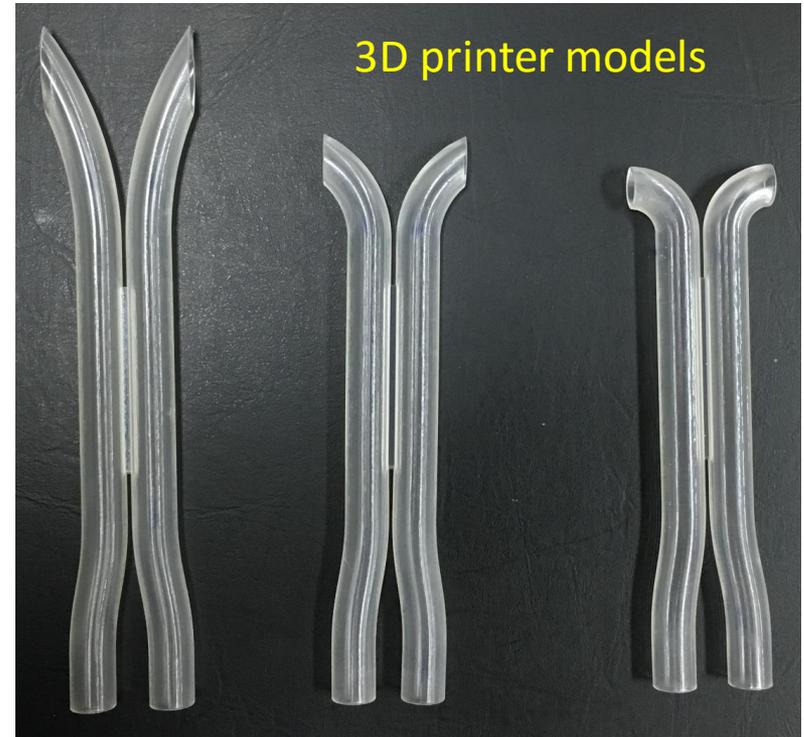
$\alpha = 15^\circ$, L = 1.6D



$\alpha = 30^\circ$, L = 1.6D

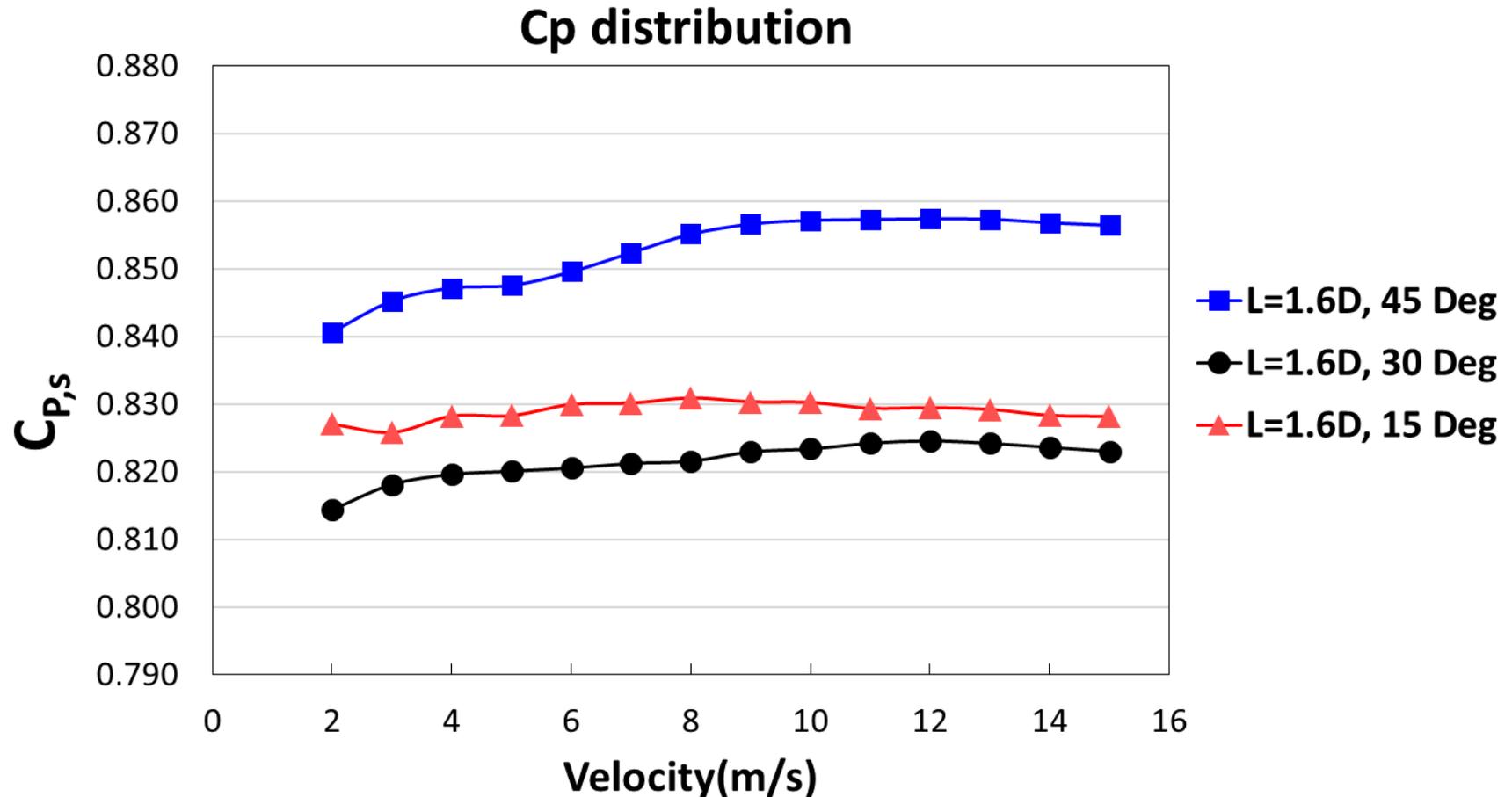


$\alpha = 45^\circ$, L = 1.6D



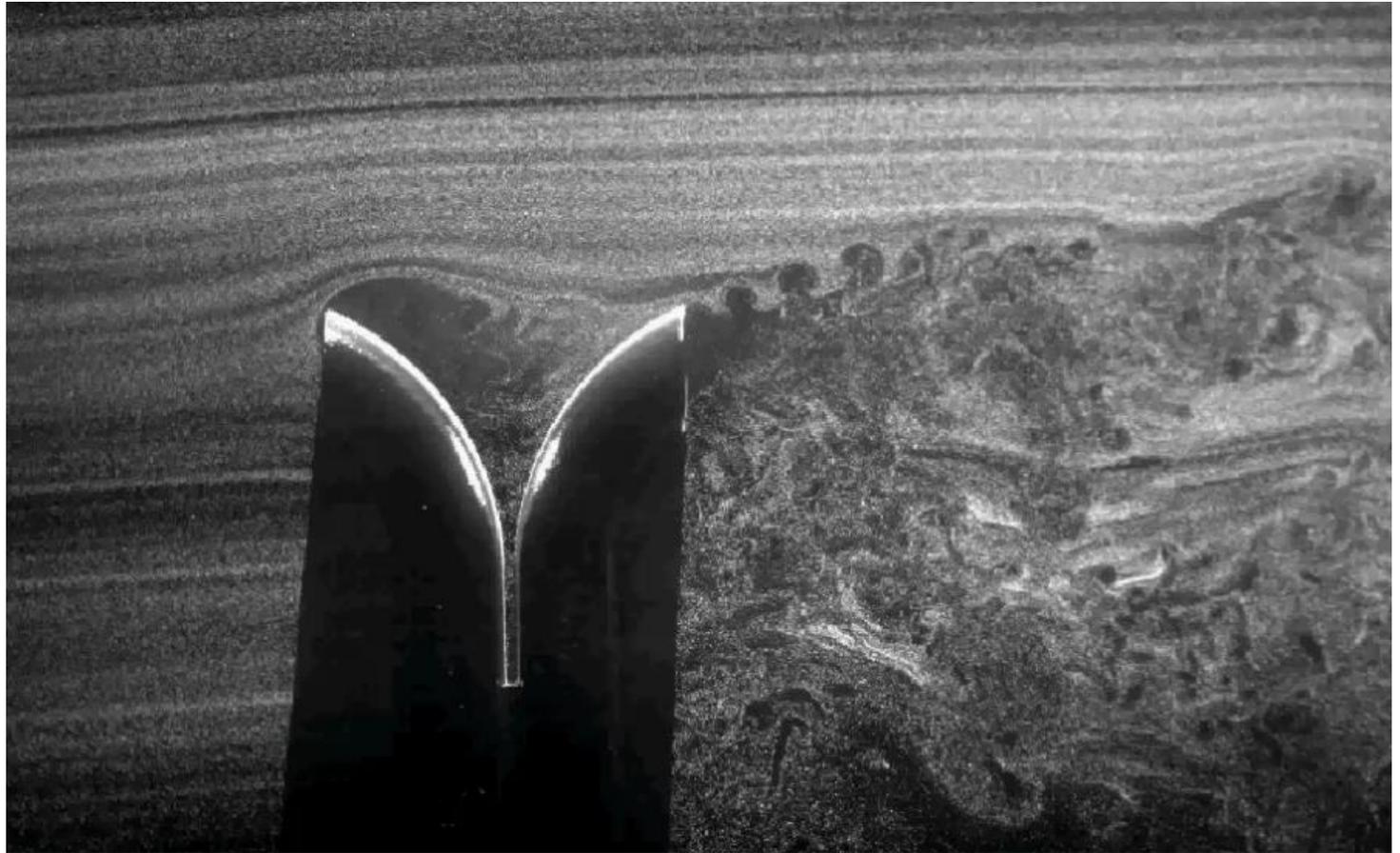
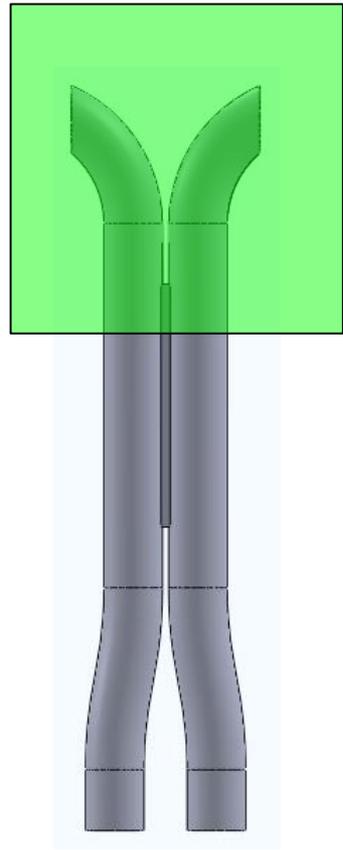
L=1.6D Models(Cp distribution)

- The $\alpha=45^\circ$ (L=1.6D) S Pitot has Cp larger than others 4%, Cp is increasing as incoming velocity increases up 15 m/s



L=1.6D, 30 Deg Model(PIV)

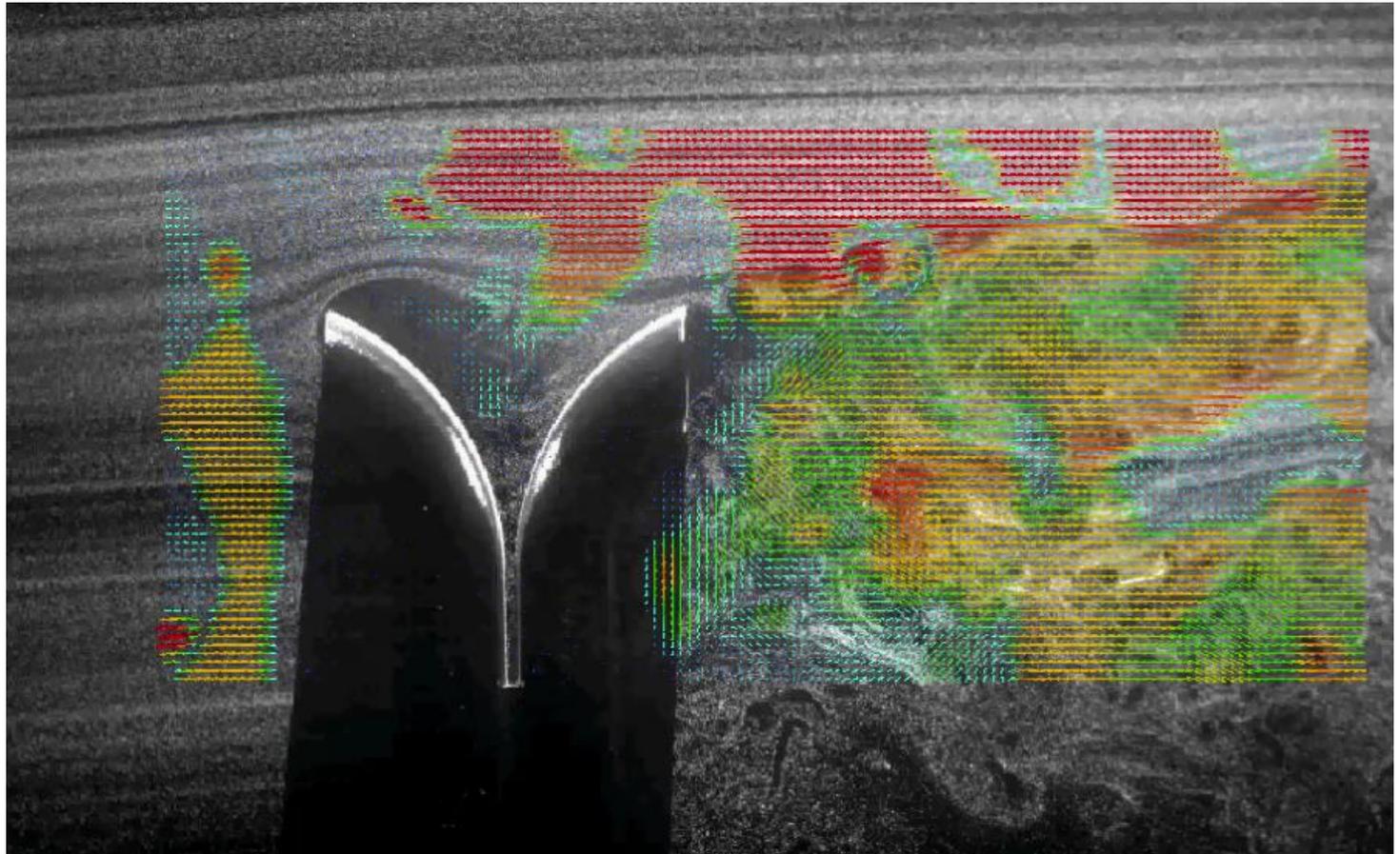
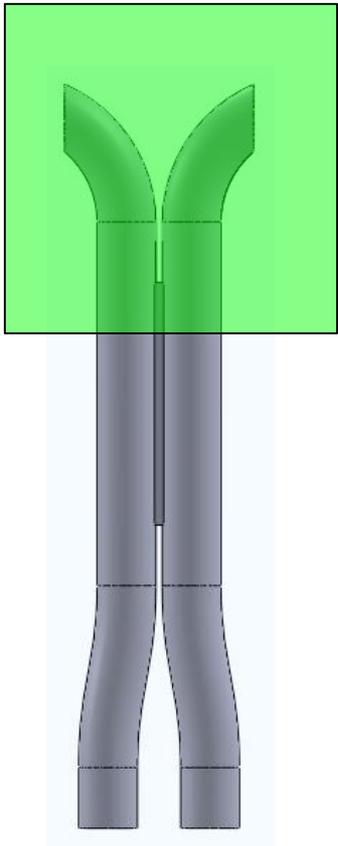
- Flow phenomenon around S-type Pitot tube



- Due to complicated geometry between the impact and wake orifices, the **separated flows** are developed to a **vortical structure** behind orifices

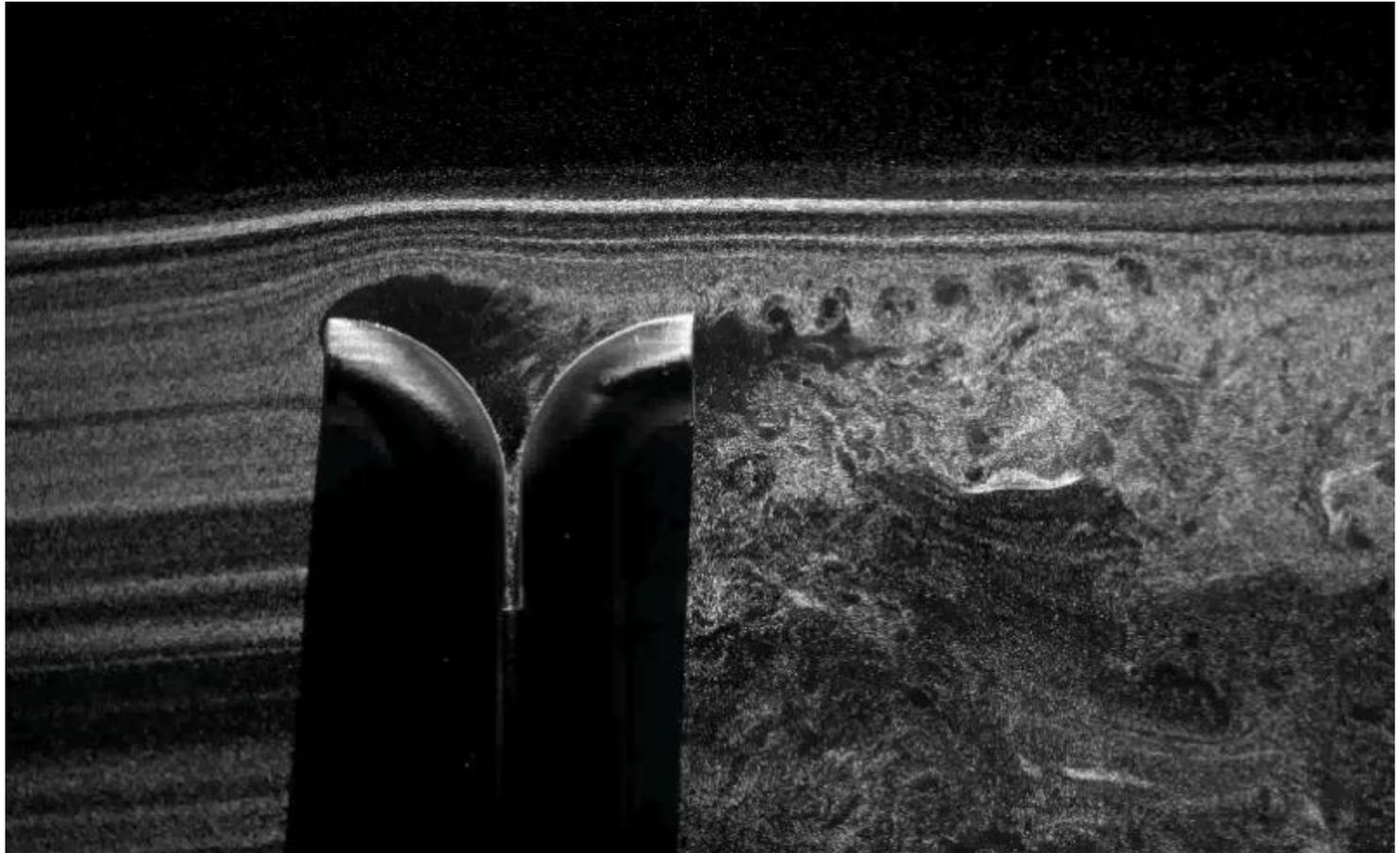
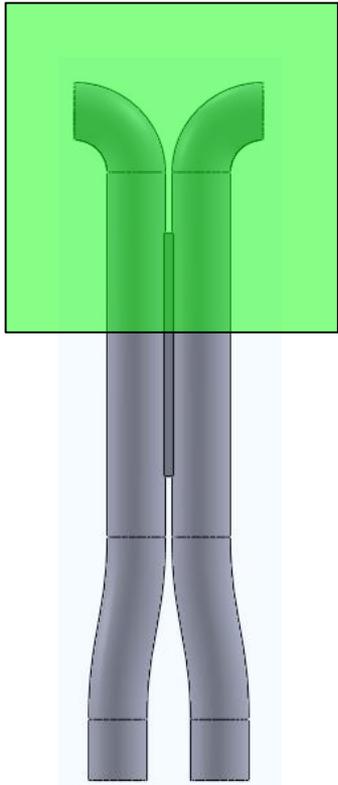
$L=1.6D$, 30 Deg Model(PIV)

- Velocity vector distribution around S-type Pitot tube



L=1.6D, 45 Deg Model(PIV)

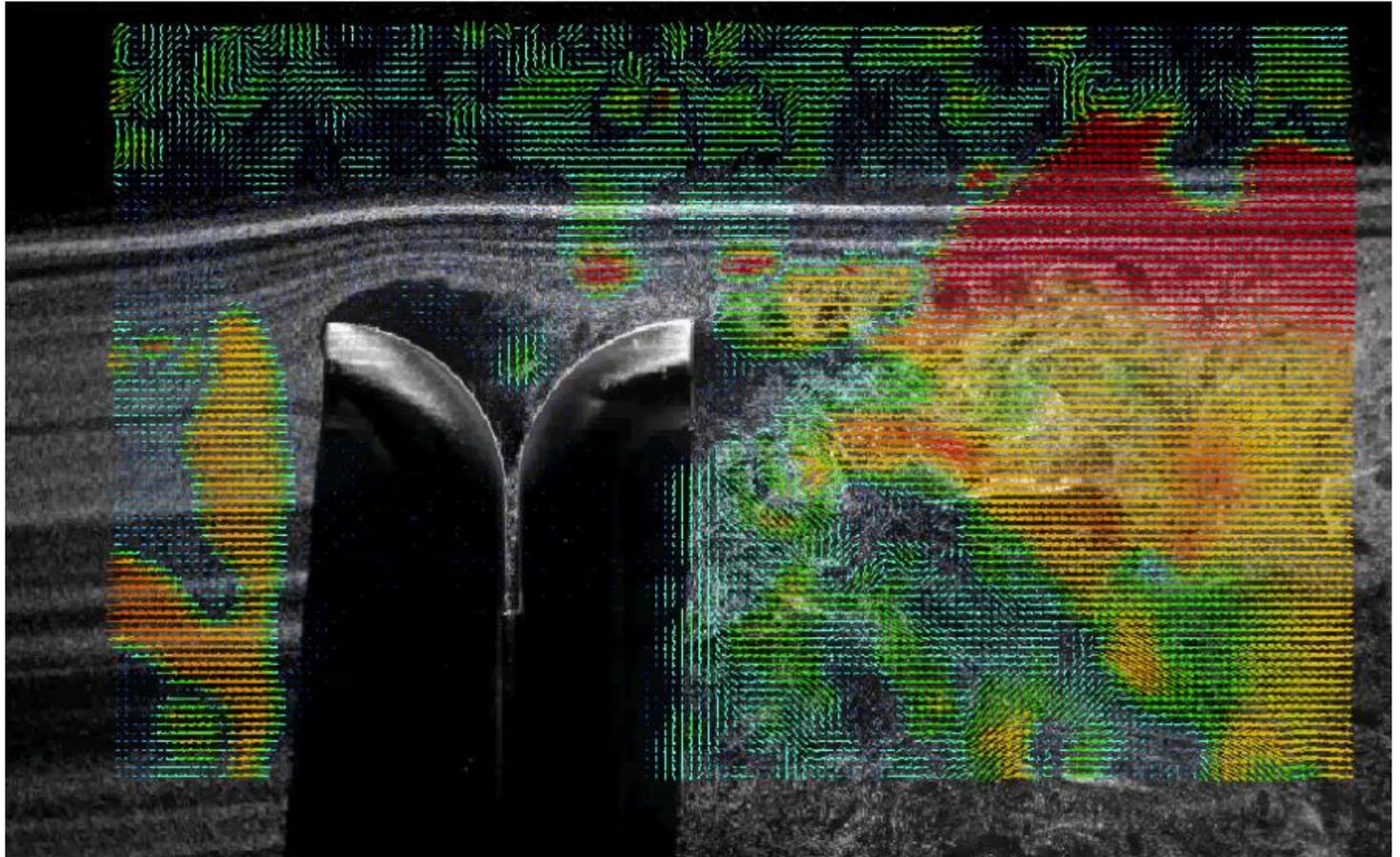
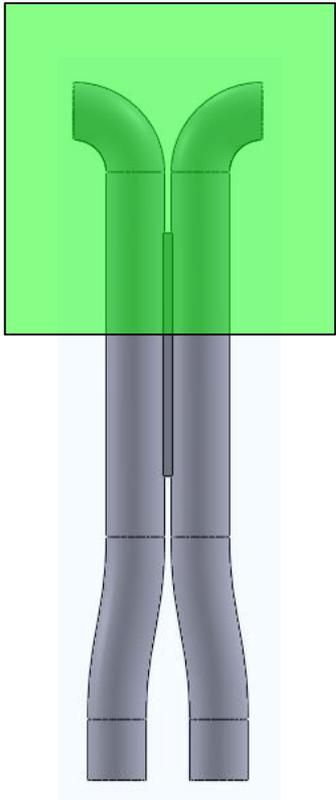
- Flow phenomenon around S-type Pitot tube (L=1.6D, 45 Deg.)



- Separated flow from wake orifice(downstream) were **developing less** due to **gradual change of curved surface** compared to 30 deg model.

$L=1.6D$, 45 Deg Model(PIV)

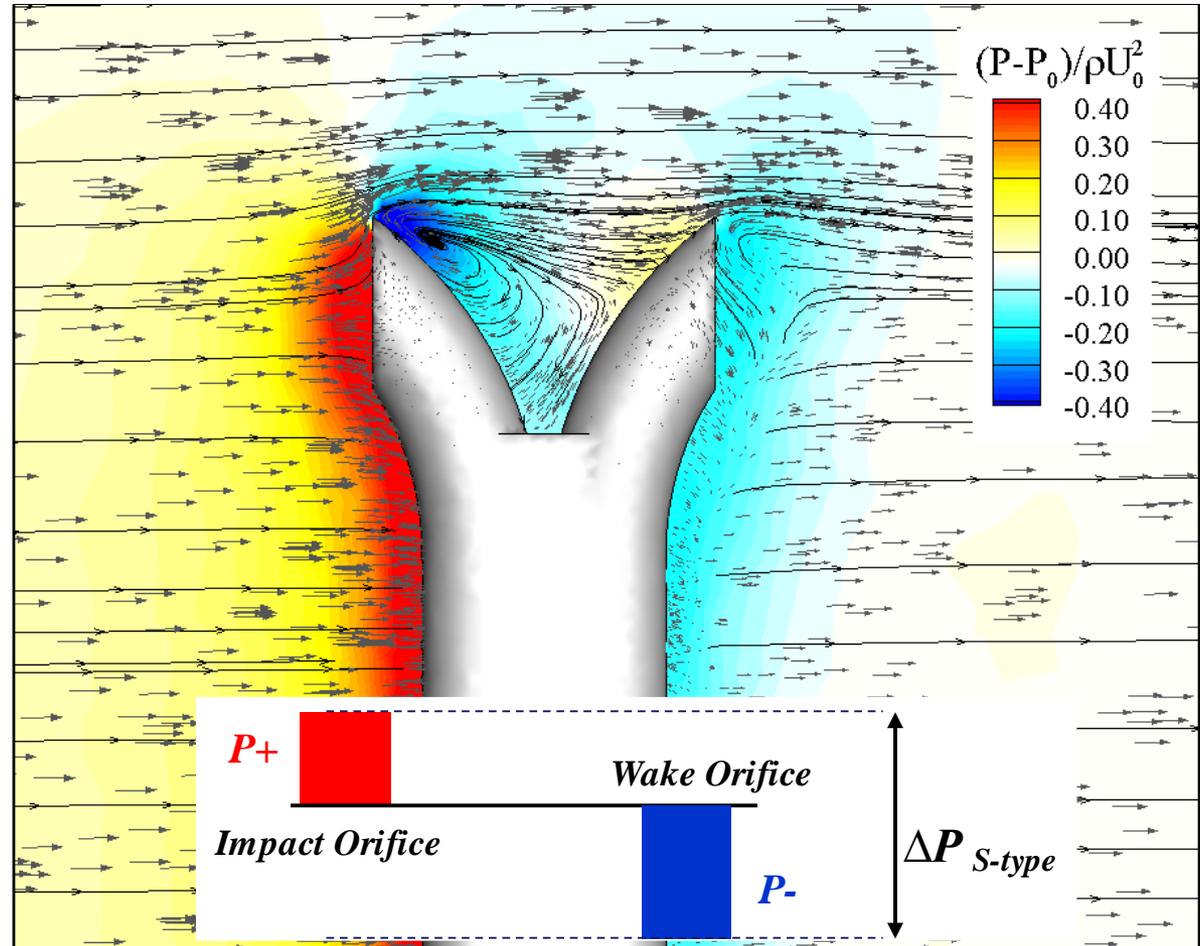
- Velocity vector distribution around S-type Pitot tube



Cp,s-type coefficients

- When vortical structure behind the wake orifice developed well
Lower pressure at wake orifice observed → Cp,s decreased

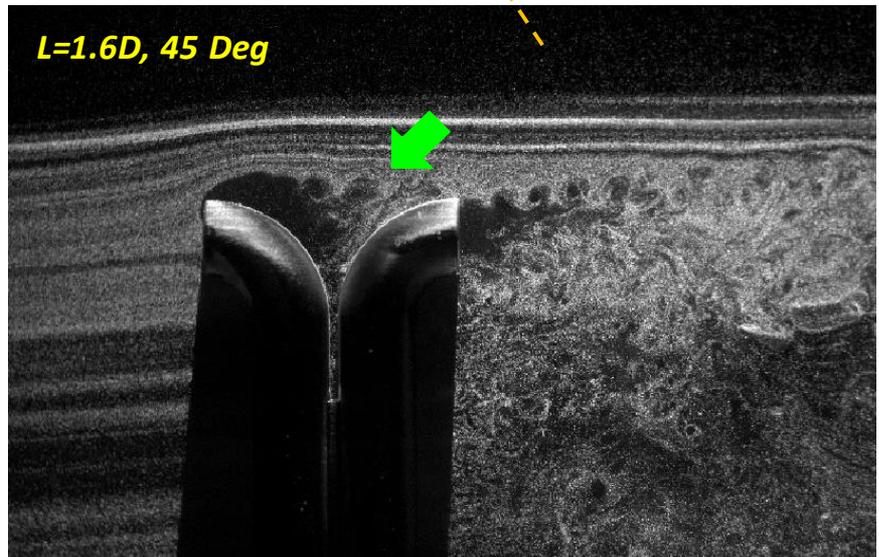
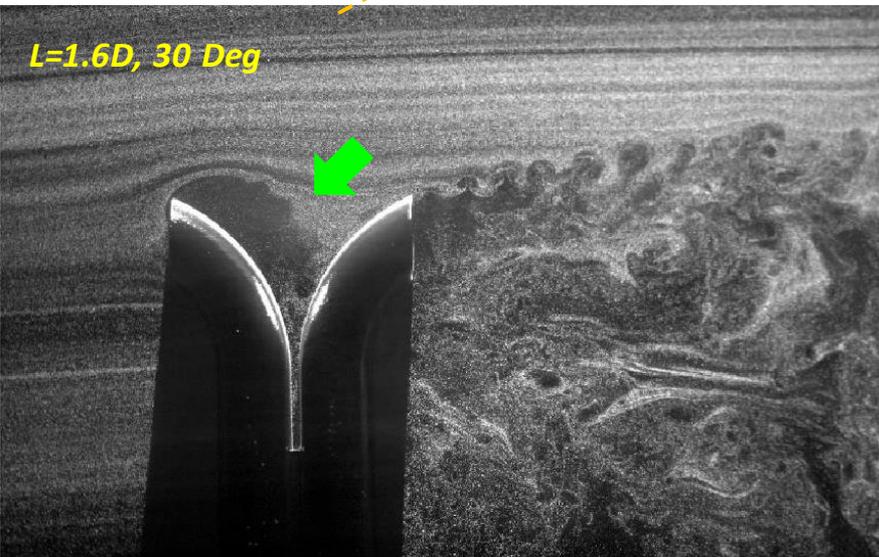
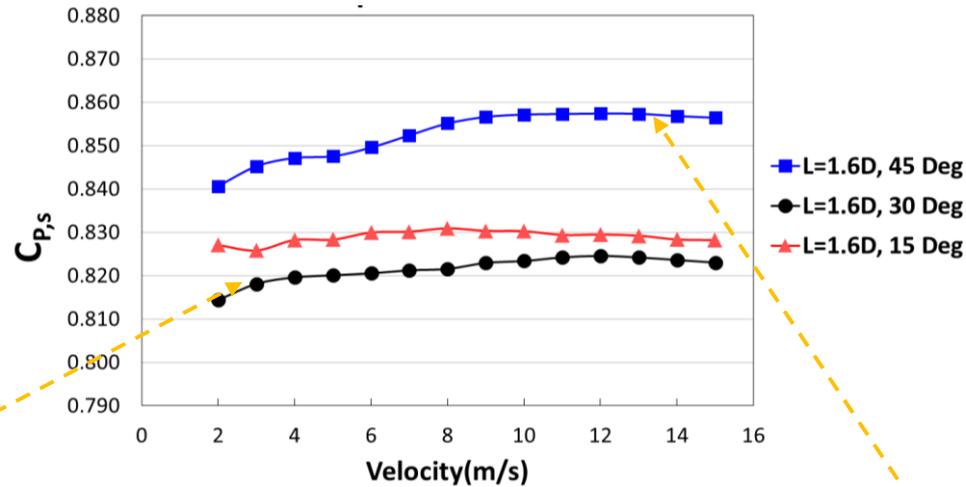
$$C_{P,S} = C_{P,Std} \left(\frac{\Delta P_{Std}}{\Delta P_{S-type}} \right)$$



Numerical simulation
FMI, Kang et al. 2015

L=1.6D 30 Deg vs 45 Deg

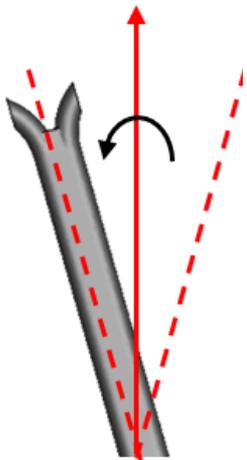
- Separated flow from wake orifice(downstream) were **developing less** due to **gradual change of curved surface** → $C_{p,s}$ increased (45 deg)



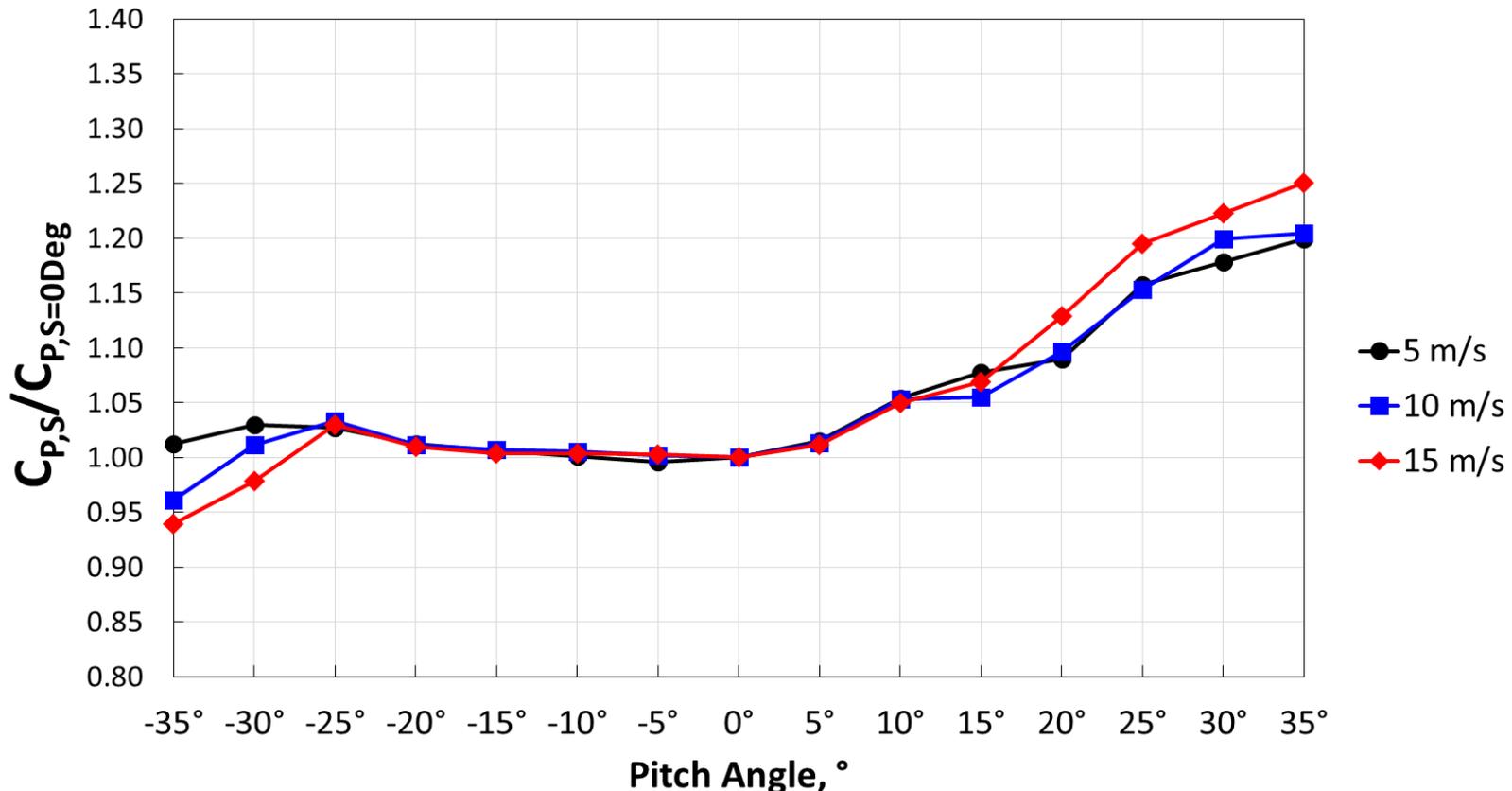
L=1.6D Model (Pitch angle)

- The normalized S-type Pitot tube coefficients increase as the pitch angle increases

Effect of Pitch angle misalignment, L=1.6D, 30Deg



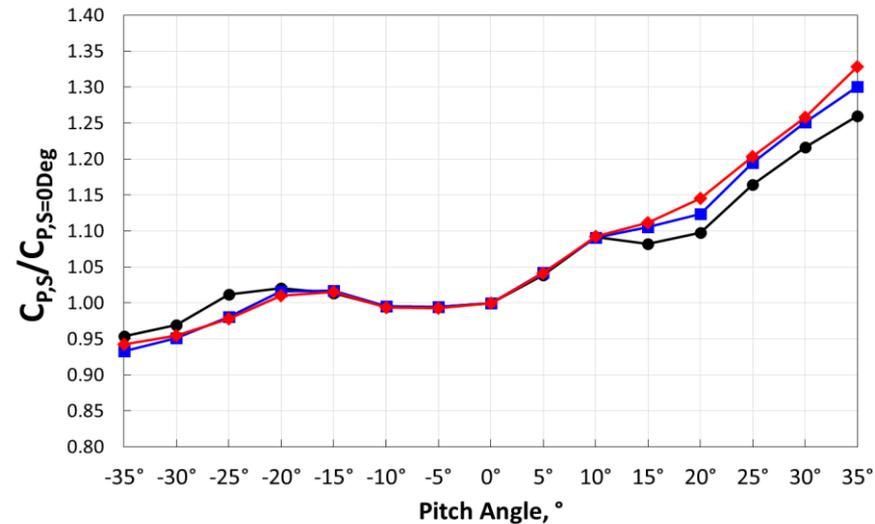
Pitch angl



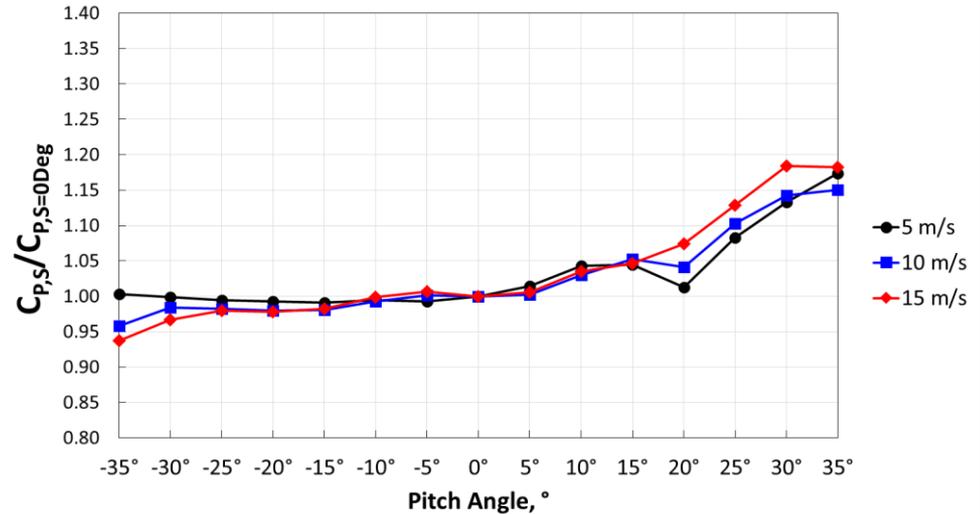
L=1.6D Model (Pitch angle)

- Three models(15, 30 and 45 Deg) show similar pattern to Pitch angle change

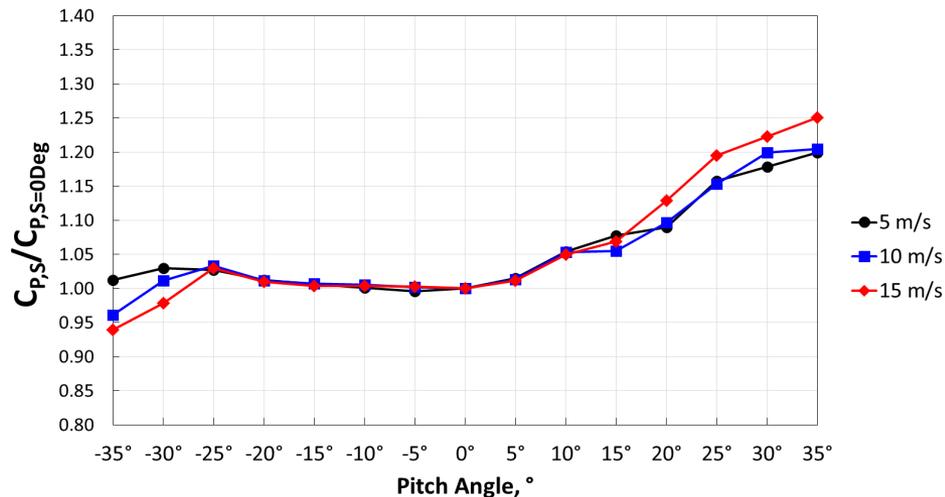
Effect of Pitch angle misalignment, L=1.6D, 15Deg



Effect of Pitch angle misalignment, L=1.6D, 45Deg

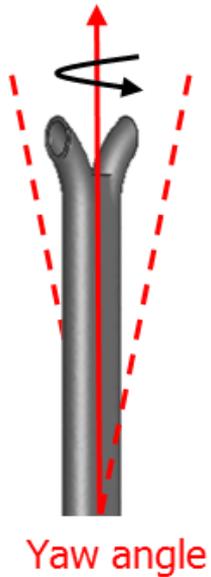


Effect of Pitch angle misalignment, L=1.6D, 30Deg

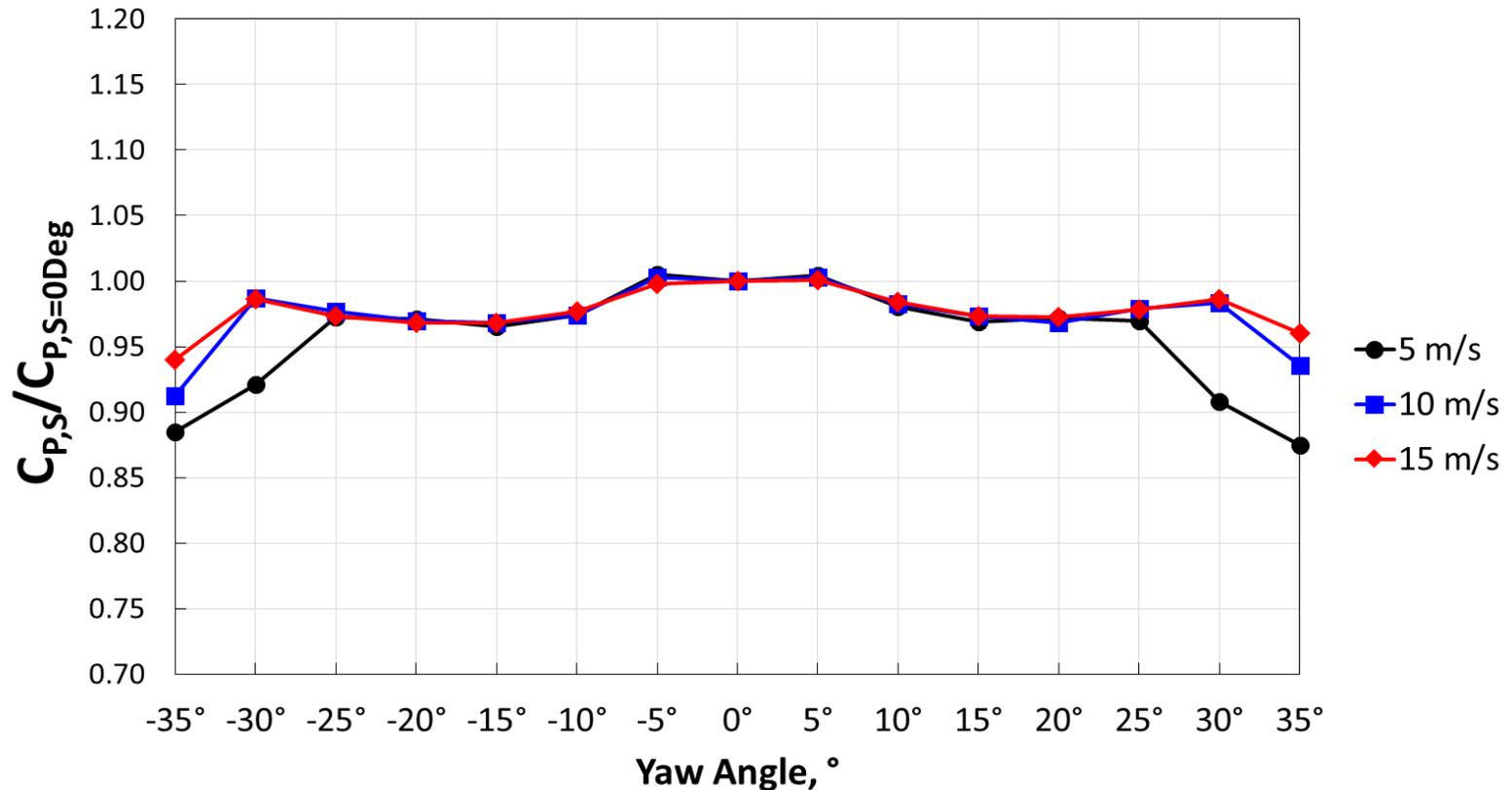


L=1.6D Model (Yaw angle)

- The normalized S-type Pitot tube coefficients decreased as the yaw angle increases with symmetric tendency



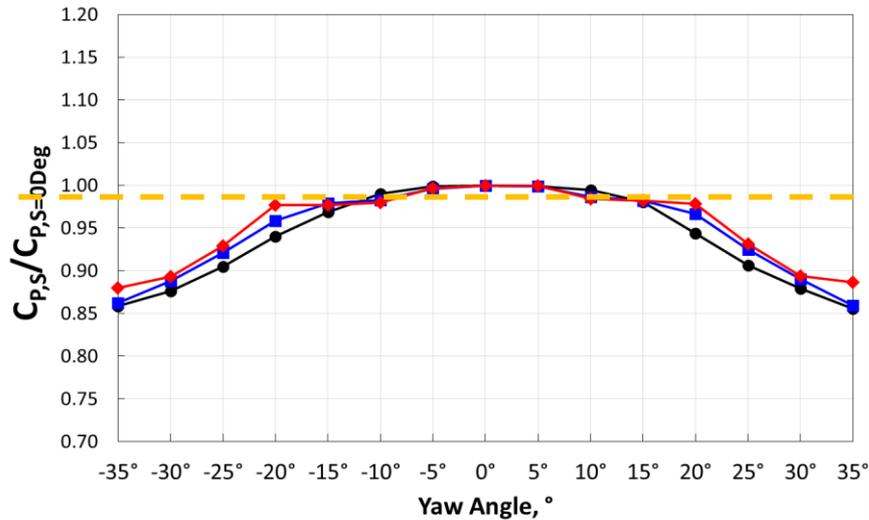
Effect of yaw angle misalignment, $L=1.6D$, 30Deg



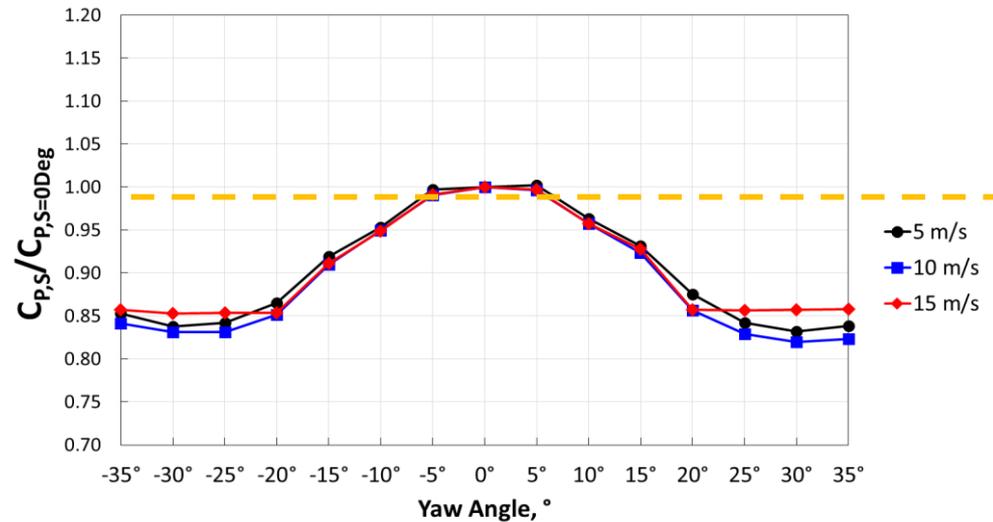
L=1.6D Model (Yaw angle)

- 30 Deg. Model show **less sensitive** to yaw angle misalignment within wide range of yaw angles

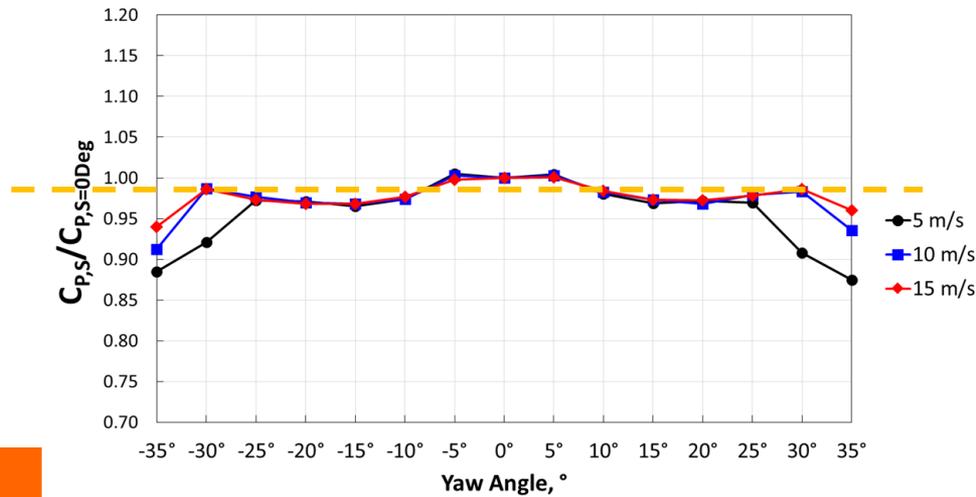
Effect of yaw angle misalignment, L=1.6D, 15Deg



Effect of yaw angle misalignment, L=1.6D, 45Deg

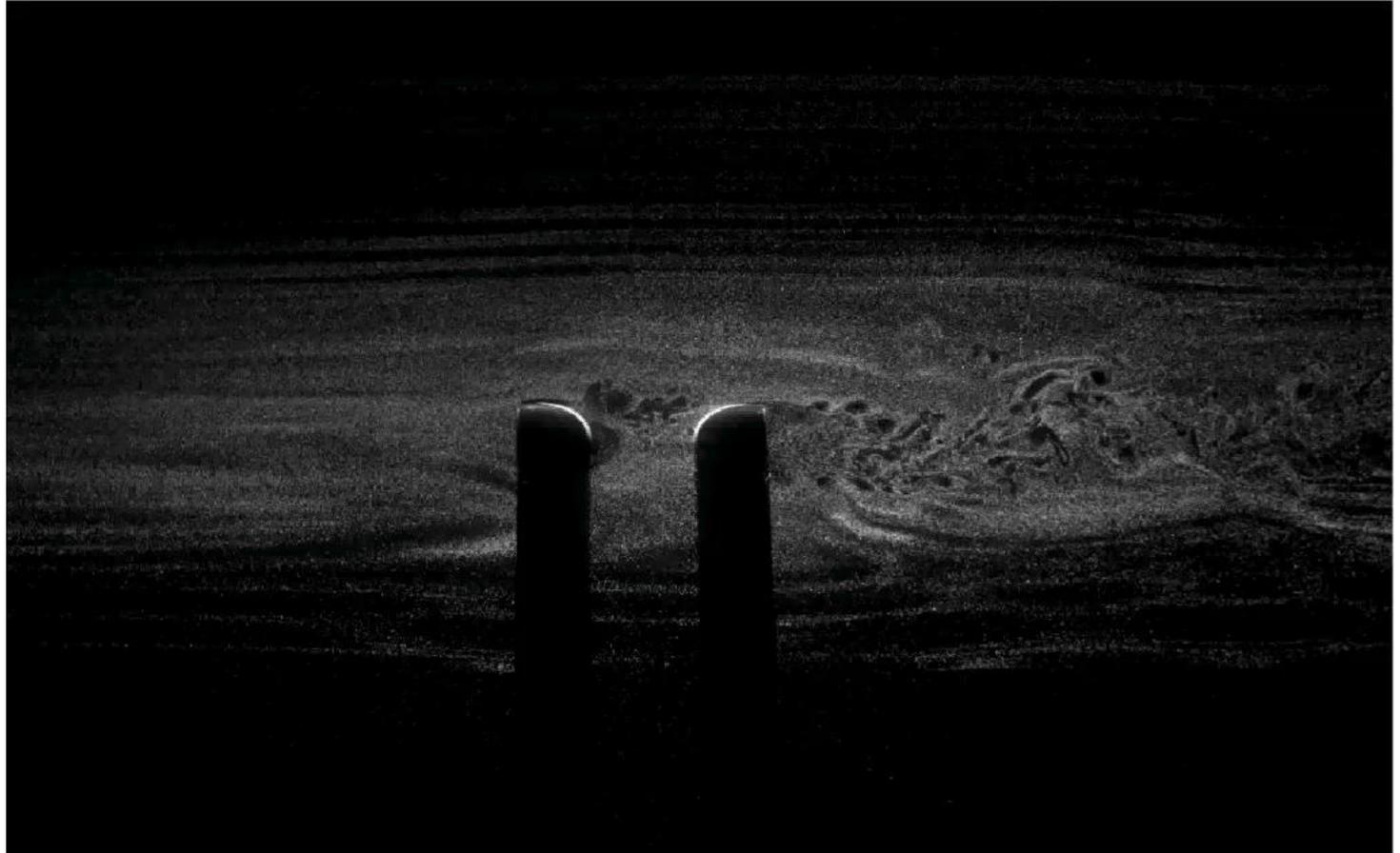
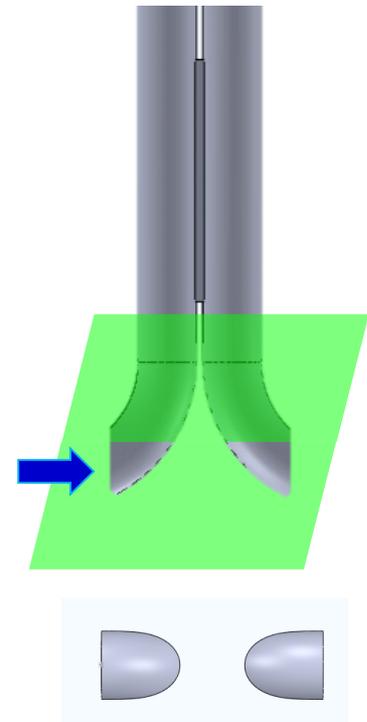


Effect of yaw angle misalignment, L=1.6D, 30Deg



L=1.6D 30 Deg. (Yaw=0°) PIV

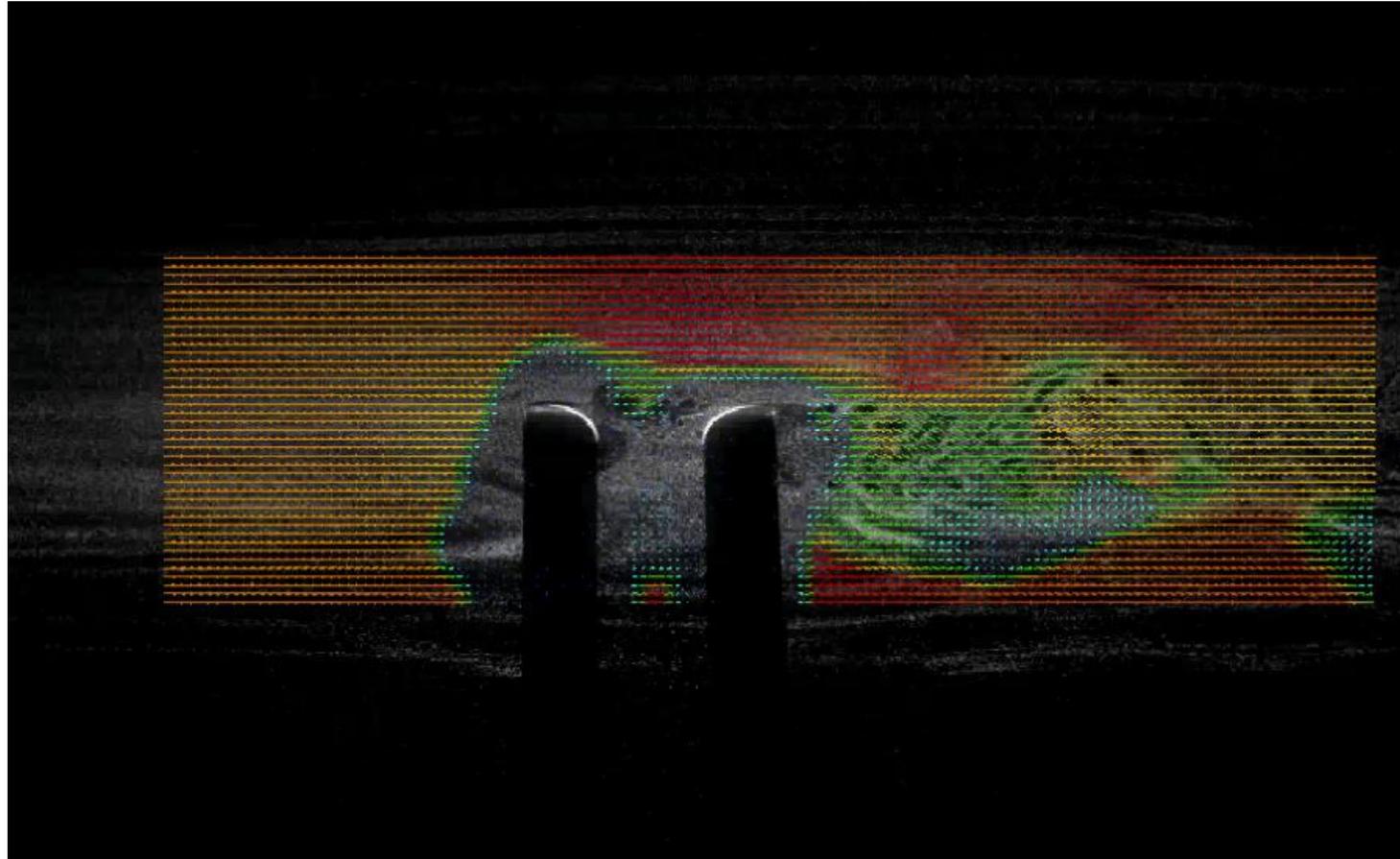
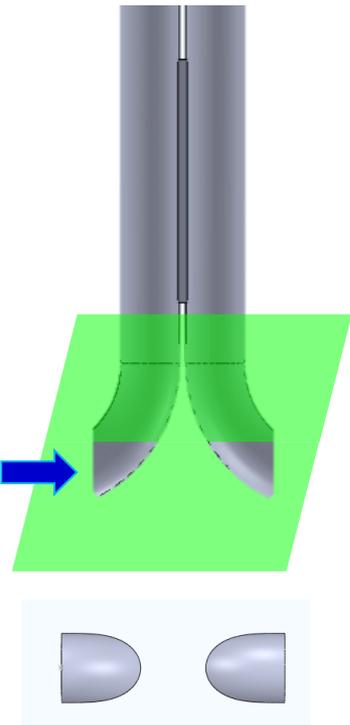
- Flow phenomenon around S-type Pitot tube (L=1.6D, 30 Deg.)



- Each vortical structures from impact and wake orifices are observed

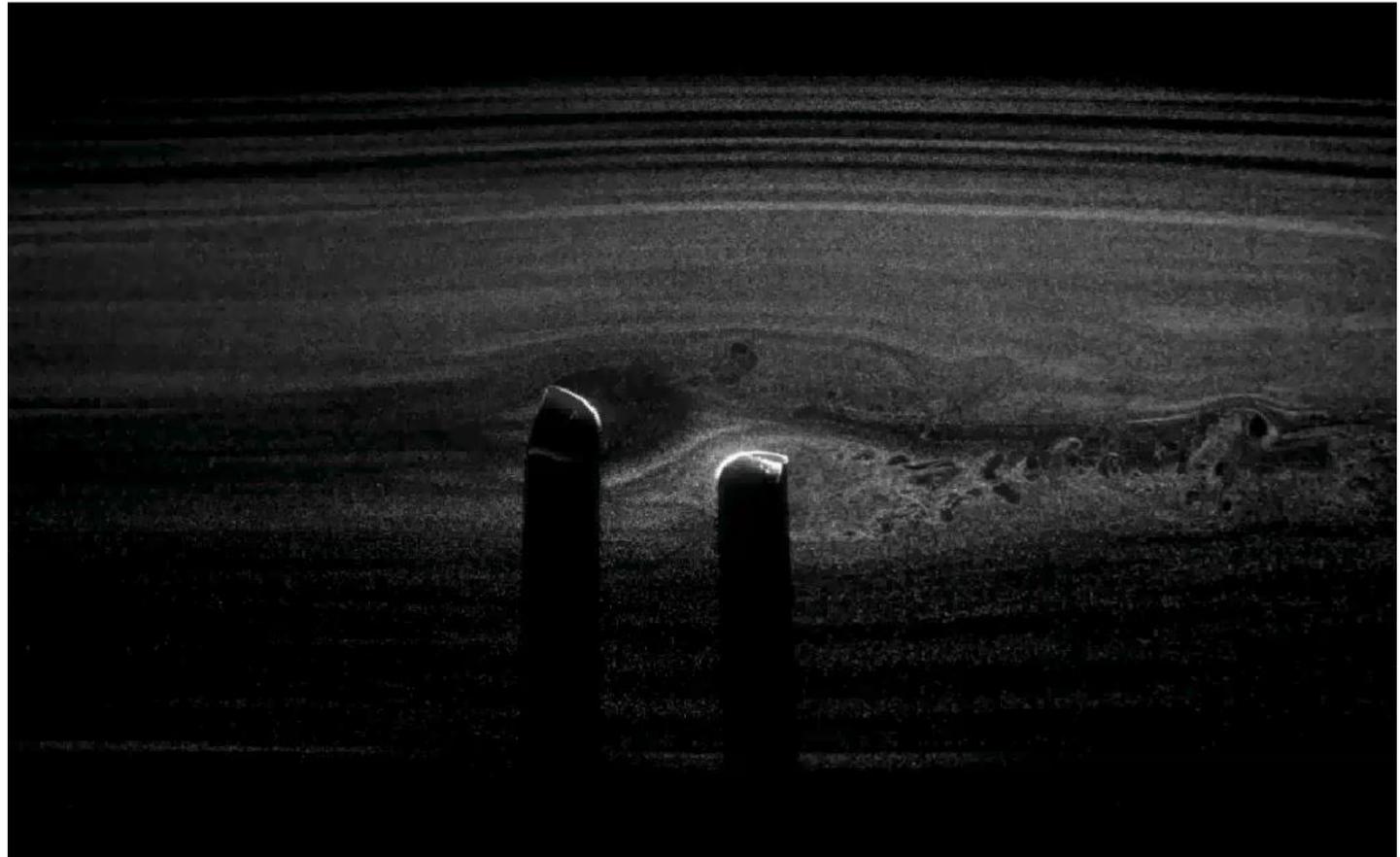
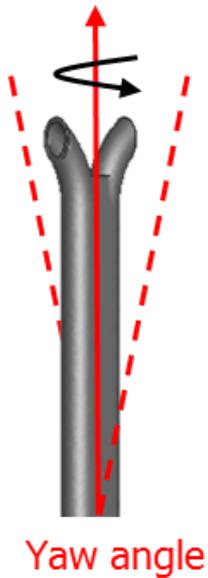
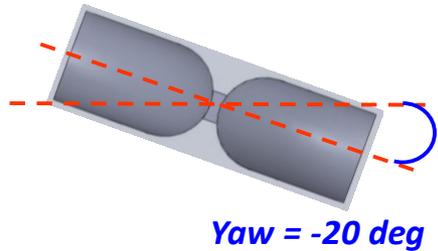
L=1.6D 30 Deg. (Yaw=0°) PIV

- Velocity vector distribution around S-type Pitot tube



L=1.6D 30 Deg. (Yaw=-20°) PIV

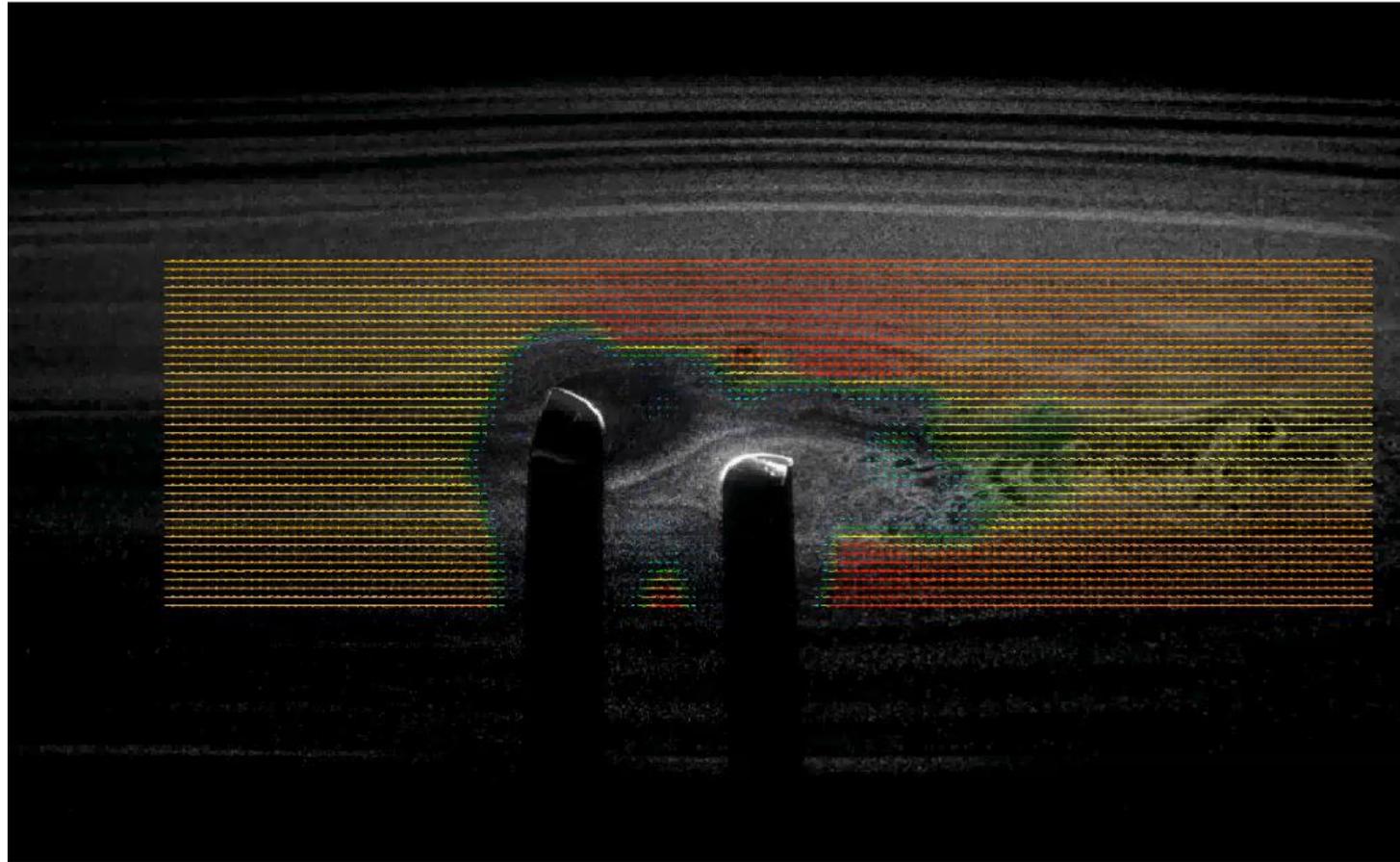
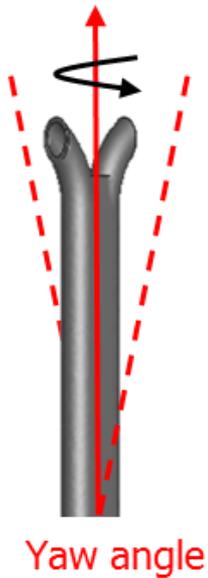
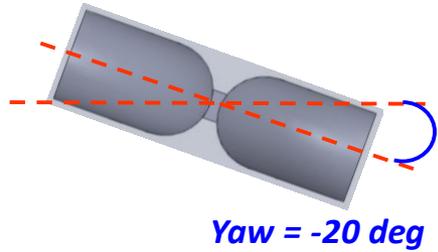
- Flow phenomenon around S-type Pitot tube (L=1.6D, 30 Deg.)



- Due to yaw angle misalignment, separated flows from surface of impact and wake orifice are enhanced

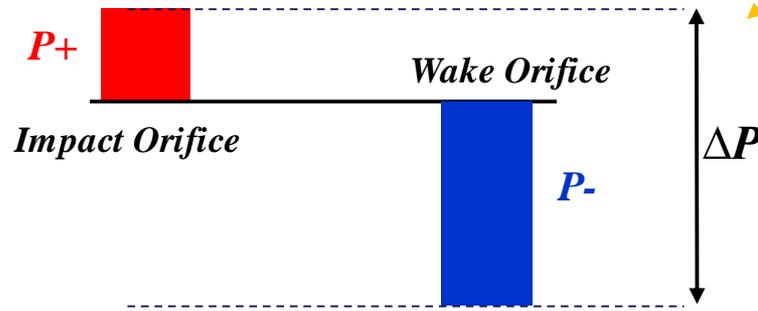
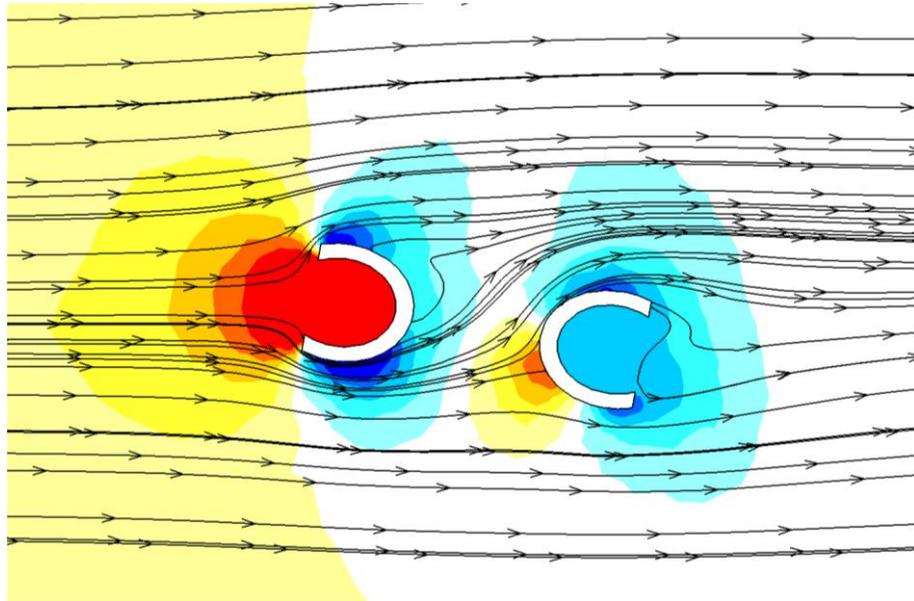
L=1.6D 30 Deg. (Yaw=-20°) PIV

- Velocity vector distribution around S-type Pitot tube



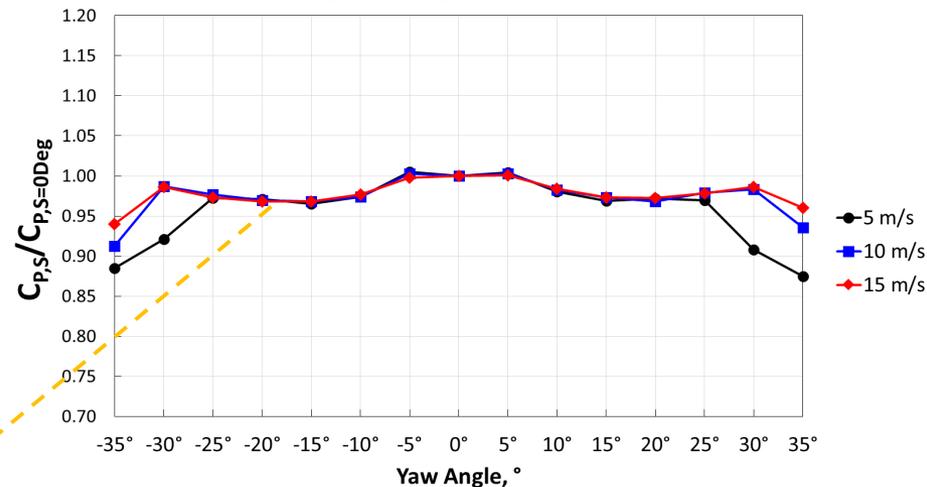
L=1.6D 30 Deg. (Yaw angle) PIV

- Pressure values near wake orifice decrease due to the enhancement of separated flow from orifice surface, which shows symmetry \pm yaw angle



Numerical simulation
FMI, Kang et al. 2015

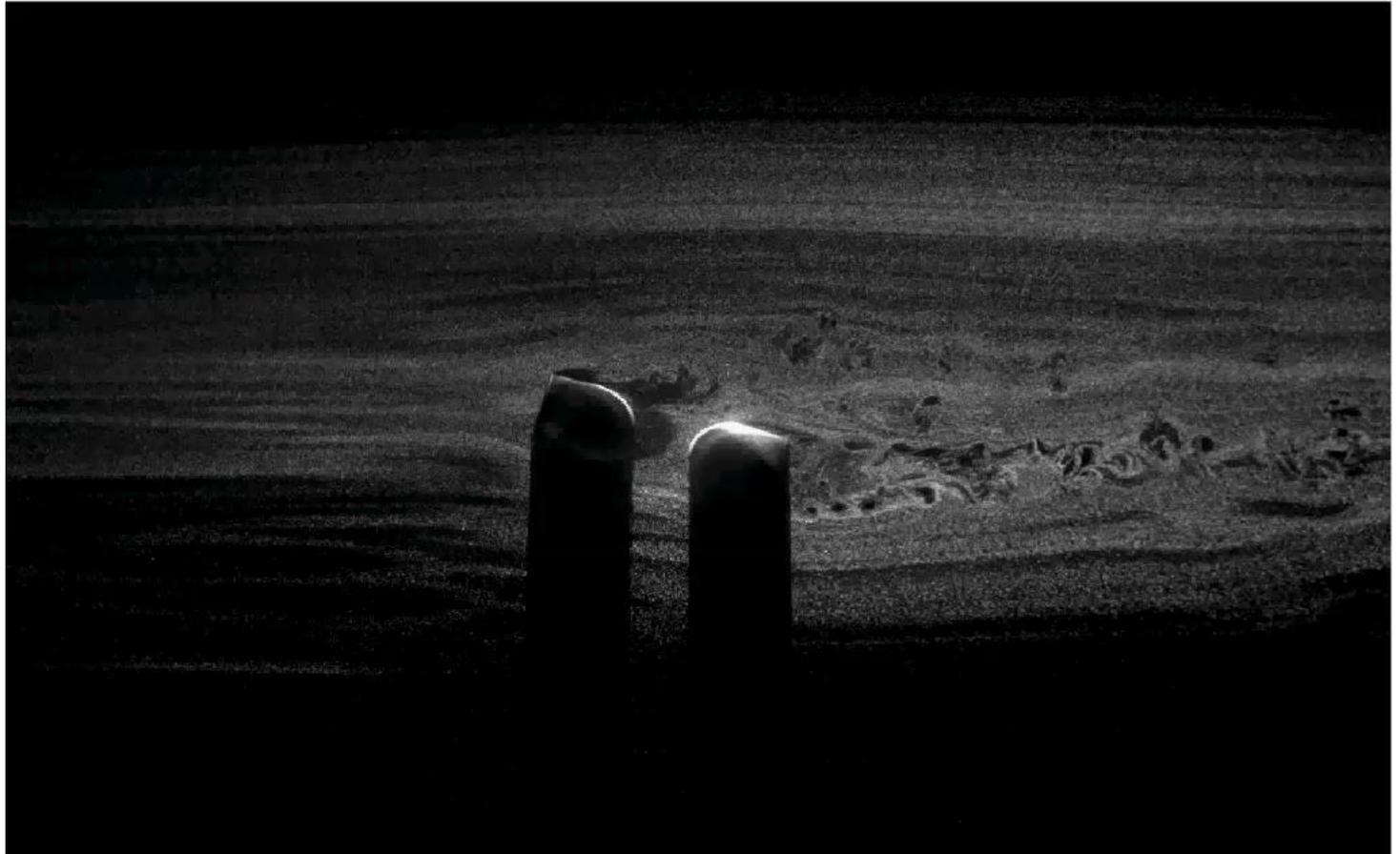
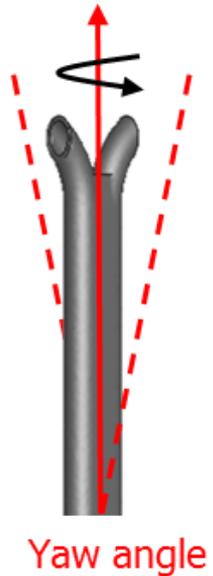
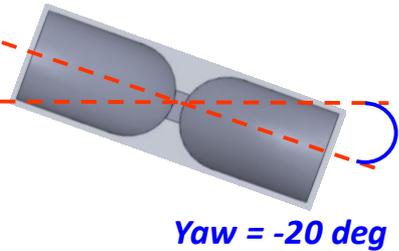
Effect of yaw angle misalignment, L=1.6D, 30Deg



$$C_{P,S} = C_{P,Std} \left(\frac{\Delta P_{Std}}{\Delta P_{S.type}} \right)$$

L=1.6D 45 Deg. (Yaw=-20°) PIV

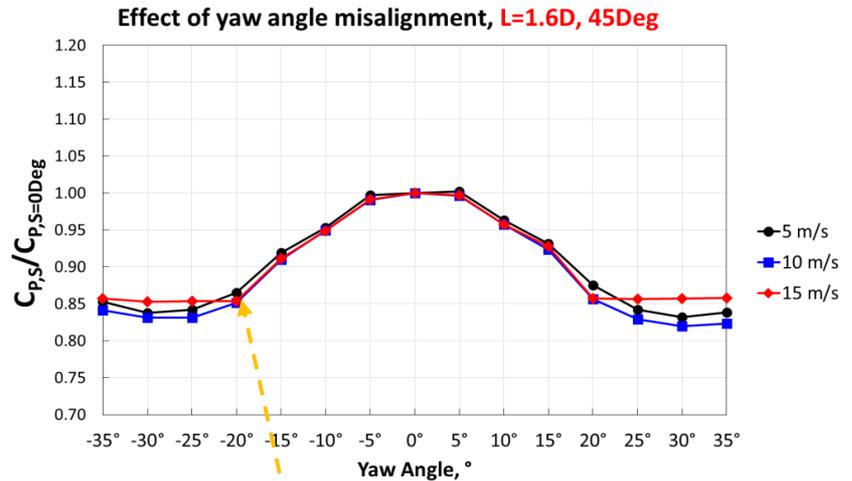
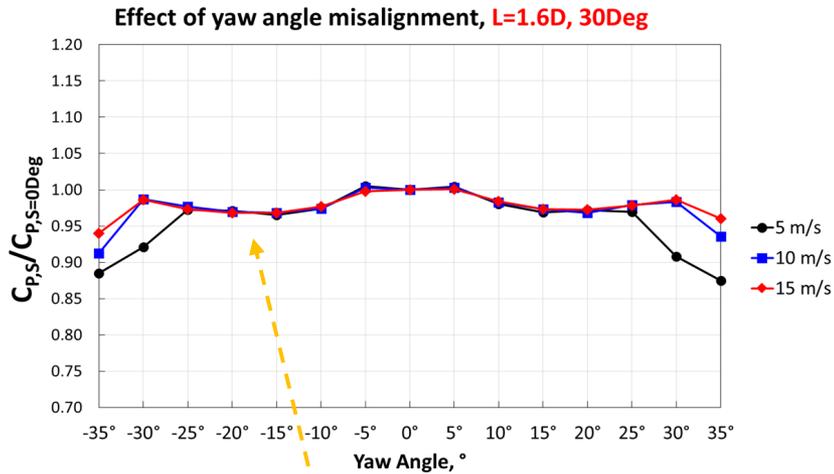
- Flow phenomenon around S-type Pitot tube (L=1.6D, 45 Deg.)



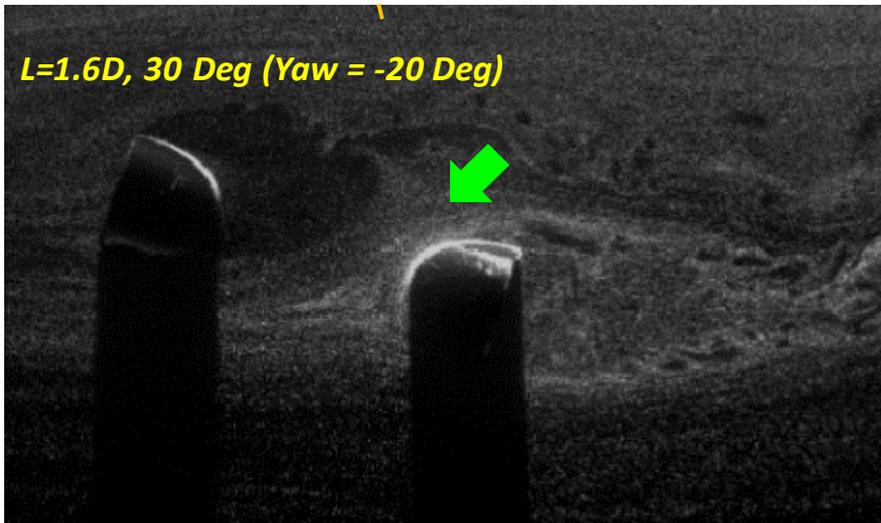
- Separated flow from impact orifice(upstream) **interfere** with vortical structures of wake orifices(downstream) due to the **proximity of two orifices**

L=1.6D 30 Deg vs 45 Deg (Yaw angle)

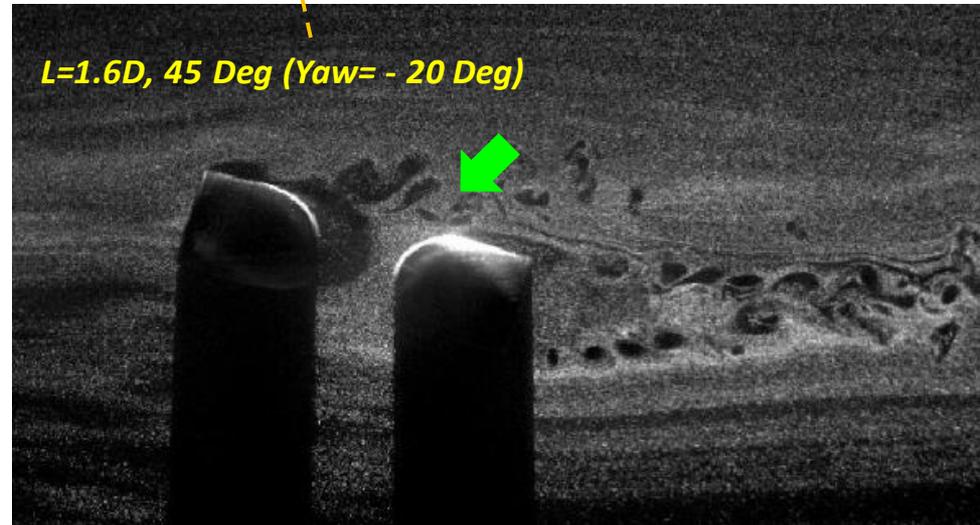
- When vortical structure behind the wake orifice were interfered with upstream separated flow, lower pressure near wake orifice
→ $C_{p,s}$ decreased (45 deg)



L=1.6D, 30 Deg (Yaw = -20 Deg)



L=1.6D, 45 Deg (Yaw = -20 Deg)



Experiments for the effect of S pitot geometry II

1. Distance between leg base and facing-opening plane (L)

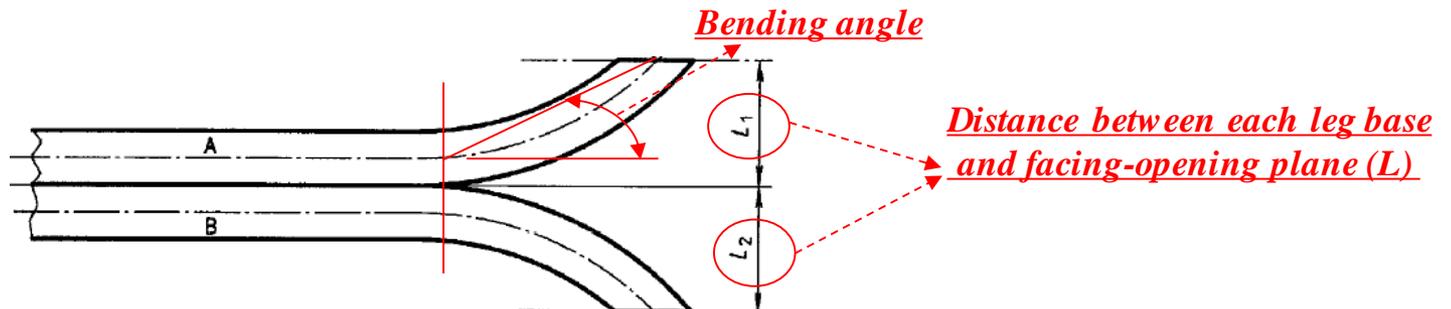
→ $L = 1.05D, 1.6D, 3D$

2. Bending Angle of opening parts

→ $\alpha = 15^\circ, 30^\circ, 45^\circ$

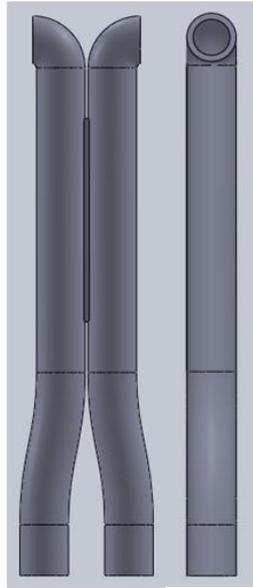
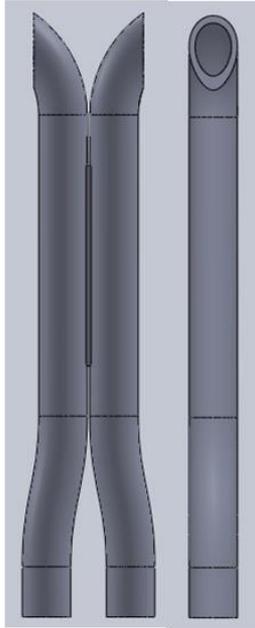
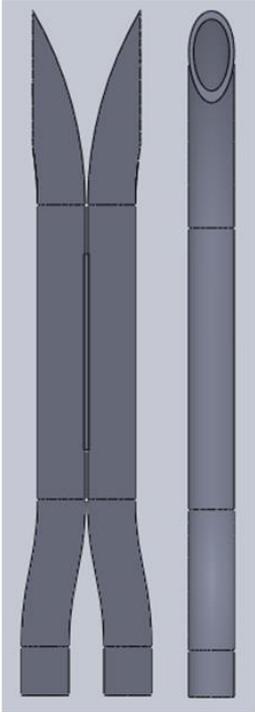
3. Shape of opening parts

→ **Curved**, Straight



L=1.05D Models

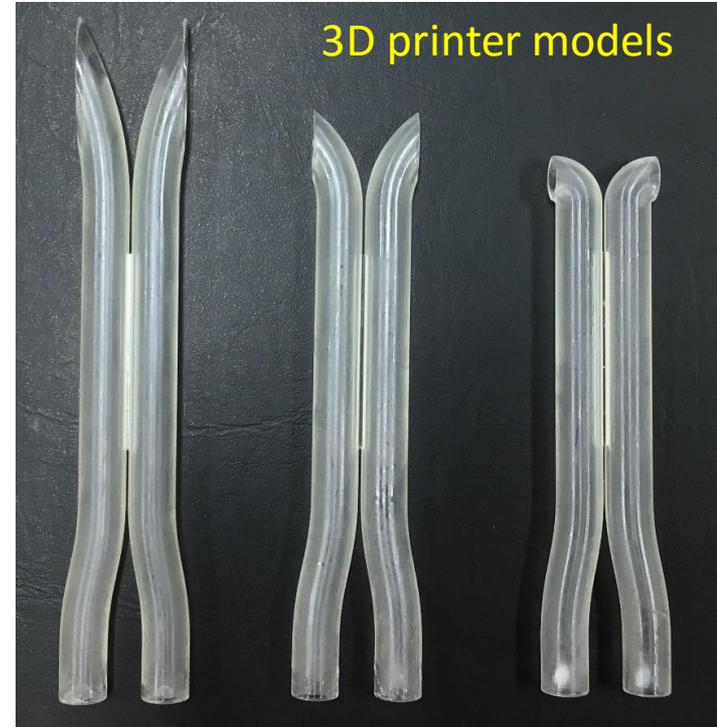
- Compare $L=1.05D$ models ($\alpha = 15$ Deg., 30 Deg. and 45 Deg.)



$\alpha = 15^\circ$, $L = 1.05D$

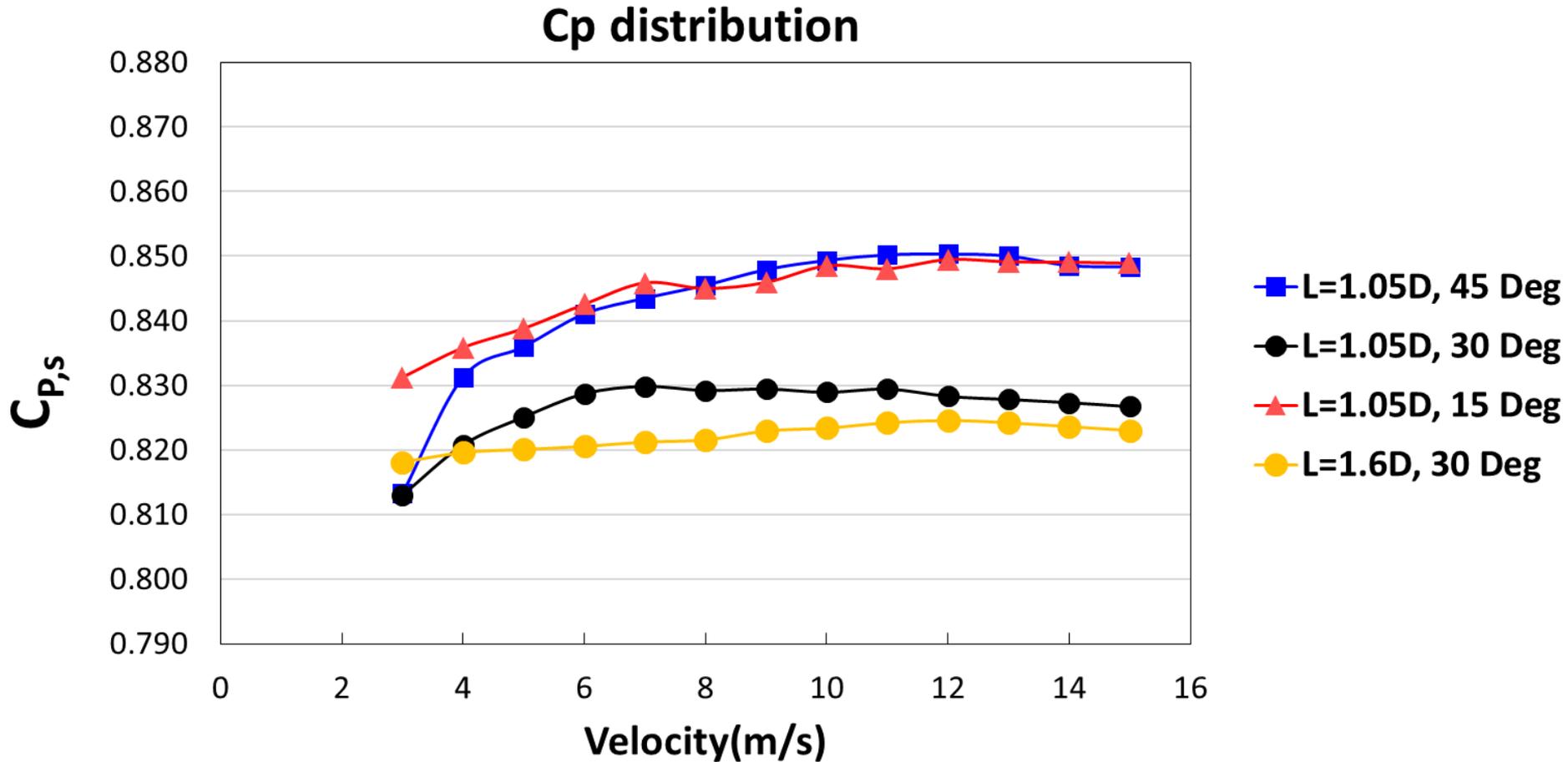
$\alpha = 30^\circ$, $L = 1.05D$

$\alpha = 45^\circ$, $L = 1.05D$



L=1.05D Models(Cp distribution)

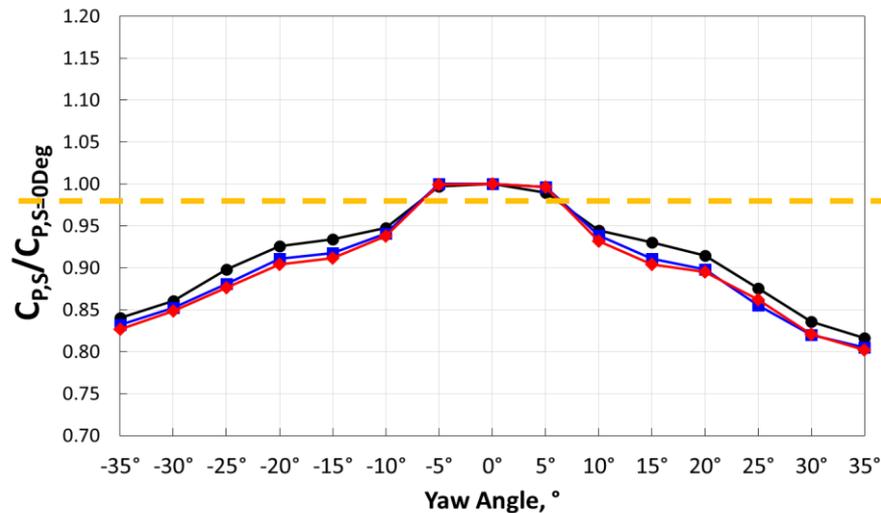
- Three models of L=1.05 S Pitot Cp is increasing as incoming velocity increases



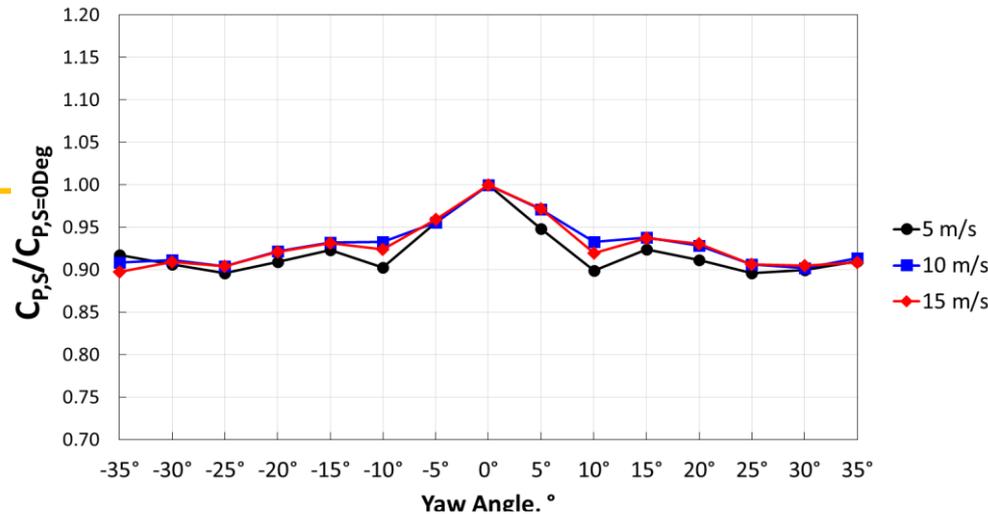
L=1.05D Model (Yaw angle)

- All three models are **sensitive** to yaw angle misalignments

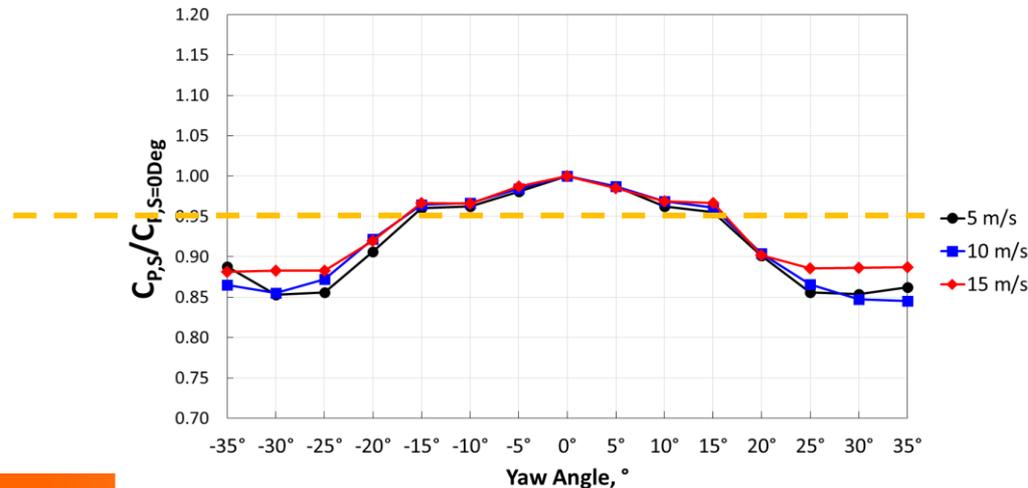
Effect of yaw angle misalignment, L=1.05D, 15Deg



Effect of yaw angle misalignment, L=1.05D, 45Deg



Effect of yaw angle misalignment, L=1.05D, 30Deg



Experiments for the effect of S pitot geometry III

1. Distance between leg base and facing-opening plane (L)

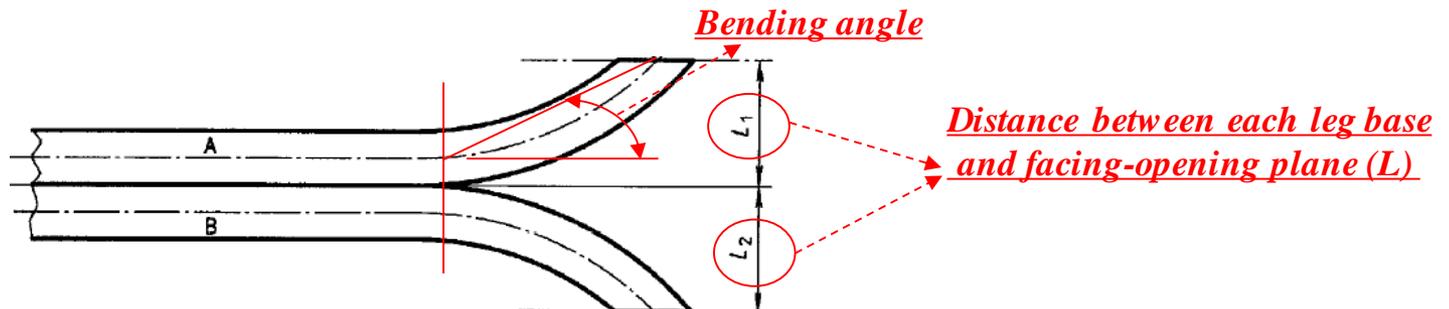
→ $L = 1.05D, 1.6D, 3D$

2. Bending Angle of opening parts

→ $\alpha = 15^\circ, 30^\circ, 45^\circ$

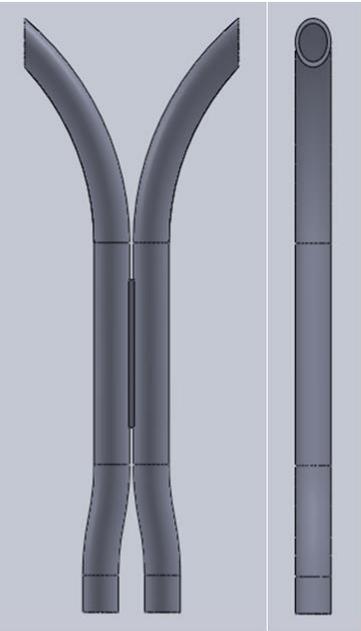
3. Shape of opening parts

→ **Curved**, Straight

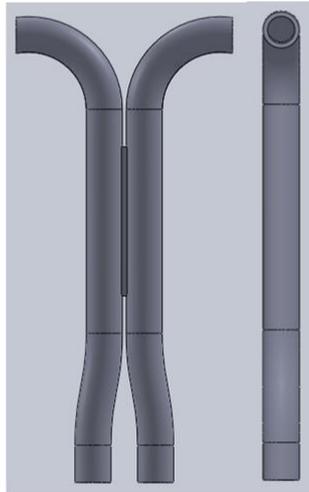


L=3D Models

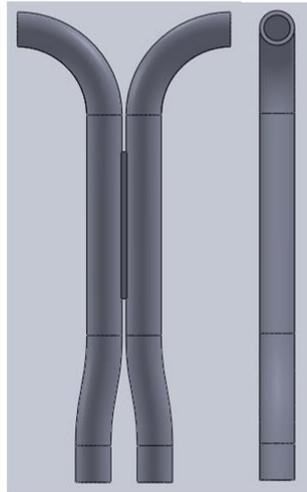
- Compare L=3D models ($\alpha = 15$ Deg., 30 Deg. and 45 Deg.)



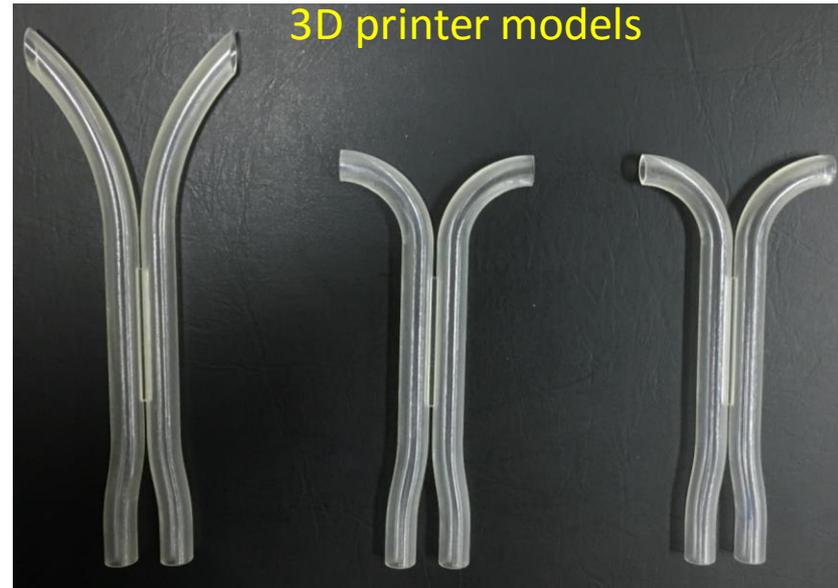
$\alpha = 15^\circ, L = 3D$



$\alpha = 30^\circ, L = 3D$

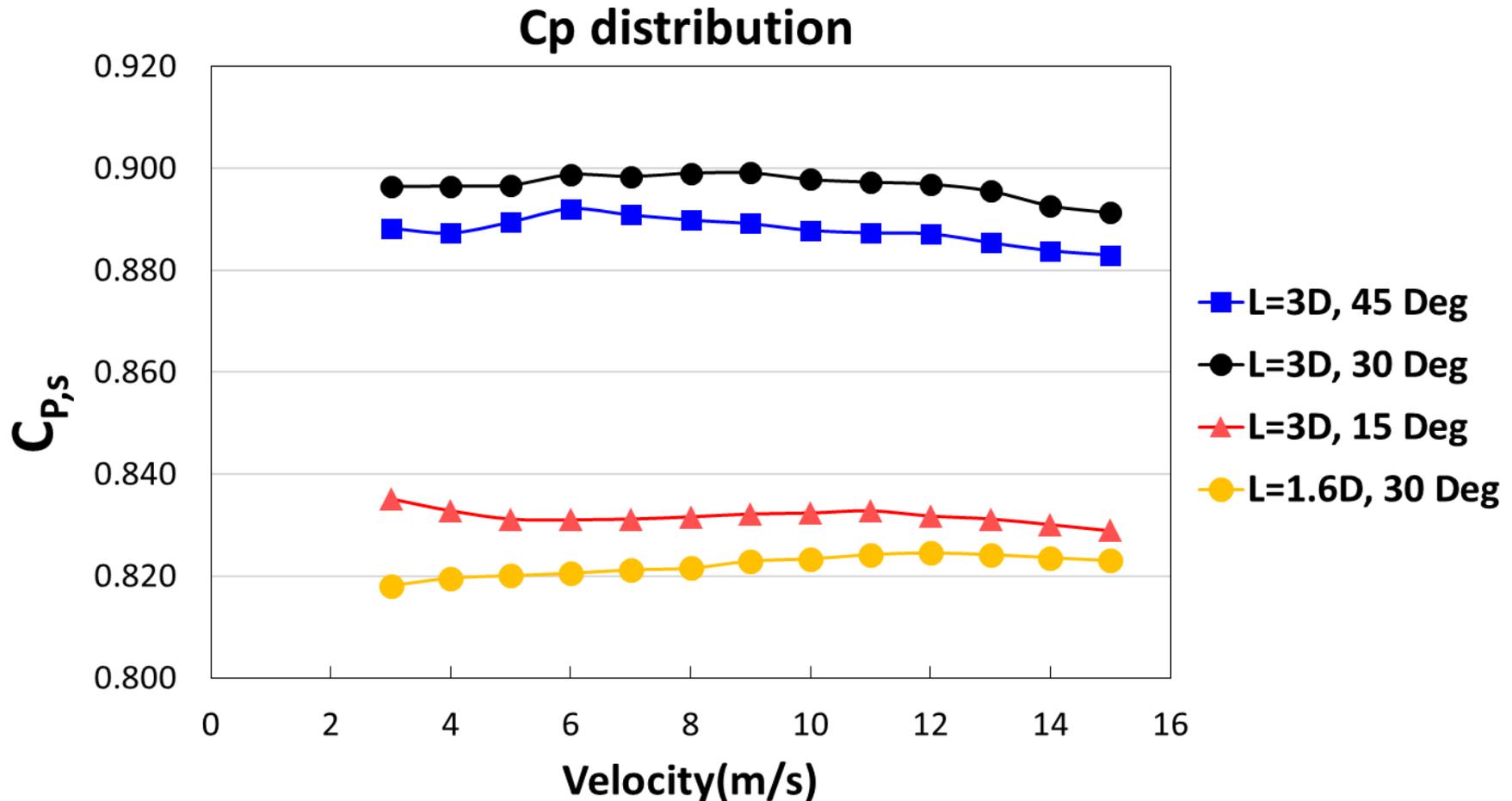


$\alpha = 45^\circ, L = 3D$



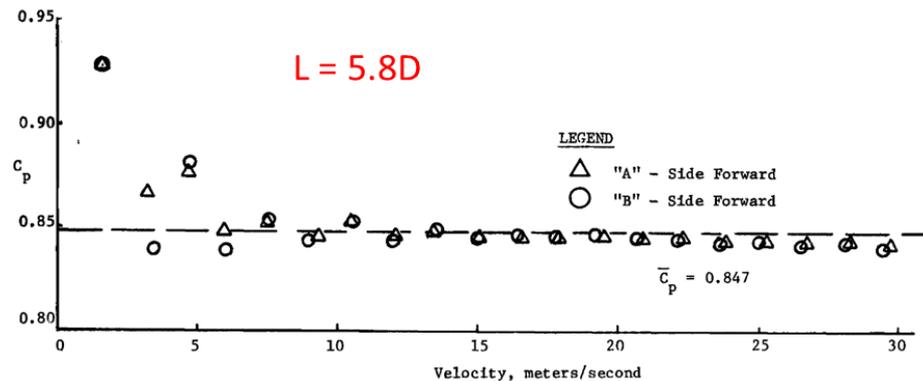
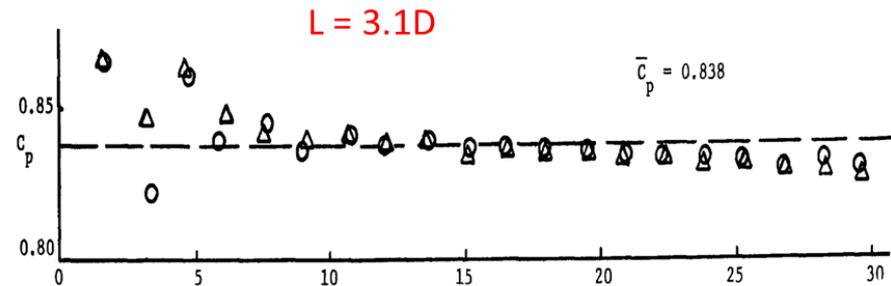
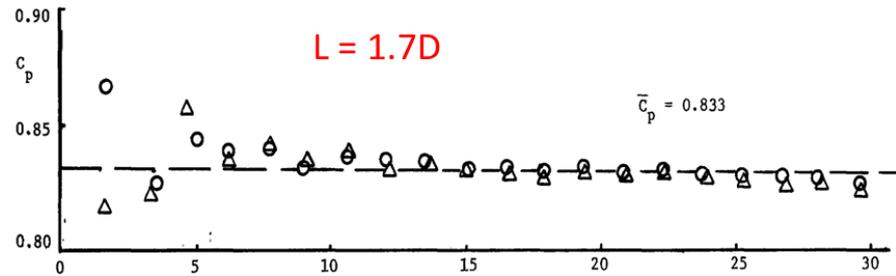
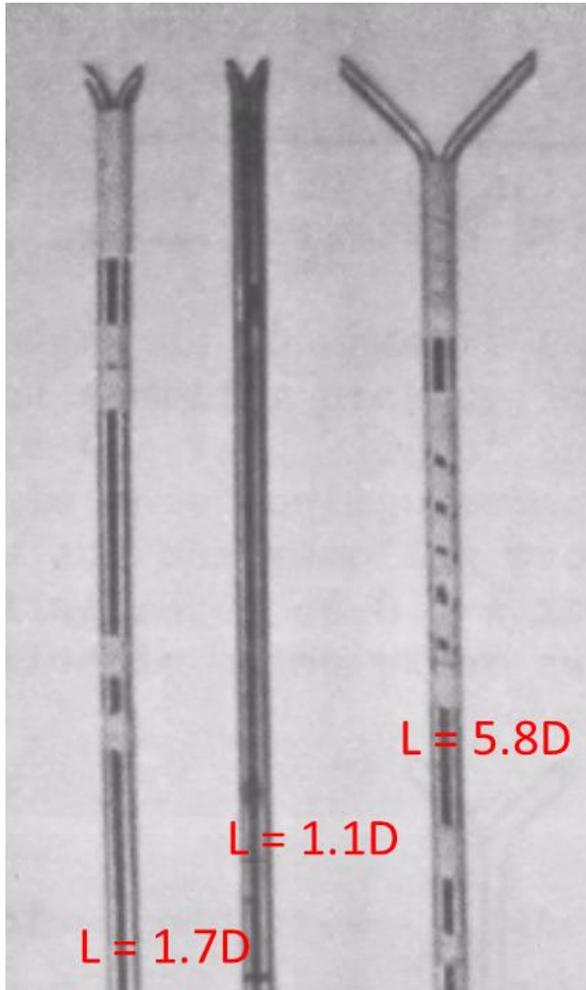
L=3D Models(Cp distribution)

- The $\alpha=15$ and 45° (L=3D) S Pitot has large Cp compared to short L models
- Cp values were almost constant with velocity change



Previous research

- S Type Pitot Tubes, (William, EPA-600, 1977)

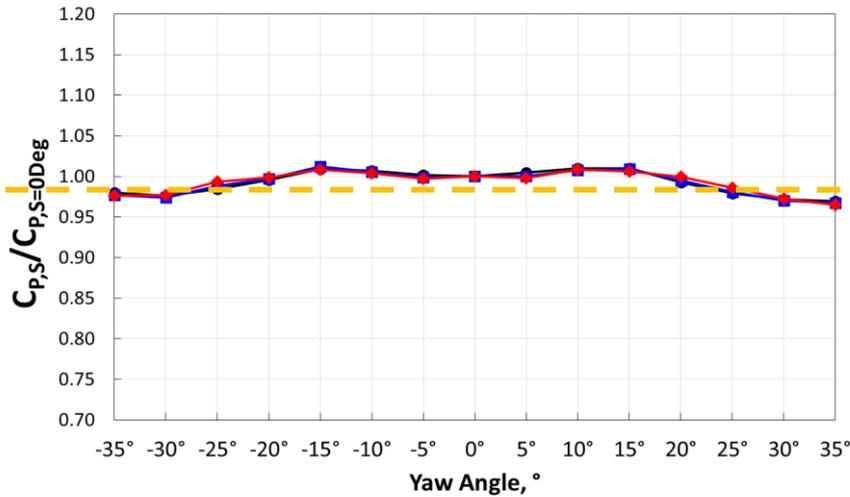


- C_p value increase as Length of S Pitot increase (consistent with present exp

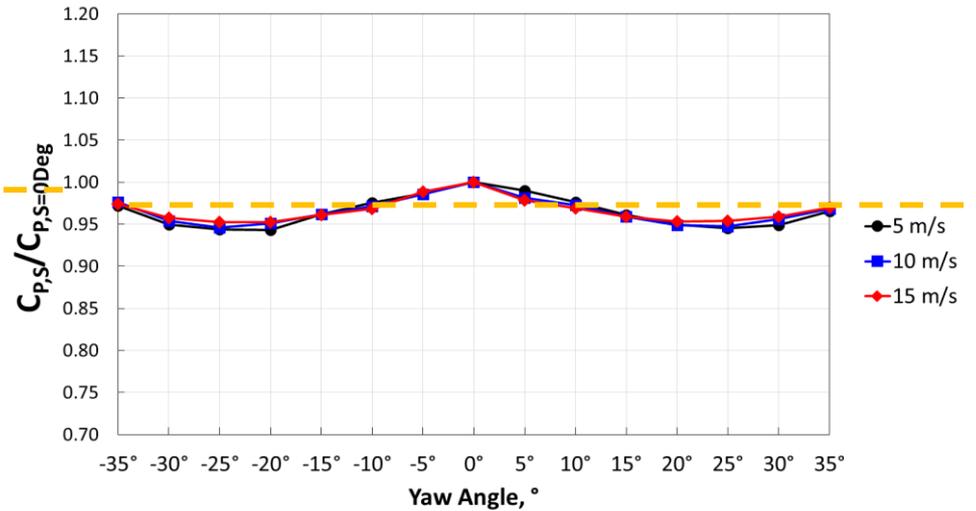
L=3D Model (Yaw angle)

- Three models show **non-sensitive** to yaw angle misalignment

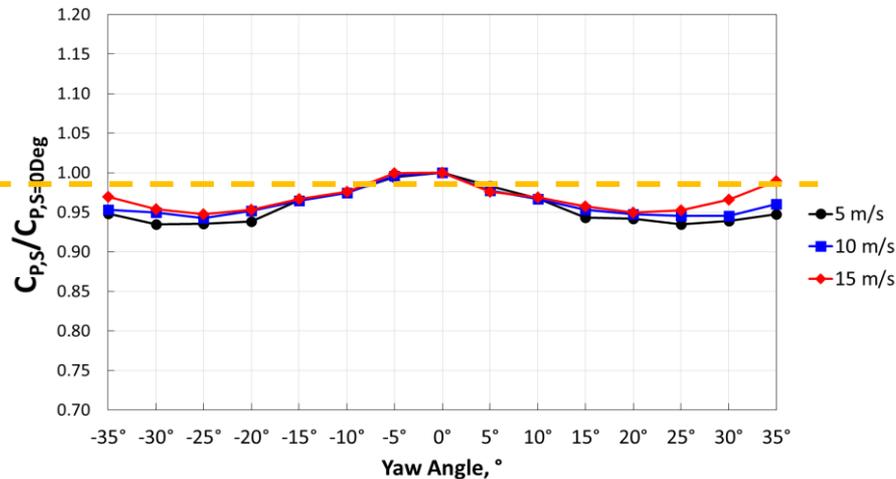
Effect of yaw angle misalignment, L=3D, 15Deg



Effect of yaw angle misalignment, L=3D, 45Deg

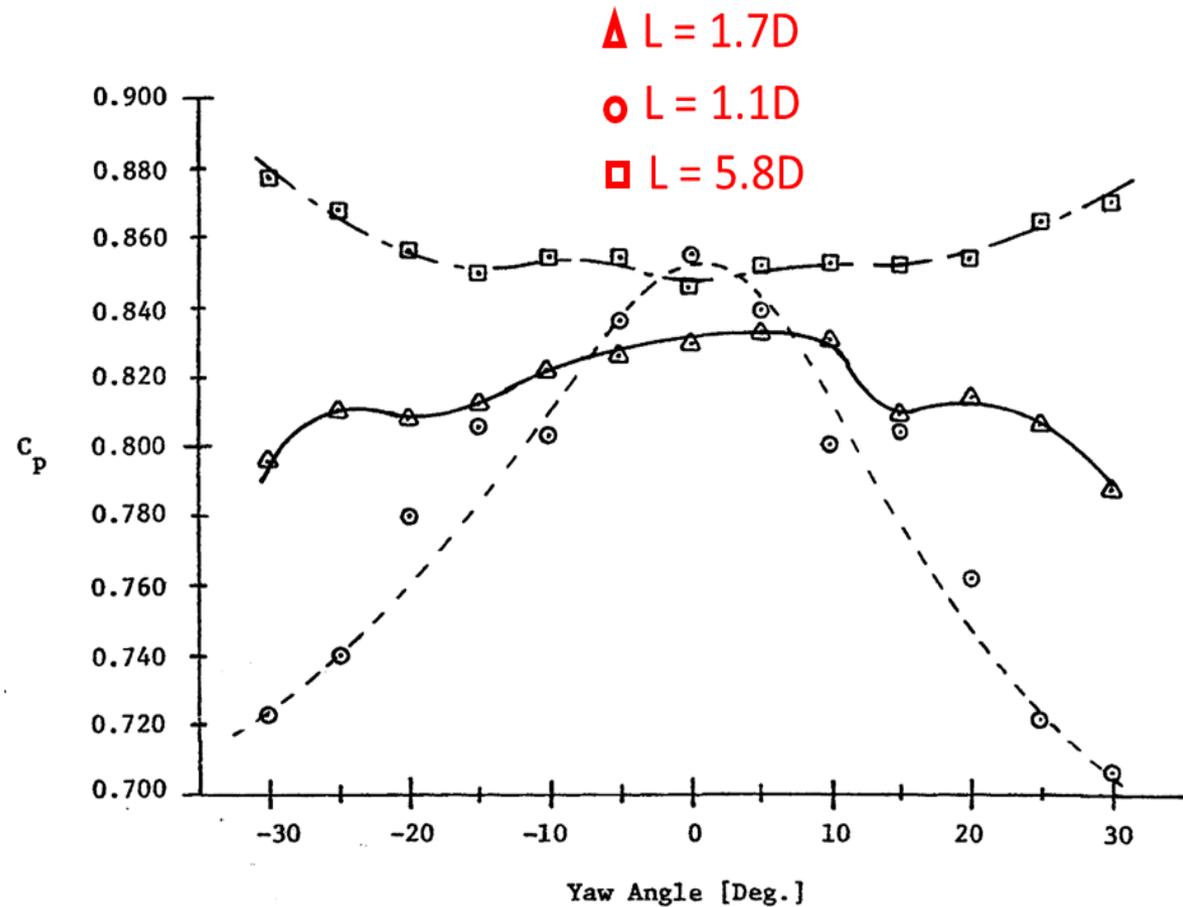
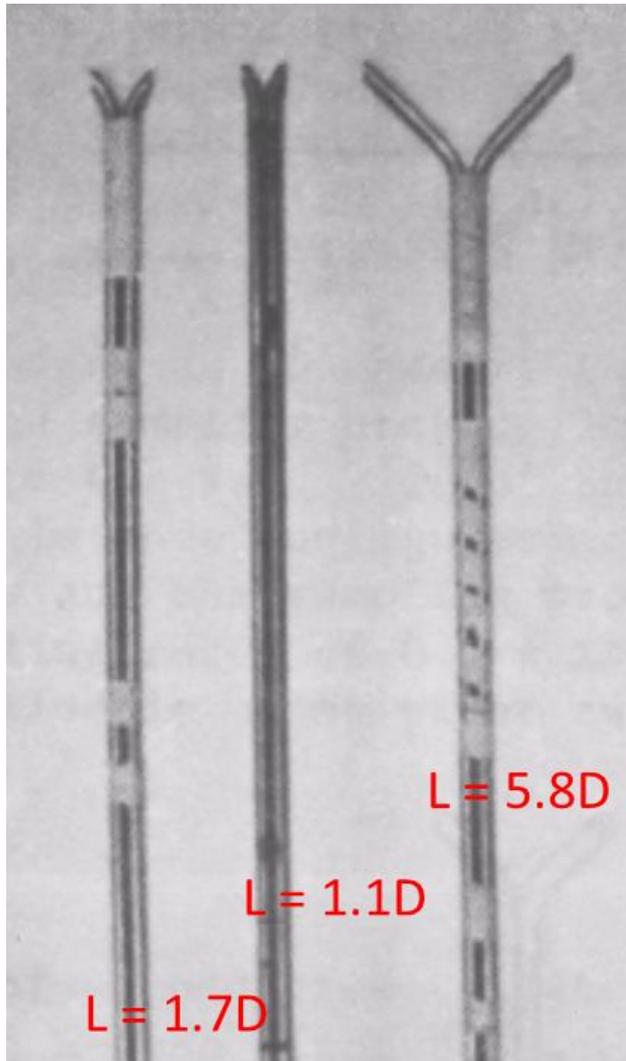


Effect of yaw angle misalignment, L=3D, 30Deg



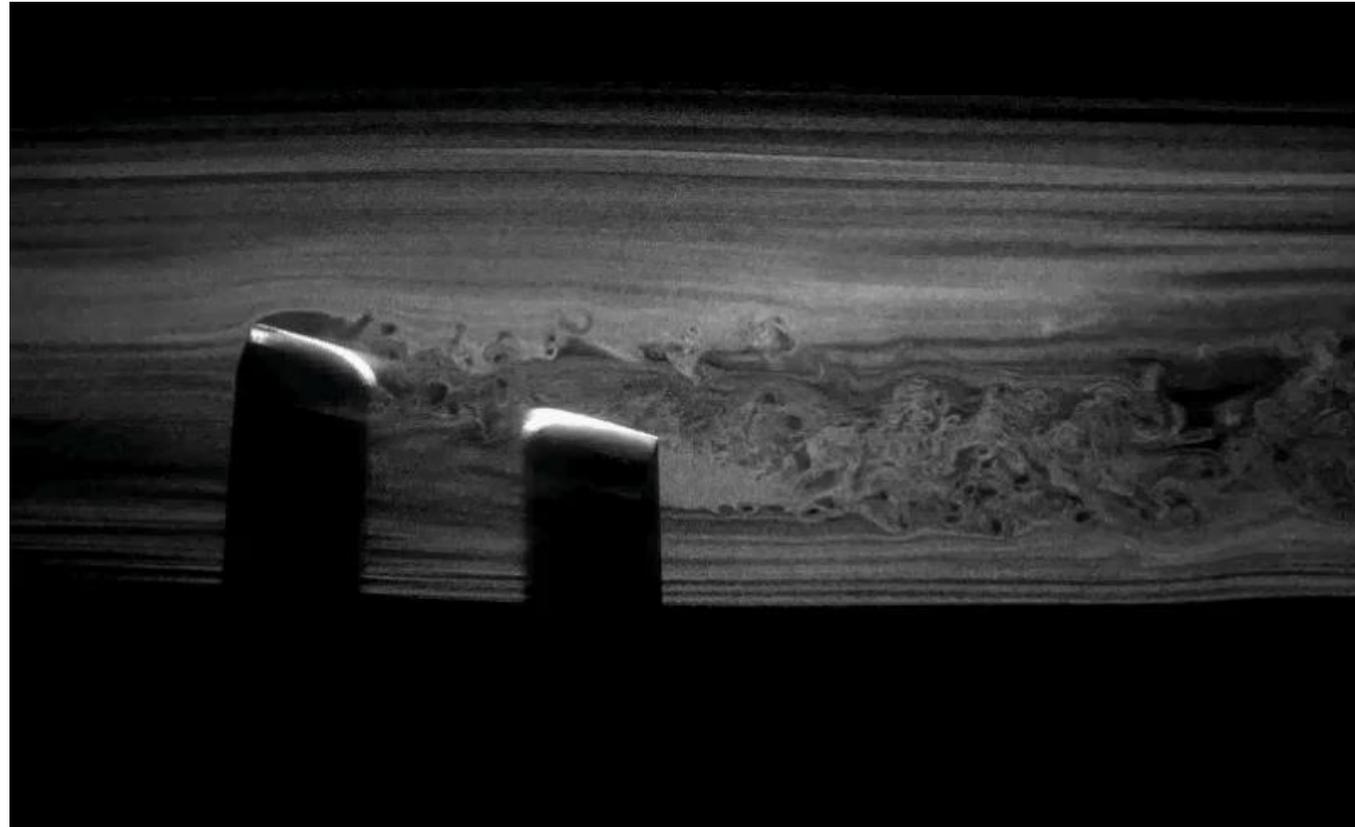
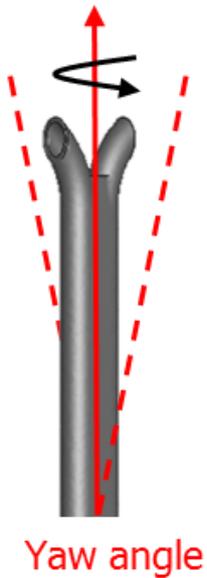
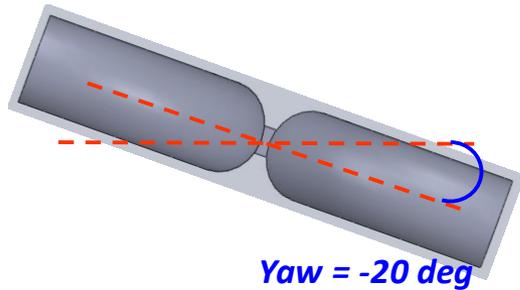
Previous research

- S Type Pitot Tubes, (William, EPA-600, 1977)



L=3D, 30 Deg. (Yaw=-20°) PIV

- Flow phenomenon around S-type Pitot tube (L=3D, 30 Deg.)



- Due to the distance between two orifice, there is less interference for vortical structures of wake orifices

Practical issue for long L model

- The hole size in the stack for installing S-type Pitot tube



Experiments for the effect of S pitot geometry IV

1. Distance between leg base and facing-opening plane (L)

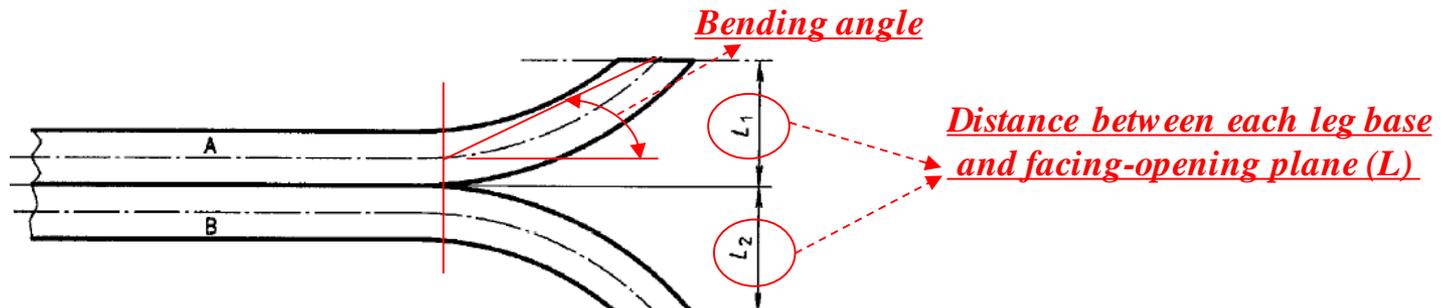
→ $L = 1.05D, 1.6D, 3D$

2. Bending Angle of opening parts

→ $\alpha = 15^\circ, 30^\circ, 45^\circ$

3. Shape of opening parts

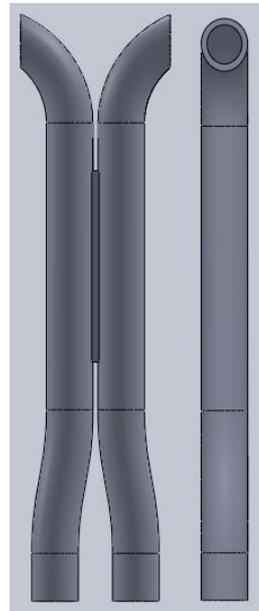
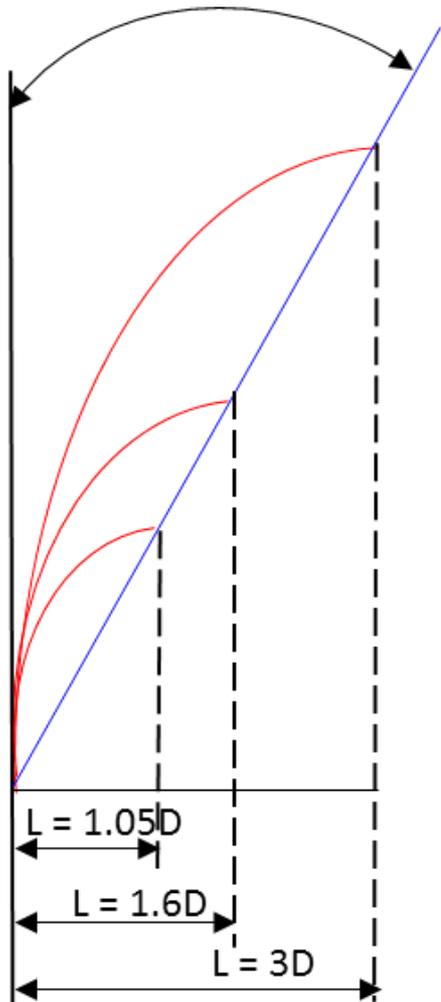
→ **Curved, Straight**



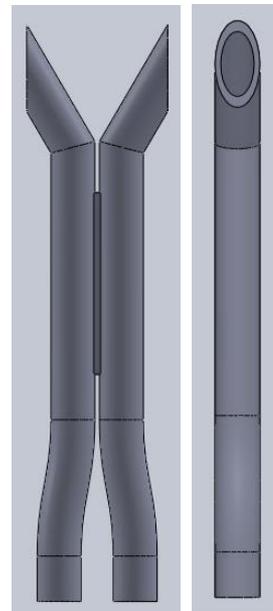
Shape of opening part

- Curved and Straight models ($L=1.6D$, 30 Deg)

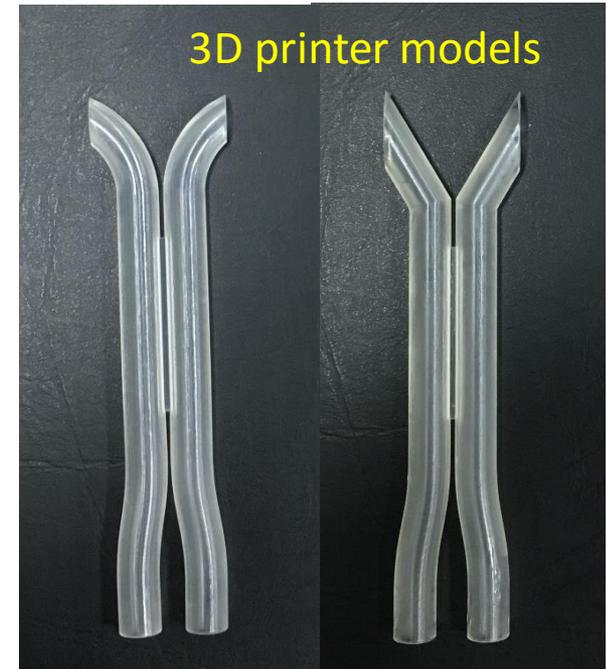
$$\alpha = 30^\circ$$



Curved

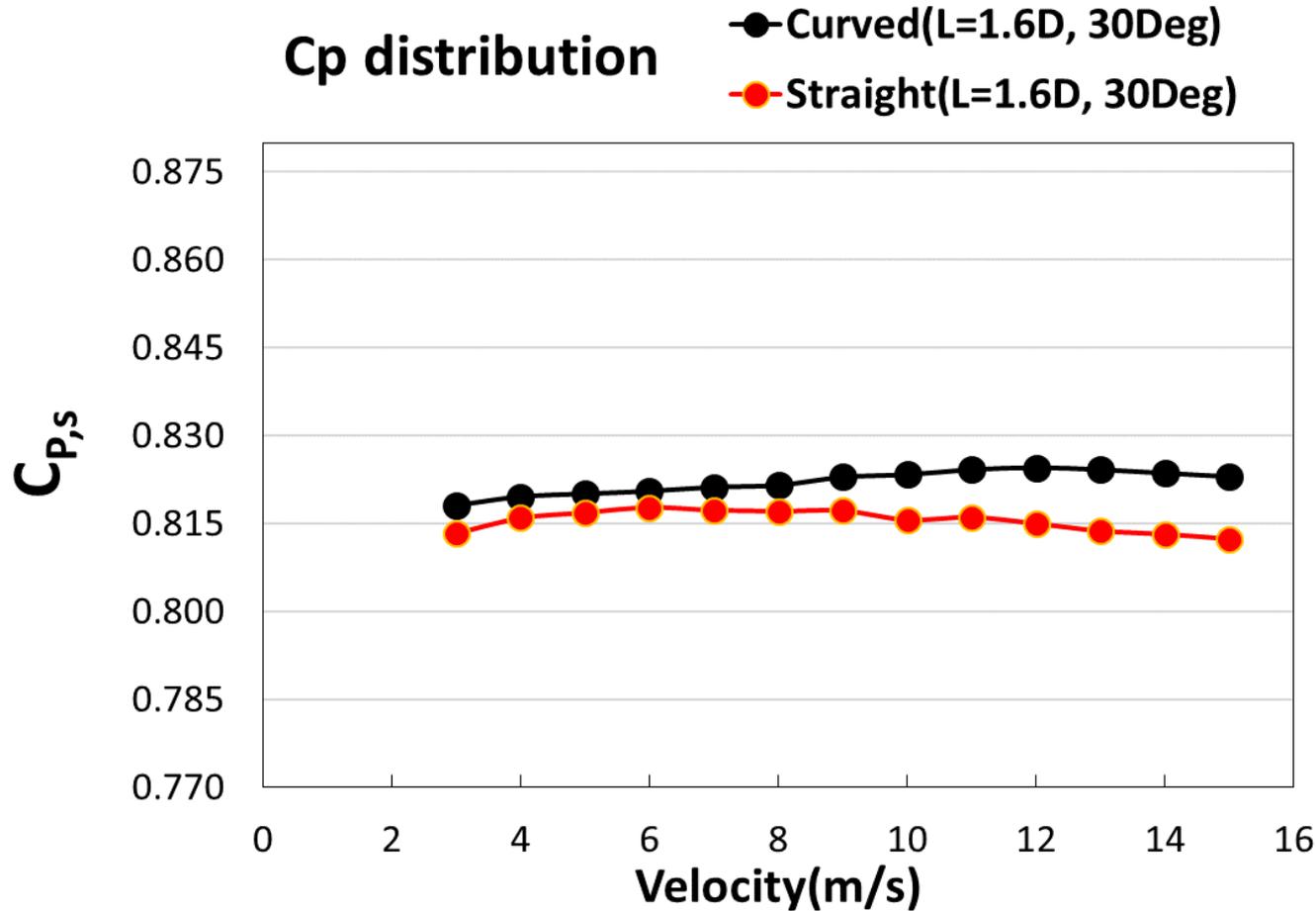


Straight



Cp distribution (Curved vs Straight)

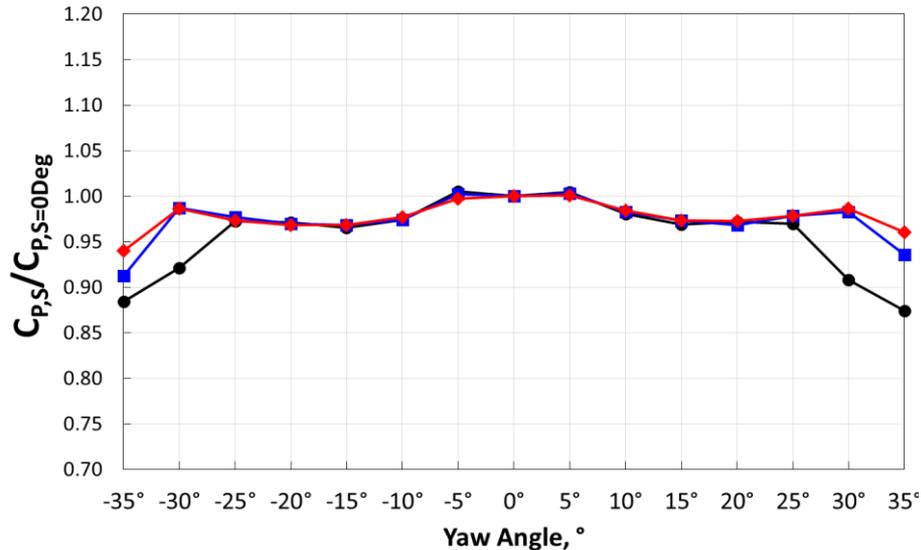
- Cp distribution of Straight model is a little linear compared to Curved model



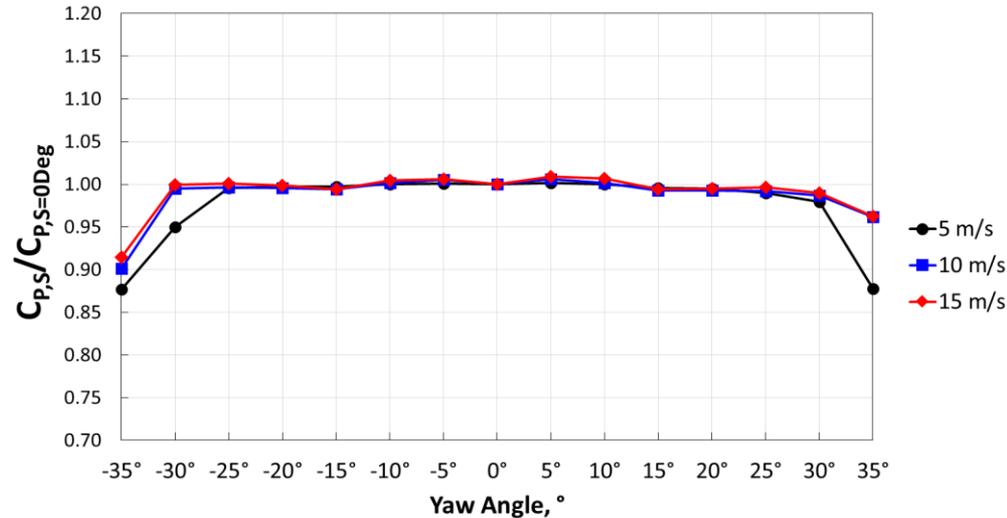
L=1.6D Curved vs Straight (Yaw angle)

- Straight model is **less sensitive** to yaw angle misalignment compare to Curved model

Yaw angle misalignment, **Curved**(L=1.6D, 30Deg)

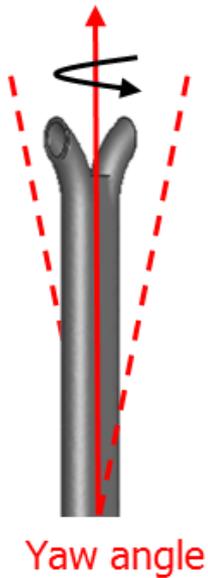
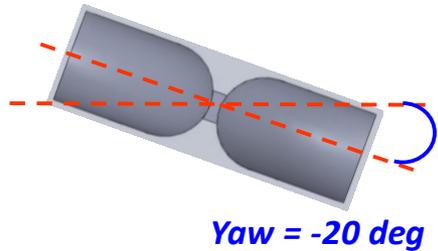


Yaw angle misalignment, **Straight** (L=1.6D, 30Deg)



L=1.6D, 30 Deg. **Straight (Yaw=-20°)** PIV

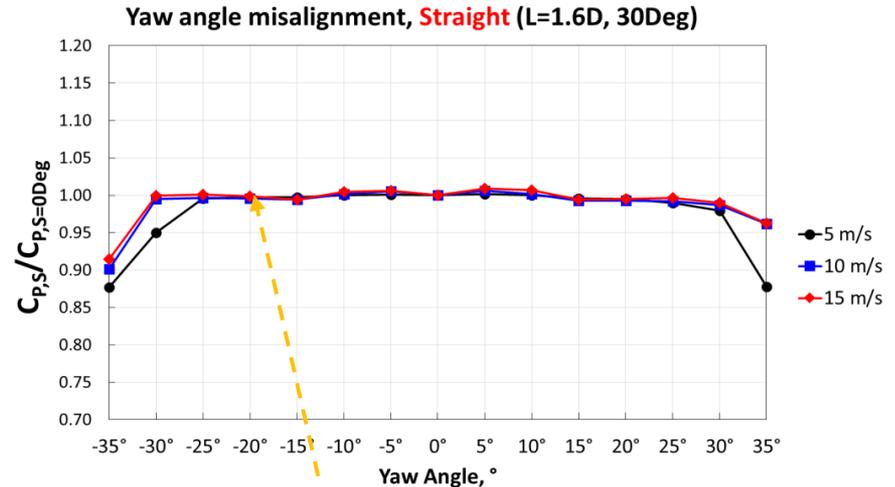
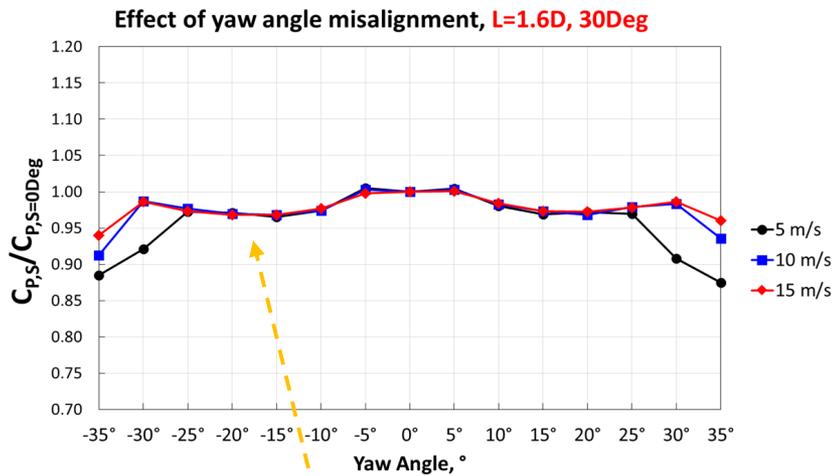
- Flow phenomenon around S-type Pitot tube (L=1.6, 30 Deg. Straight)



- Vortical structures from impact and wake do not affect each other near orifices

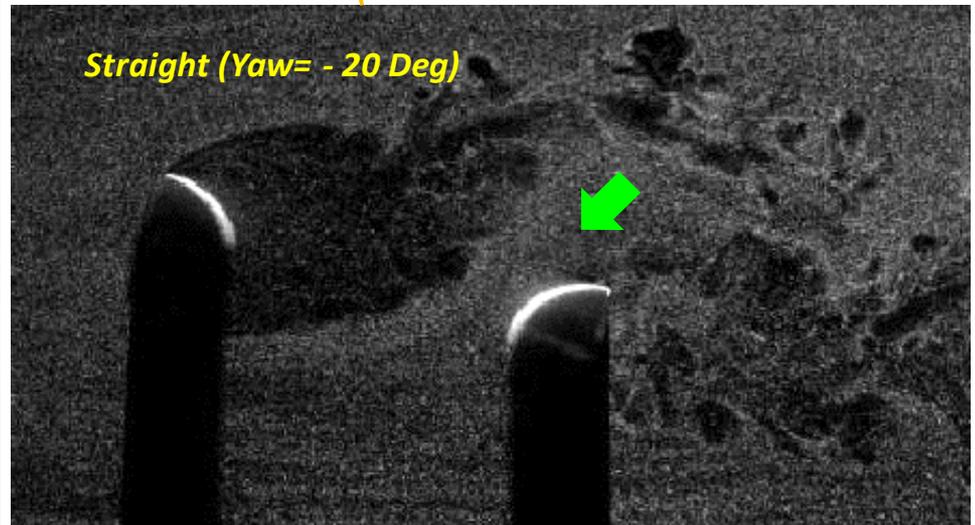
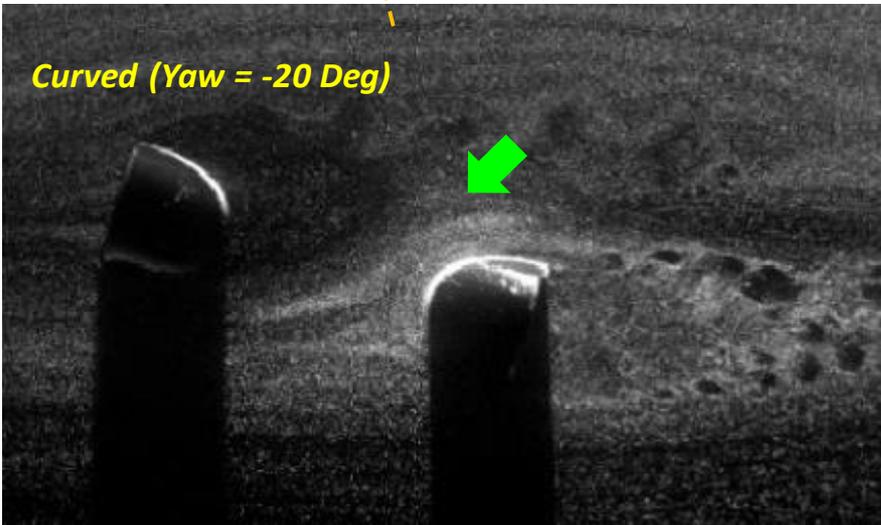
Curved vs Straight (Yaw angle)

- Despite same length ($L=1.6D$), vortical structures from impact and wake do not affect each other near orifices due to difference of opening shape



Curved (Yaw = -20 Deg)

Straight (Yaw = -20 Deg)



Conclusion

- S-type Pitot tube is mainly applied to measurement stack velocity for Smokestack TMS in KOREA
- No detail guideline for manufacturing S-type Pitot tube geometry
- Various geometric parameters on S-type Pitot tube coefficients with yaw and pitch misalignment were investigated by wind tunnel experiments

Conclusion

- S-type Pitot tube is mainly applied to measurement stack velocity for Smokestack TMS in KOREA
- No detail guideline for manufacturing S-type Pitot tube geometry
- Various geometric parameters on S-type Pitot tube coefficients with yaw and pitch misalignment were investigated by 3D printing and wind tunnel experiments
- $L=1.6D$, 30 Deg. Model shows the good linearity of C_p distribution and less sensitivity to yaw angle misalignment
- S-type Pitot tube with Long distance($L=3D$) shows better characteristics than $L=1.6D$. But in the real smokestack, it could be non-practical.
- Straight model are least sensitive to yaw angle misalignment. But for the ideal geometry of S-type Pitot tube in the smokestack, more research is need.

Thank you for your kind attention!



Better Standards, Better Life!
표준이 올라가면, 생활이 즐거워집니다!