



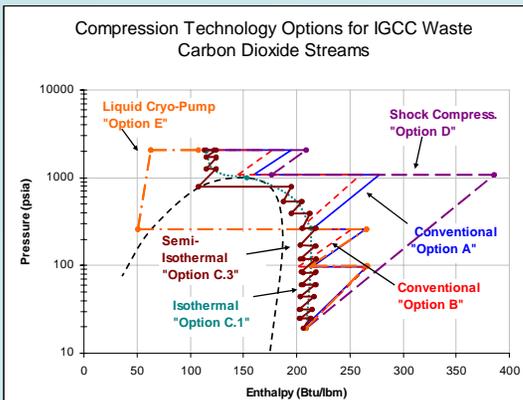
Research and Development Needs for Advanced Compression of Large Volumes of Carbon Dioxide

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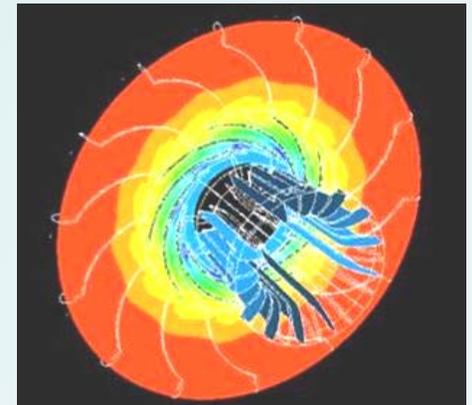
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Workshop on Future Large CO₂ Compression Systems
Sponsored by
DOE Office of Clean Energy Systems,
EPRI, and NIST

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- 170 Buildings



CO₂ R&D Needs

- Reduce the power penalty associated with CCS
- Compression must be integrated and optimized with various capture schemes
 - Amine solvents
 - Chemical looping
 - Membranes
- Reliability of the equipment important
- Beneficial to leverage existing compression technology
- Equation of state near critical point and with mixtures



Motivation of Current Project

- CO₂ capture has a significant compression penalty
- Final pressure around 1,500 to 2,200 psia for pipeline transport or re-injection.
- Based on a 400 MW plant, the typical flow rate is ~600,000 to 700,000 lbm/hr.
- Project goal: Double-digit reduction of compression power for CO₂ capture
- Many thermodynamic processes studied.
- Several challenges with the application discussed.
- Research applicable to PC, Oxy-Fuel, IGCC & NGCC

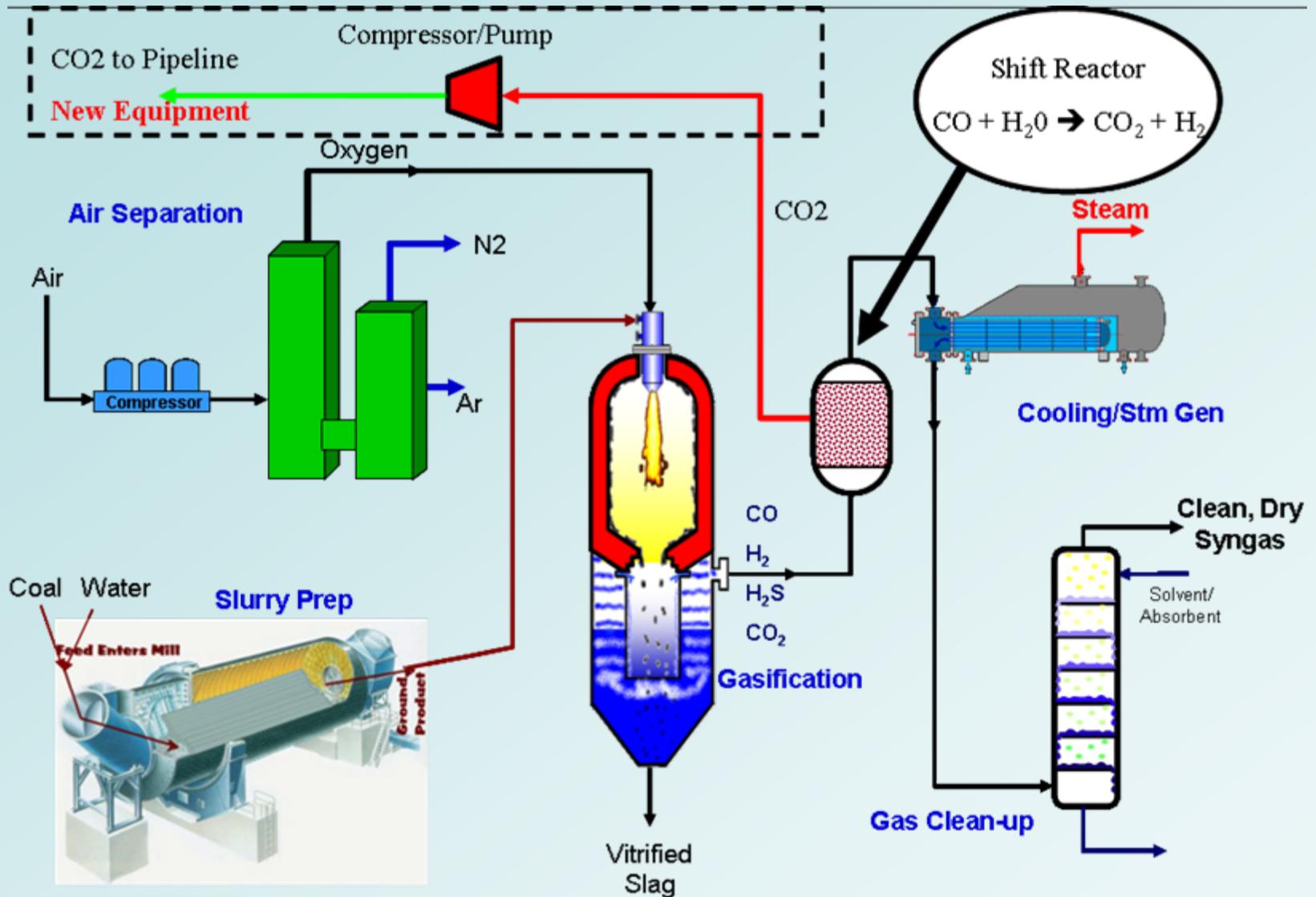


General Comments

- The type of compressor is highly dependent on the starting pressure
 - Approximately 20 to 500 psia for CO₂ scrubbing of the fuel stream (for IGCC).
 - Approximately 15 psia from PC and Oxy-Fuel.
- High pressure ratio results in significant heat of compression.
- Various compressor types have been considered.
- Isothermal compression - one concept considered to reduce the power of compression.
- Liquefaction of CO₂ has also been studied.



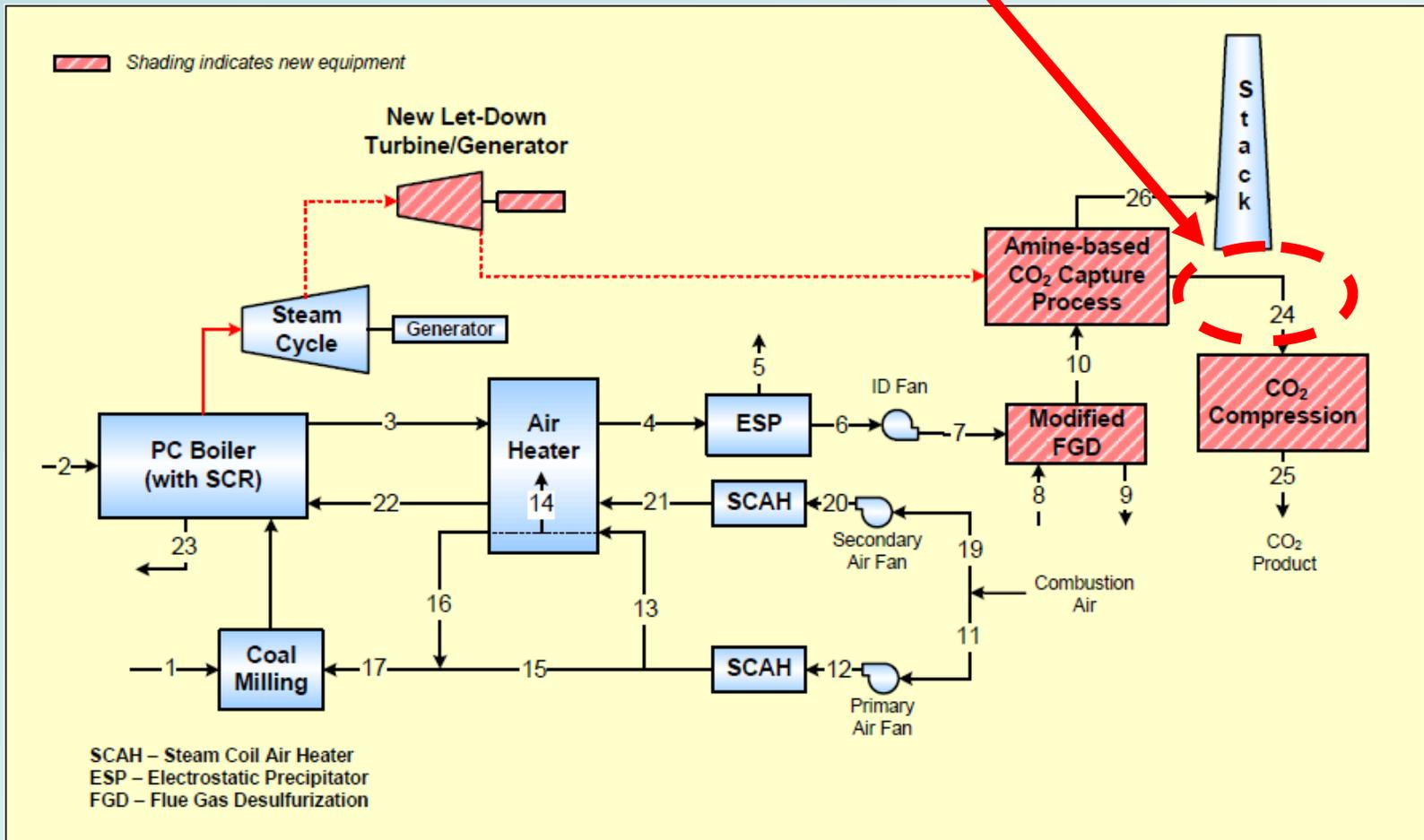
IGCC Process with Carbon Capture





DOE PC Reference Case

- Only CO₂ stream considered

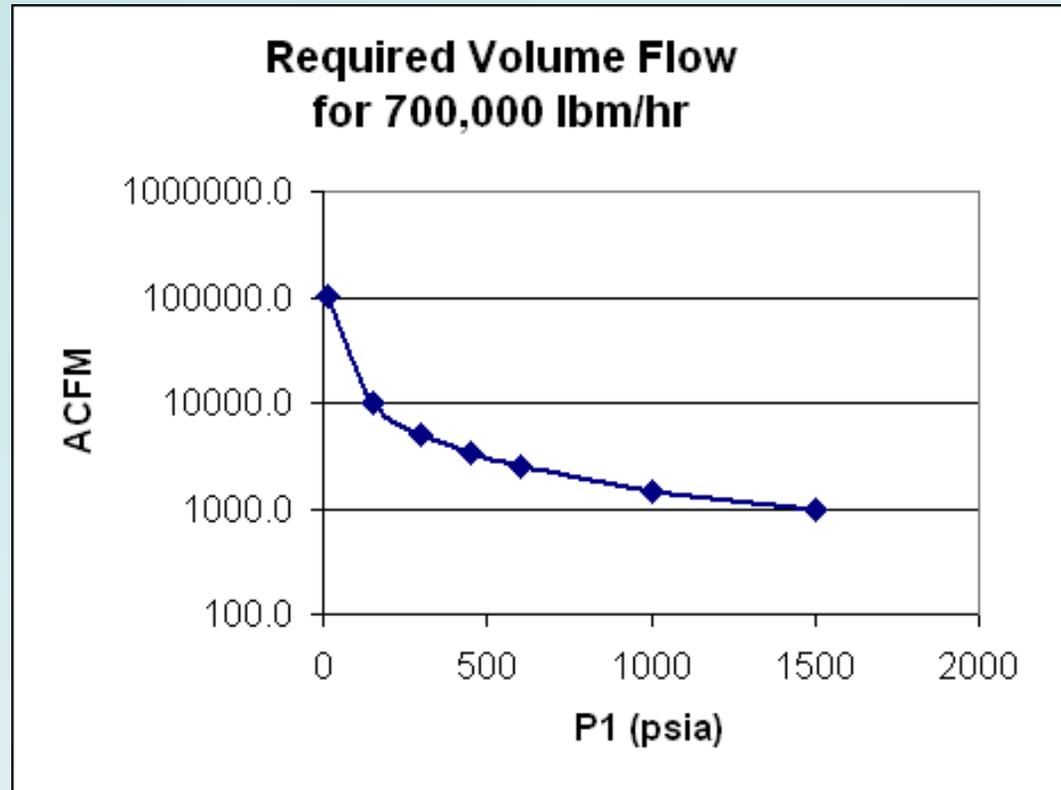




Challenges: Volume Reduction

Mass Flow Rate = 700,000 lbm / hr = 144.89 MMSCFD

Pressure (psia)	Volume Flow (acfm)
14.7	100,595.2
150	9,858.3
300	4,929.2
450	3,286.1
600	2,464.6
1,000	1,478.8
1,500	985.8



High volume flow reduction adds to challenge in compressor selection



Challenges: Multiple Streams

- Uncompressed CO₂ streams in a typical IGCC plant with a physical absorption separation method using Selexol solvent.

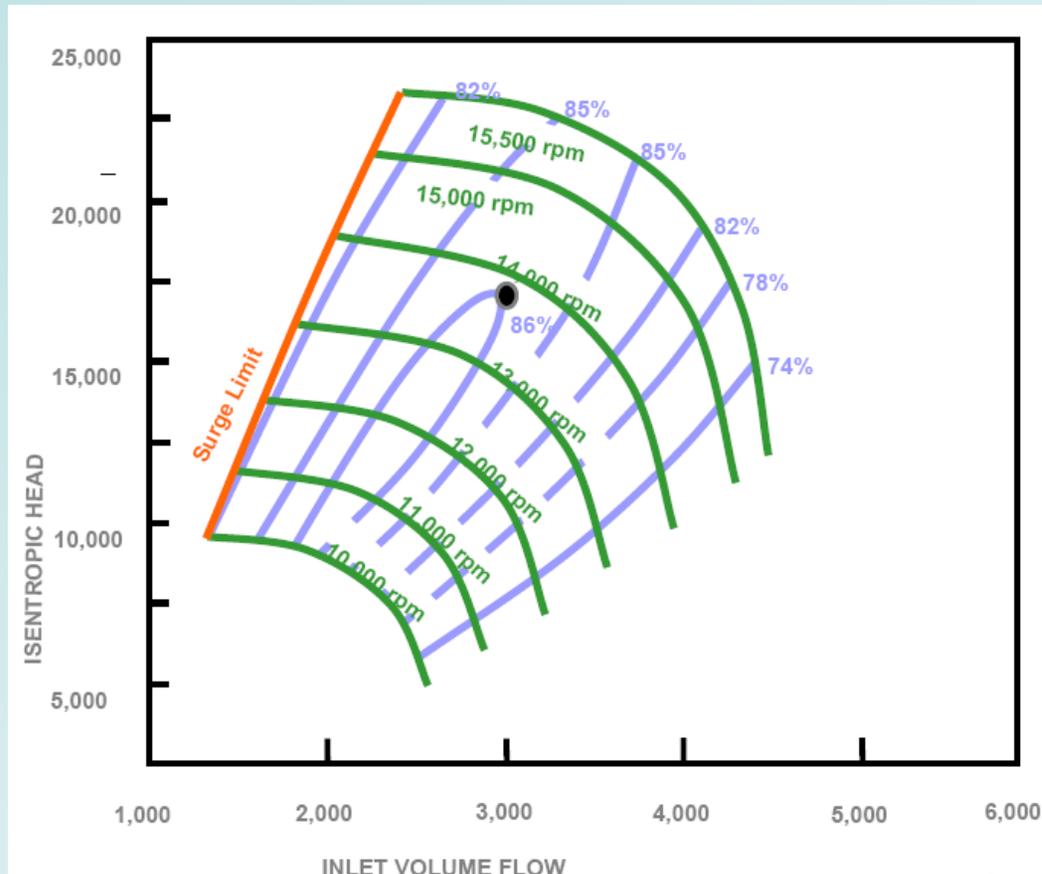
CO₂ Gas Streams	LP	MP	HP 1	HP 2
Pressure (psia)	21.9	160.0	250.0	299.0
Temperature (°F)	51.0	68.0	90.0	75.0
Density (lbm/ft ³)	0.177	1.3	1.87	2.088
Flow Rate (acfm)	33,257	2,158	3,374	1,073

Higher pressure separation streams help reduce volume reduction. This allows a more uniform frame size in compressor selection.



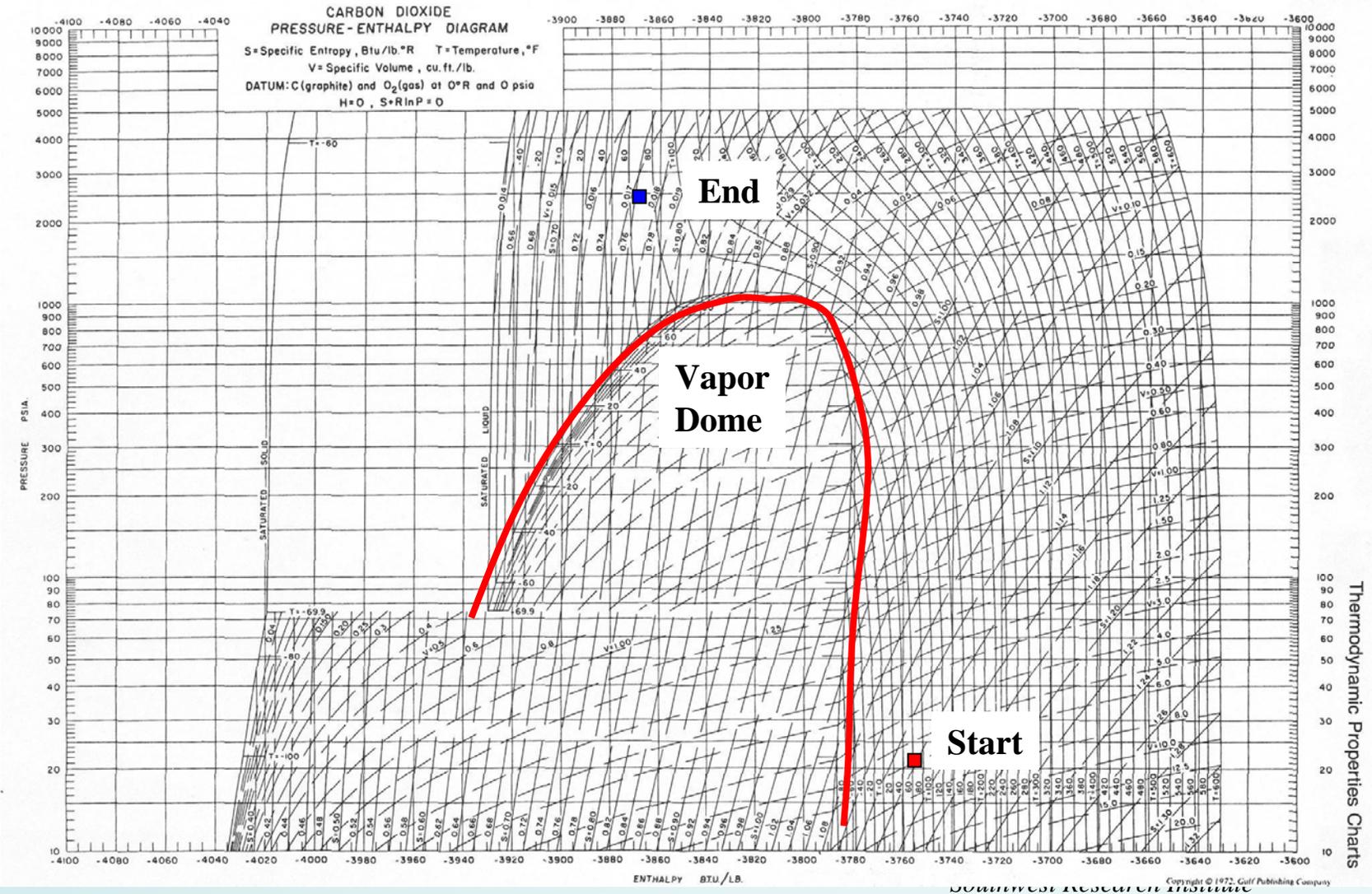
Challenges: Wide flow range required

- CO₂ mass flow proportional to power plant Output (e.g. 50-100%)





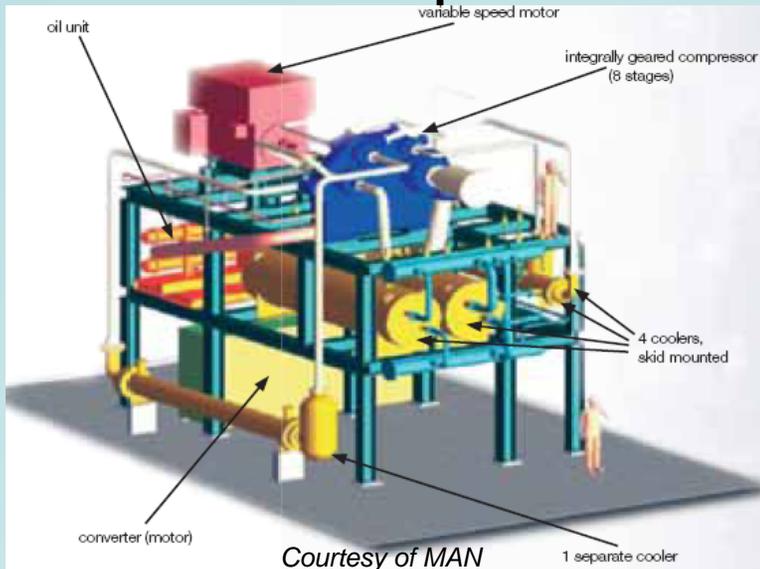
Challenges: High Mole Weight





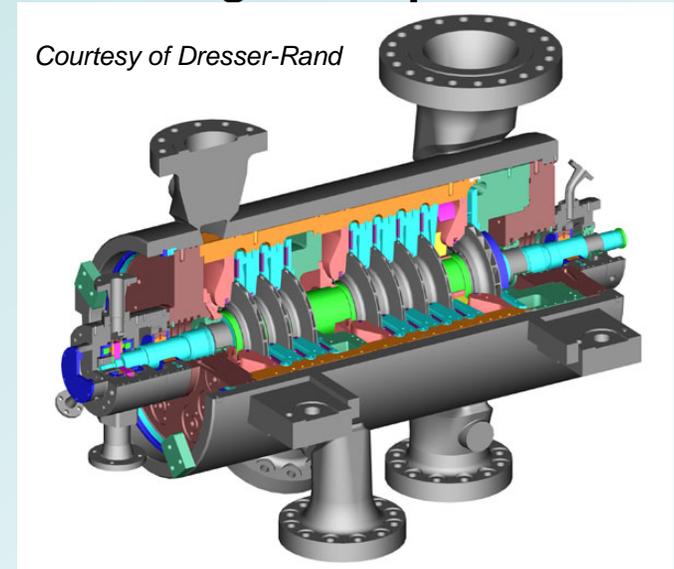
Challenges: High Reliability

Integrally Geared Isothermal Compressor



- Integrally geared can achieve near isothermal compression
- Can contain up to 12 bearings, 10 gas seals plus gearbox
- Typically driven by electric motor
- Impellers spin at different rates
 - Maintain optimum flow coef.

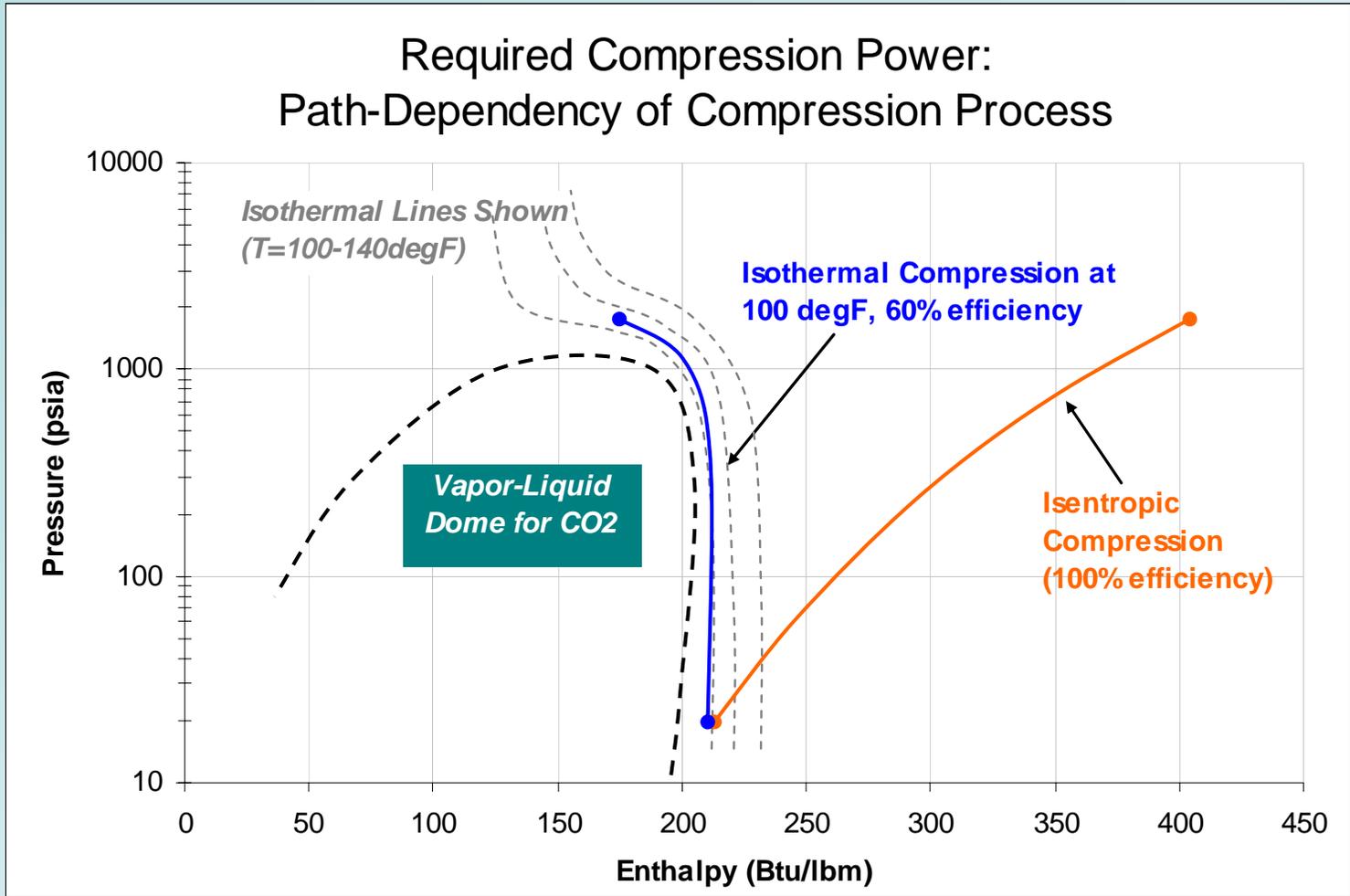
Single-Shaft Multi-stage Centrifugal Compressor



- Multi-stage centrifugal proven reliable and used in many critical service applications currently (oil refining, LNG production, etc.)
- Fewer bearings and seals
 - (4 brgs & seals for 2 body train)
- Can be direct driven by steam turbine



Path Dependent Process Comparison



Comparing a 60% isothermal compressor to a 100% efficient isentropic compressor...Which is better???



Isentropic vs. Isothermal Compression

Isentropic Compression Calculations for 20-2200 psia										
P1	P2	T1	T2	h1	h2	rho1 (lbm/ft3)	rho2 (lbm/ft3)	Polytropic Efficiency	W/mdot (Btu/lbm)	BHP
20	220	70	415	216.05	290.92	0.156	1.0446	0.99	74.870	5879.6
220	2200	415	875	290.92	404.12	1.0446	6.6665	1.00	113.200	8889.6
									Mdot (lb/hr)=	200000
									Mdot (lb/hr)=	200000
									Total BHP =	14769.2

Isothermal Compression Calculations at 100 degF and 60% efficiency										
Low Pressure									Mdot (lb/hr)=	200000
P1	P2	To	P2/P1	In (P2/P1)	Ideal W/mdot (Btu/lbm)	Assumed Efficiency	Actual W/mdot (Btu/lbm)	BHP		
20	100	100	5.00	1.61	37.62	0.600	62.705	4924.2		
Side Stream + Medium Pressure									Mdot (lb/hr)=	200000
100	260	100	2.60	0.96	21.28	0.600	35.461	2784.8		
170	260	100	1.53	0.42	9.32	0.600	15.541	1220.4		
High Pressure									Mdot (lb/hr)=	200000
260	600	70	2.31	0.84	16.41	0.600	27.344	2147.3		
600	1097	70	1.83	0.60	6.50	0.600	10.841	851.4		
1097	2200	70	2.01	0.70	3.92	0.600	6.536	513.3		
									Total BHP =	12441.4

Isentropic Compression
(100% efficiency) = 14,769 BHP

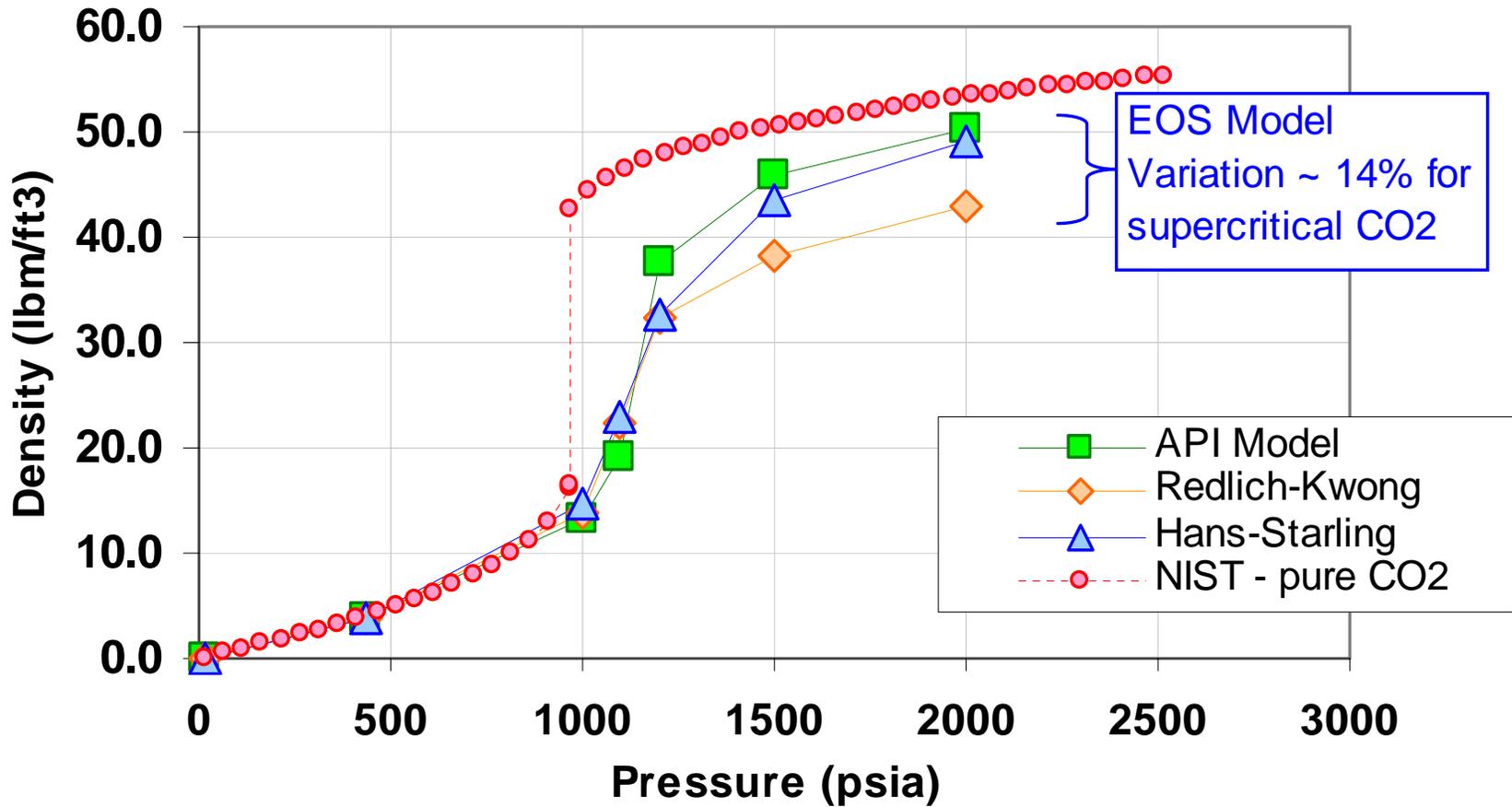
Isothermal Compression
(60% efficiency) = 12,441 BHP

The 60% efficient isothermal compressor is preferred.



Deviation in Models for CO₂ Mixtures

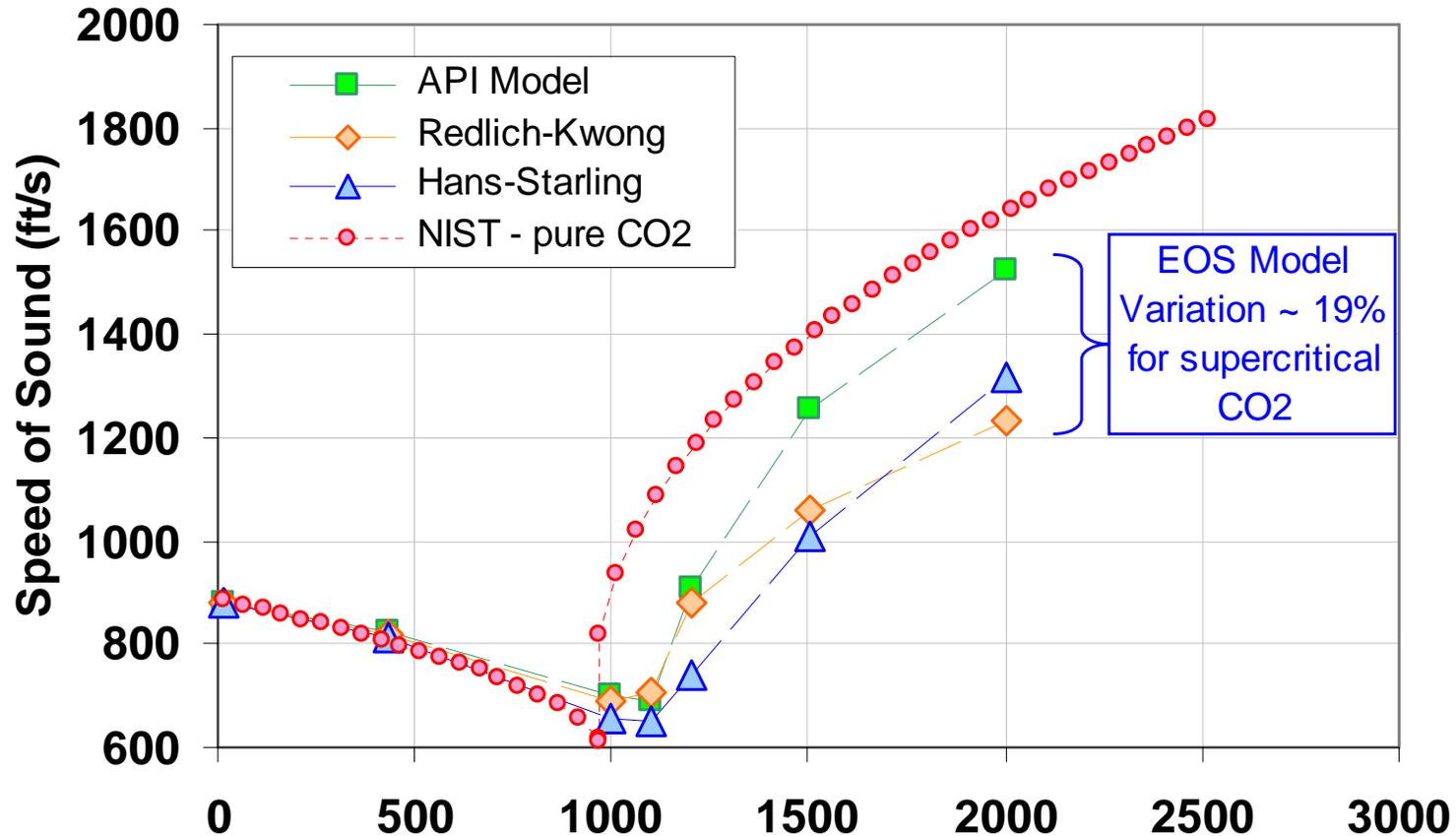
Variation in Predicted Gas Density for CO₂ Mixture





Deviation in Models for CO₂ Mixtures

Variation in Predicted SOS for CO₂ Mixture



Large differences exist in gas properties predicted by standard equation of state models (API, RKS, HANS) and pure CO₂ correlation models from 1000-2000 psia.



Gas Properties Testing

- Gas properties testing for acid gas at SwRI
- Molecular weight and speed of sound





Back to Current Project



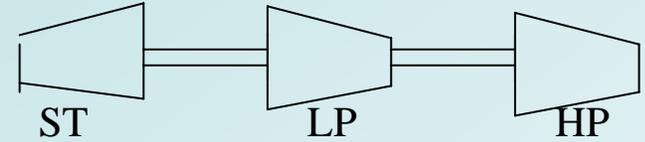
Project Overview

- Phase I (Completed)
 - Perform thermodynamic study to identify optimal compression schemes
- Phase II (Complete in 2010)
 - Pilot testing of two concepts:
 - Isothermal compression
 - Liquid CO₂ pumping
 - Total Project Amount \$1.5 million



D-R Selection Using Conventional Centrifugal Compressors (Baseline)

- Requires two parallel trains
- Intercooling between each section



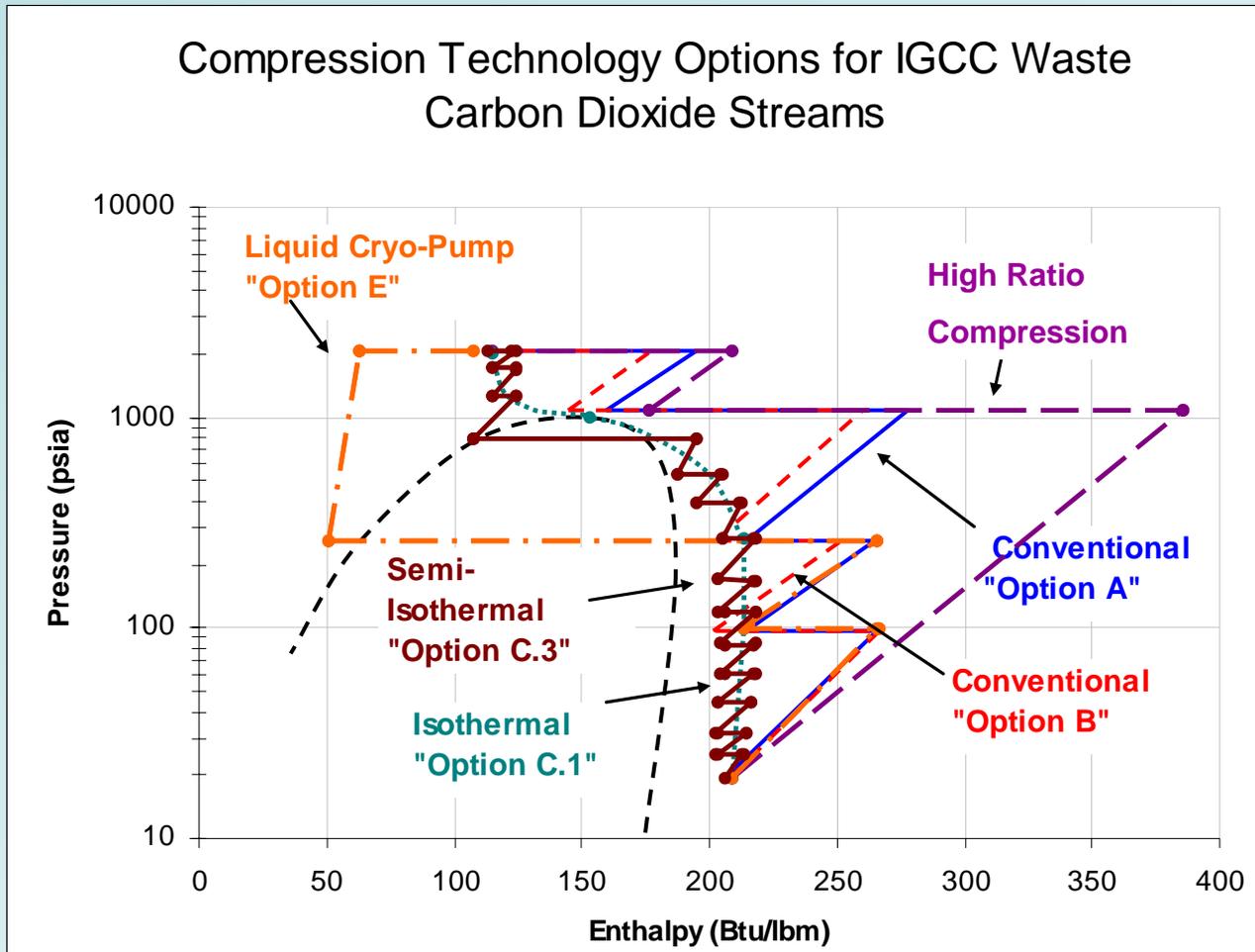
OPERATING CONDITIONS	
9	
10	
11	(ALL DATA ON PER UNIT BASIS)
12	
13	
14	● GAS HANDLED (ALSO SEE PAGE)
17	● WEIGHT FLOW, (Lb/Hr) (WET)
18	INLET CONDITION
19	● PRESSURE (PSIA)
20	● TEMPERATURE (°F)
22	● MOLECULAR WEIGHT
25	■ INLET VOLUME, (ACFM)(WET)
26	DISCHARGE CONDITI
27	● PRESSURE (PSIA)
28	■ TEMPERATURE (°F)
29	■ Cp/Cv(Kavg)
30	■ COMPRESSIBILITY (ZAvg)
36	
37	■ GHP REQUIRED (HP)
40	■ SPEED (RPM)

Base				
D18R7B			D16R9B	
SEC #1	SS In	SEC #2	SEC #1	SEC #2
LP	MP		Blend	
176,649	168,445	260,872	517,475	517,475
21.90	170.0	96.58	248.0	1,087
51.00	68.00	90.21	100.00	100.0
43.88	43.13	43.63	41.61	41.61
16,634		5,908	4,694	745.0
106.6		258.0	1,097	2,215
299.3		258.1	369.8	231.4
1.271		1.272	1.274	1.230
0.9910		0.9685	0.9334	0.6919
3,684		3,656	12,126	5,180
		5,166		

Total Power = 49,292 HP (37 MW, 5.2% of 700 MW Output)



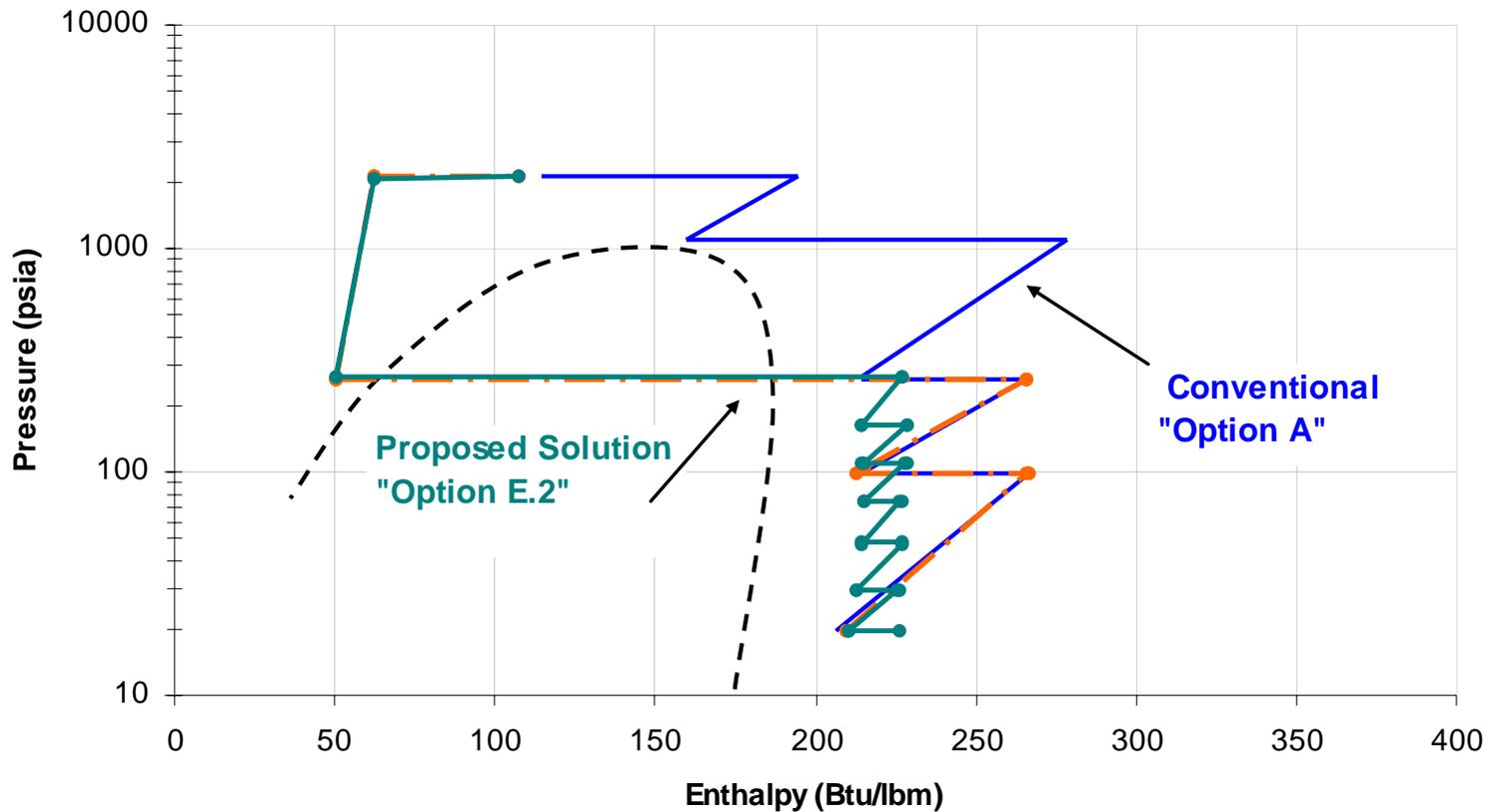
Summary of Thermodynamic Analysis





Proposed Solution for Optimal Efficiency

Compression Technology Options for IGCC Waste Carbon Dioxide Streams



Optimal solution combines inter-stage cooling and a liquefaction approach.



Summary of Thermodynamic Analysis

Option	Compression Technology	Power Requirements	% Diff from Option A	Cooling Technology
A	Conventional Dresser-Rand Centrifugal 10-stage Compression	23,251 BHP	0.00%	Air-cool streams between separate stages
B	Conventional Dresser-Rand Centrifugal 10-stage Compression with additional cooling	21,522 BHP	-7.44%	Air-cool streams between separate stages using ASU cool N2 stream
C.1	Isothermal compression at 70 degF and 80% efficiency	14,840 BHP	-36.17%	Tc = 70 degF inlet temp throughout
C.4	Semi-isothermal compression at 70 degF, Pressure Ratio ~ 1.55	17,025 BHP (Required Cooling Power TBD)	-26.78%	Tc = 70degF in between each stage.
C.7	Semi-isothermal compression at 100 degF, Pressure Ratio ~ 1.55	17,979 BHP (Required Cooling Power TBD)	-22.67%	Tc = 100degF in between each stage.



Summary of Thermodynamic Analysis

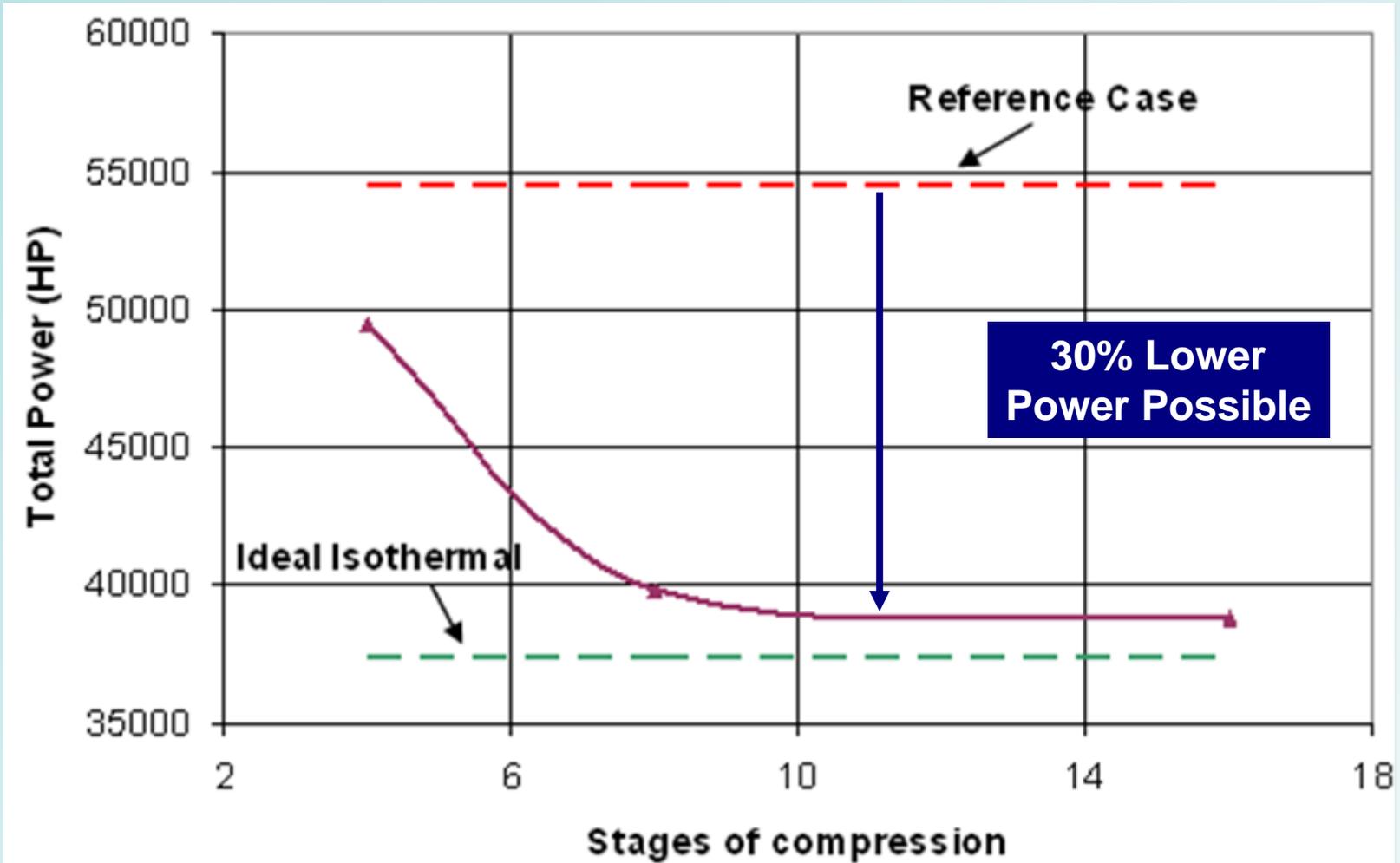
Option	Compression Technology	Power Requirements	% Diff from Option A	Cooling Technology
D.3	High ratio compression at 90% efficiency - no inter-stage cooling	34,192 BHP	47.06%	Air cool at 2215 psia only
D.4	High ratio compression at 90% efficiency - intercooling on final compression stage	24,730 BHP	6.36%	Air cool at 220 and 2215 psia
E.1	Centrifugal compression to 250 psia, Liquid cryo-pump from 250-2215 psia	16,198 BHP (Includes 7,814 BHP for Refrigeration) ¹	-30.33%	Air cool up to 250 psia, Refrigeration to reduce CO ₂ to -25degF to liquify
E.2	Centrifugal compression to 250 psia with semi-isothermal cooling at 100 degF, Liquid cryo-pump from 250-2215 psia	15,145 BHP (Includes 7,814 BHP for Refrigeration) ¹	-34.86%	Air cool up to 250 psia between centrifugal stages, Refrigeration to reduce CO ₂ to -25degF to liquify

Note: Heat recovery not accounted for.



Compression Power for PC Plant

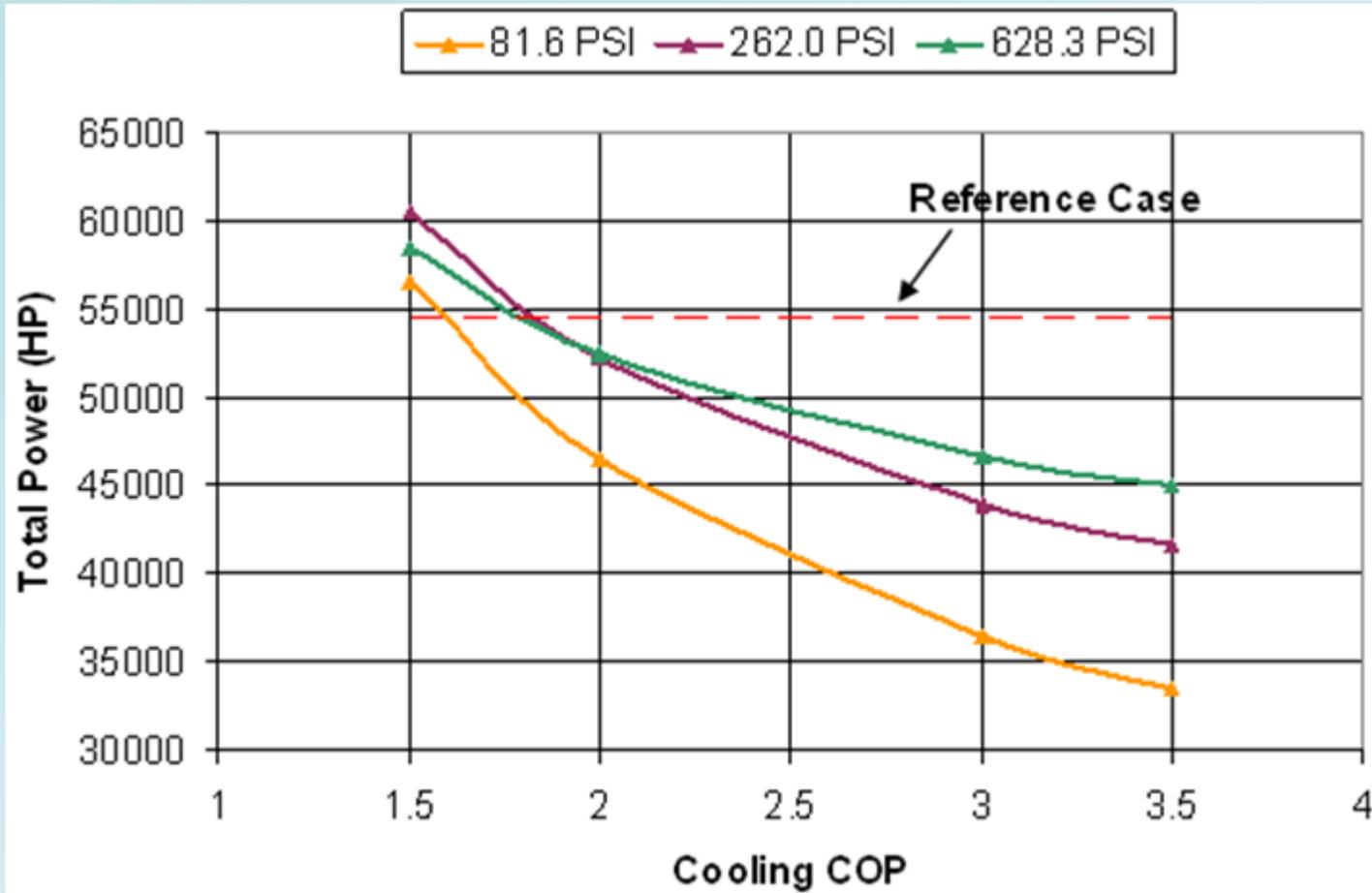
Isothermal Compression





Compression Power for PC Plant

Liquefaction/Pumping Compression





Project Goals

- Develop internally cooled compressor stage that:
 - Provides performance of an integrally geared compressor
 - Has the reliability of a in-line centrifugal compressor
 - Reduces the overall footprint of the package
 - Has less pressure drop than a external intercooler
- Perform qualification testing of a refrigerated liquid CO₂ pump



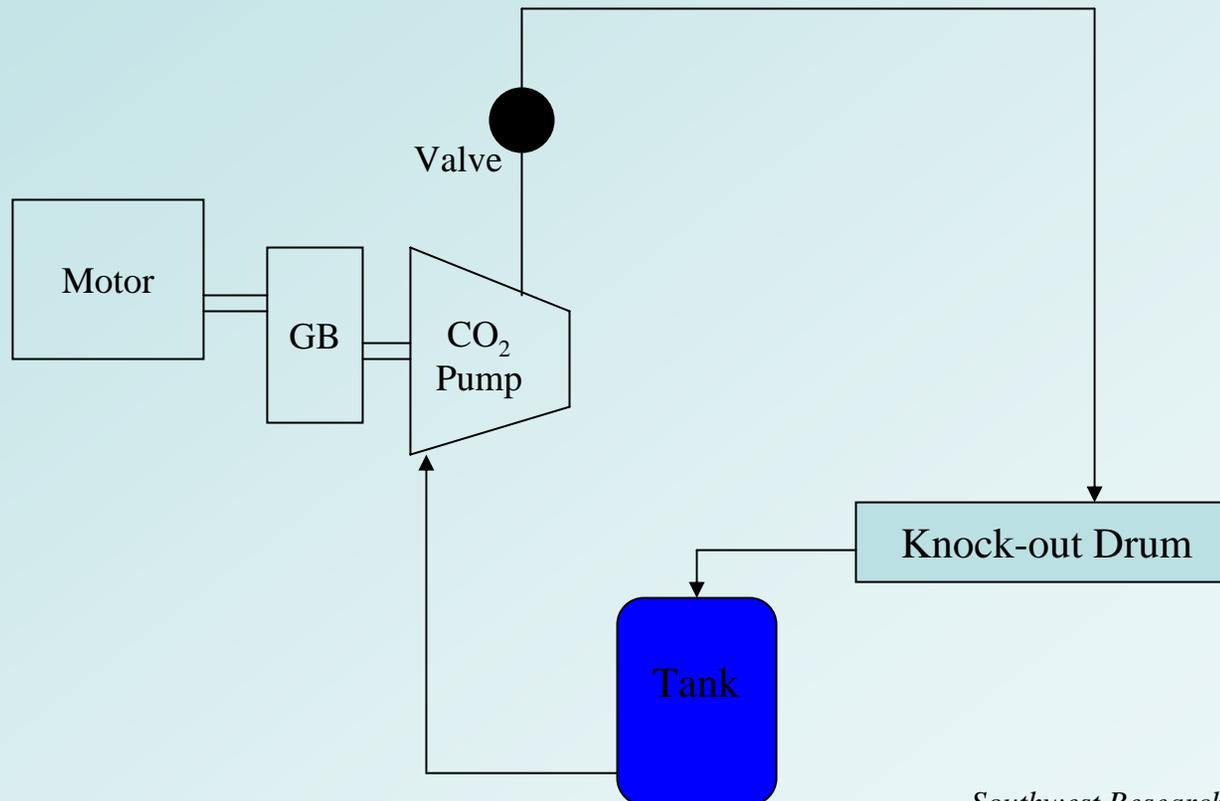
Phase 2 Project Plan

- Experimentally validate thermodynamic predictions.
- Two test programs envisaged:
 - Liquid CO₂ pumping loop
 - Closed-loop CO₂ compressor test with internal cooling
- Power savings will be quantified in both tests.



Liquid CO₂ Pumping Loop Testing

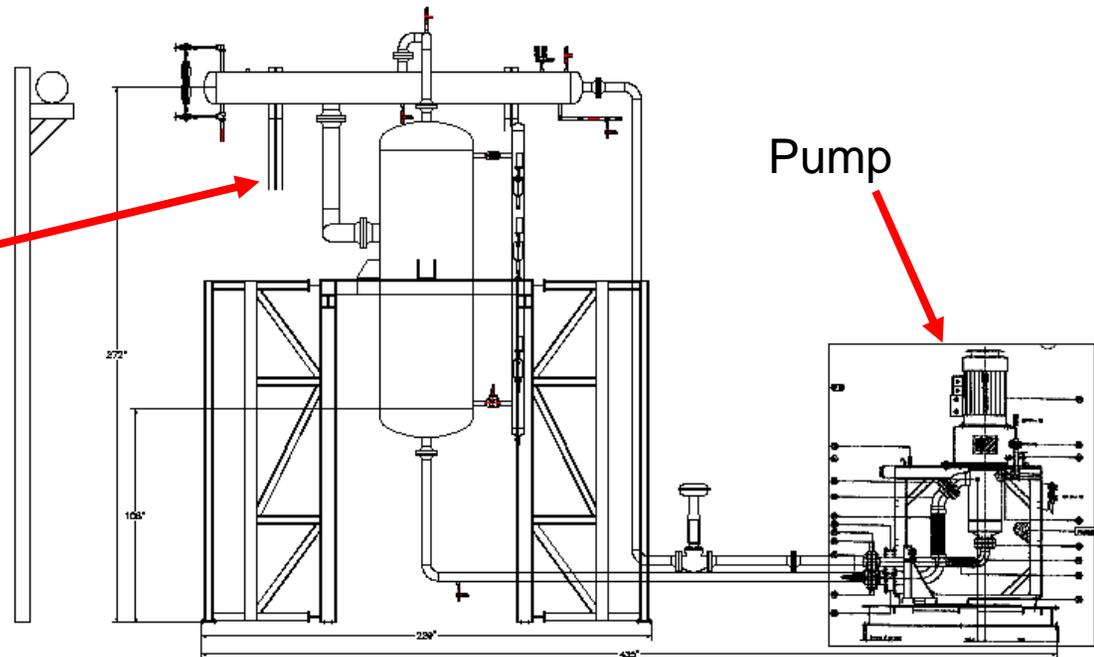
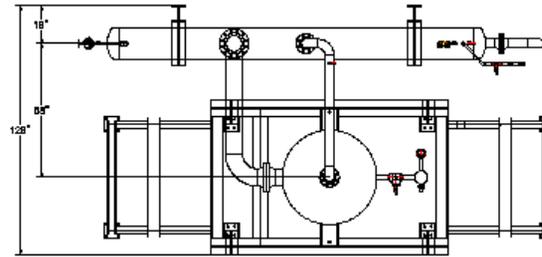
- Testing will measure pump efficiency
- Validate pump design
- Measure NPSH requirements looking for signs of cavitation
- Investigate gas entrainment effects
- Cryostar will supply the pump (250 KW, 100 gpm)





Liquid CO₂ Loop

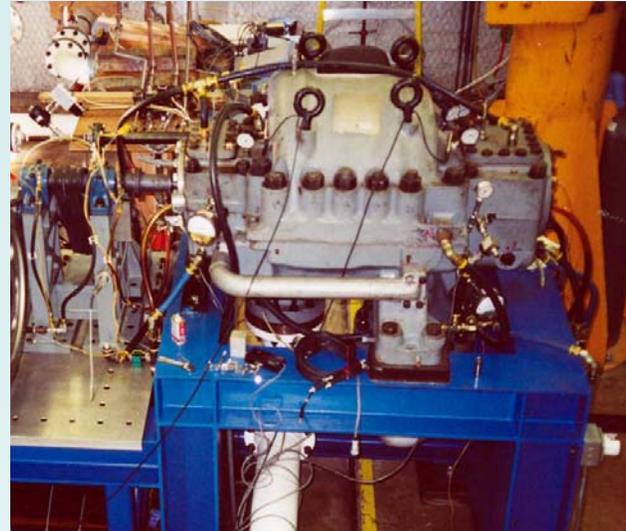
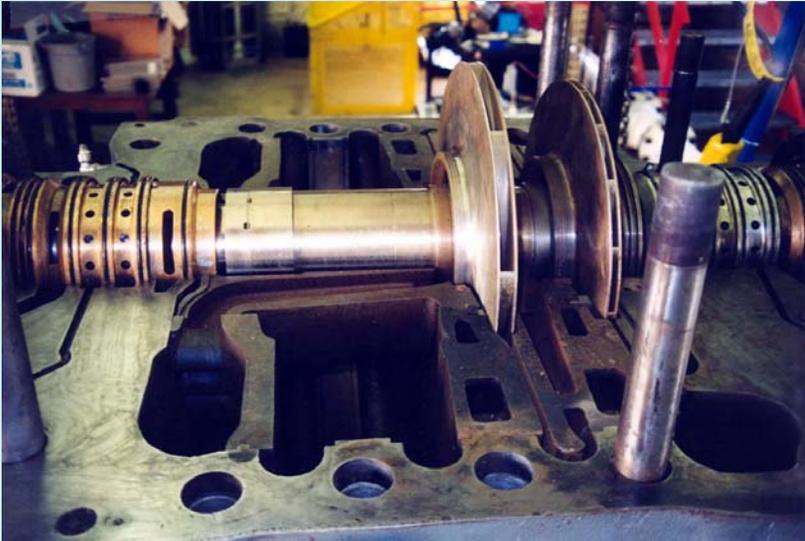
- Vessel layout showing elevated reservoir and knock-out drum
- Pump will be mounted at ground level.
- Orifice run will be located between pump and control valve (in supercritical regime)
- Knock-out drum structural support completed





Internally Cooled Compressor Testing

- Goal: To measure effectiveness of internally cooled diaphragm
- Existing Multi-Stage Test Rig will be utilized using CO₂
- New impeller and internals will be manufactured and tested
- Diaphragms will contain optimized flow path and cooling jacket design
- Stage performance will be measured (P1, T1, P2, P2, Q)
- Both ambient and chilled cooling water will be employed
- Heat transfer enhancement devices employed





Program Benefits

- Provide enabling technology to compress CO₂ from a PC, Oxy-Fuel, or IGCC power plant, cost-effectively minimizing the financial impact of CO₂ sequestration.
- This program identified up to 35% power savings over a conventional CO₂ compression solution.
- Technology applicable to all power plant types plants
- The thermodynamic process is more important than compressor efficiency.
- The internally-cooled compressor concept should result in significant capital savings over an integrally geared compressor
- Liquefaction and pumping equipment will add some additional capital expense, but some is offset by lower cost pump compared to high-pressure compressor.
 - A 35% power reduction will save a utility \$4.2 million per year, based on 4¢ / kwh, which will provide a fast return on investment.
- Testing will be complete 1st Qtr 2010



Areas Needing Further Research

- Further work to reduce the power penalty associated with CCS and utilize waste heat
- Compression must be integrated and optimized with various capture schemes
- Perform optimum driver study
 - i.e. gas turbine, motor, steam turbine
- Develop more reliable compression designs
- Perform more gas properties measurements of CO₂ mixtures
- Refine equation of state near critical point and with mixtures
- Perform optimization of pipeline booster stations
 - Station spacing, liquid vs. gas, driver selection
- Improve reliability of recip EOR recycle compressors
 - i.e. valve reliability
 - Variable speed of sound pulsation models (real gas effects)
- Perform further corrosion studies on the effects of moisture on pipeline corrosion



Questions???

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