

# Challenges in Creating a Pure Element Tracer Diffusion Database

Nagraj Kulkarni

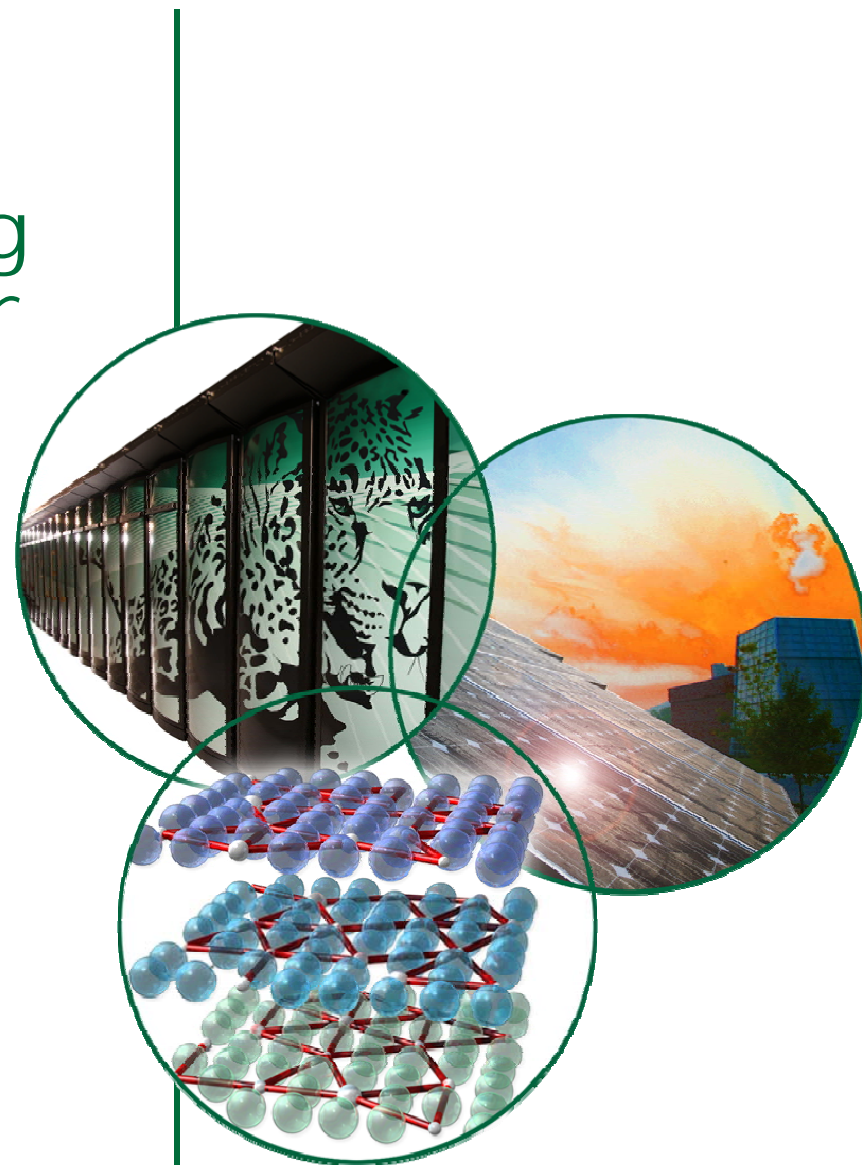
University of Tennessee

Oak Ridge National Laboratory

NIST Diffusion Workshop

Gaithersburg, MD

March 26, 2009

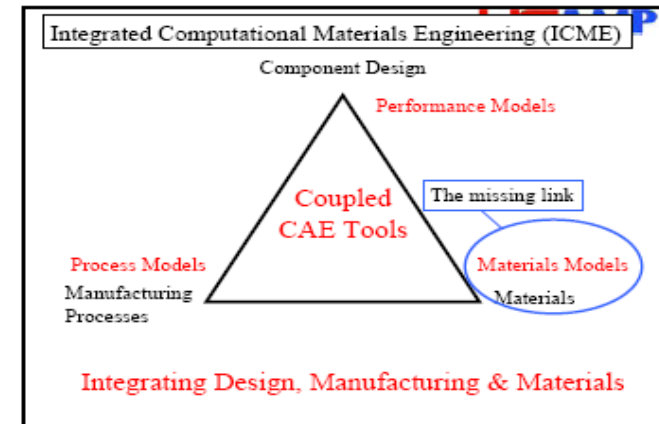


# Outline

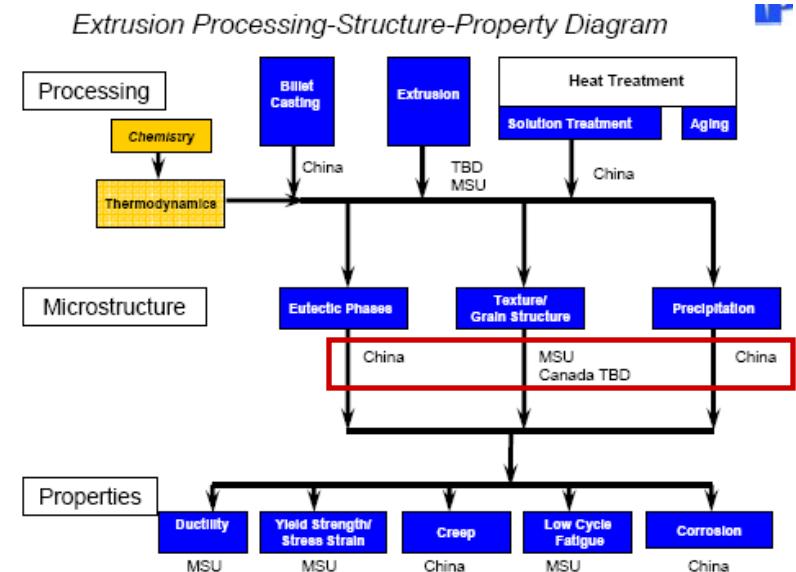
- Diffusion Databases: Key questions
- Technical issues
  - Formalisms: Many!
  - Data for databases: Many!
  - Content of database: Types of diffusion data
  - Approach for constructing db's: Calphad only?
  - Modeling/software: long, exciting road ahead
- Tracer diffusion databases
  - Past Concerns, Current Approach
  - DOE Isotope Program
  - SIMS Instrumentation challenges
- Experimental challenges, current efforts

# Diffusion databases: Key Questions

- Why do we need these?
  - How is this information used for something useful?
- Who needs these?
  - Industrial applications and partners
  - Basic R&D efforts at universities, labs, etc.
- Who will support the work?
  - Offices within the federal government
    - Commerce (NIST), Energy (ORNL, Argonne, etc.), NSF, Homeland Security, NIH, Transportation, Defense (DARPA, Army, Air Force, etc.)
  - Industry partners
  - Industry/University/Government collaborations
    - Sematech, SRC, Focus Centers, professional organizations, etc.
  - International organizations, **multinational partnerships**



**DOE/US-AMP Mg-ICME program requires thermo & diffusion databases**



# Diffusion Formalisms for Databases

- Mobility
- Phenomenological
- Others
  - Interdiffusion (effective), Jump frequencies, ...

# A: "Mobility" Formalism/Database: DICTRA

- Intrinsic flux expression that ignores cross-terms

$$J_k = - \sum_{i=1}^n L_{ki} \frac{\partial \mu_i}{\partial x} = -L_{kk} \frac{\partial \mu_k}{\partial x} = -c_k M_k \frac{\partial \mu_k}{\partial x} \quad (L_{ki} = 0, k \neq i)$$



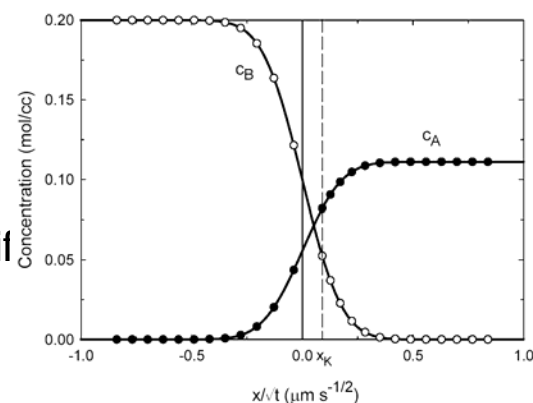
Lawrence Darken

- $M_k$  is known as the "mobility" [Darken 1948]:
  - One unique mobility for each component in a multicomponent system with above assumption
  - Vacancy wind effects included (perhaps artificially) in diagonal terms since off-diagonal phenomenological coefficients ignored
- Multicomponent Darken theory connects mobilities with **tracer diffusion coefficients**
  - Diffusion coefficients in other frames (e.g., lab frame for interdiffusion) can be obtained from mobilities (or  $L_{kk}$ 's) and thermodynamic information by suitable transformations

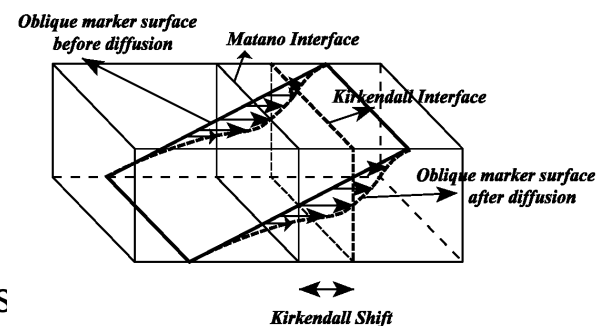
$$L_{kk} = c_k M_k = \frac{c_k D_k^*}{RT}$$

# Input for Mobility Databases: Diffusion data + thermodynamics

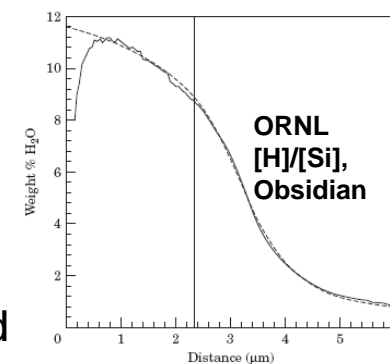
- Interdiffusion Data: **Convert to mobilities with thermo**
  - Steep concentration gradients, molar volume changes, grain boundary effects, can introduce errors in measurements and subsequent analysis: **still manageable**
  - Very long annealing times may be needed for improved accuracy if kinetics are slow
    - Very difficult in **compounds** unless solubility range is extended



- Intrinsic Diffusion Data: **Convert to mobilities with thermo**
  - Require suitable “inert” markers throughout diffusion zone
    - Multiple markers rarely employed except at original “Kirkendall Interface” due to experimental difficulties
  - Vacancy super-saturation (porosity) or under-saturation can cause errors in both analysis



- Tracer Diffusion Data: **Directly obtain mobilities**
  - Most reliable but use of radioactive tracers is time-consuming and expensive



6 **Tracer data using non-radioactive (stable) isotopes not established**

# B: Phenomenological Formalism: Tracer Database

- Intrinsic fluxes defined in the lattice or Kirkendall frame where driving forces are chemical potential gradients

$$J_k = - \sum_{i=1}^{n-1} L_{ki}^n \text{grad } \mu_i \quad (k = 1, 2, \dots, n) \quad \sum_{k=1}^n J_k = - J_v$$

- $L_{ki}$ 's obtained from tracer diffusion database using Manning, Moleko *et al.*, or latest theories

$$L_{11} = \frac{X_1}{V} \cdot \frac{Dt_1}{R \cdot T} \cdot \left[ 1 + \frac{2 \cdot X_1 \cdot Dt_1}{M_o \cdot (X_1 \cdot Dt_1 + X_2 \cdot Dt_2 + X_3 \cdot Dt_3)} \right]$$

$$L_{12} = \frac{2 \cdot X_1 \cdot Dt_1 \cdot X_2 \cdot Dt_2}{V \cdot R \cdot T \cdot M_o \cdot (X_1 \cdot Dt_1 + X_2 \cdot Dt_2 + X_3 \cdot Dt_3)}$$

- Chemical potentials from Calphad databases

➤ *Tracer diffusion database is independent of thermodynamic database*

➤ *No assumptions other than the usual phenomenological assumption*

# Other Formalisms for Databases?

- Interdiffusion

- Multicomponent version (extension of Fick's Law) with concentration gradients as driving forces

$$J_k = - \sum_{j=1}^{n-1} D_{kj}^n \text{grad } c_j$$

- Using "square-root diffusivity" approach interdiffusion coefficients can always be measured (sufficient solid solubility) (Morral et al.)
- Effective integrated interdiffusivities (Dayananda et al.)
  - Amenable to databases?

- Jump Frequencies

- Multicomponent intrinsic flux composed of biased and unbiased fluxes (DeHoff et al.)

$$J_k = 2\alpha_{k+} \lambda c_k \Gamma_k - \frac{1}{6} \lambda^2 \frac{dc_k \Gamma_k}{dx}$$

8  $\Gamma_k$  are tracer jump frequencies



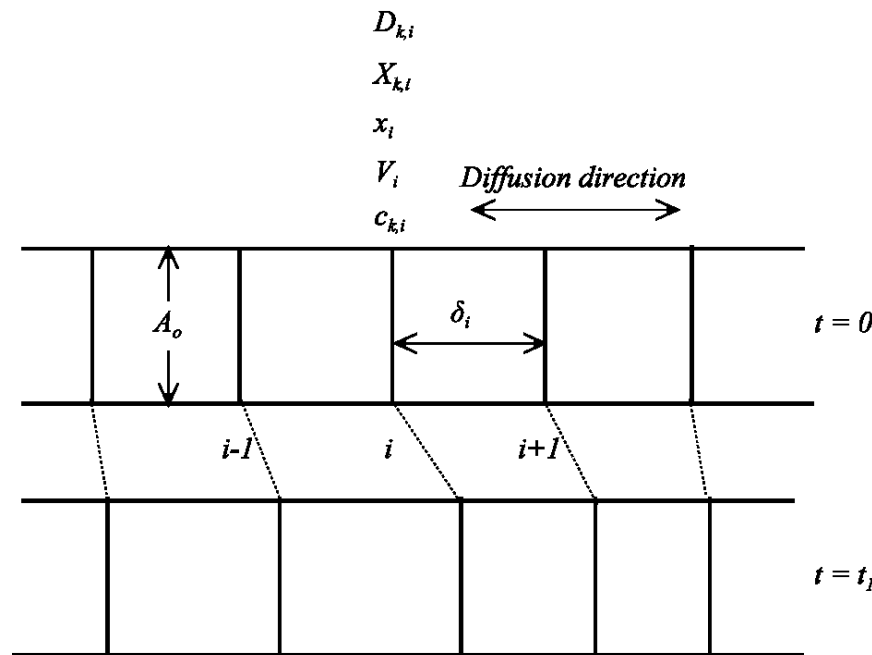
# Which Formalism to Use?

- **Mobility or Phenomenological Formalism or Others?**

# Intrinsic Diffusion Simulation for Assessing Diffusion Formalisms

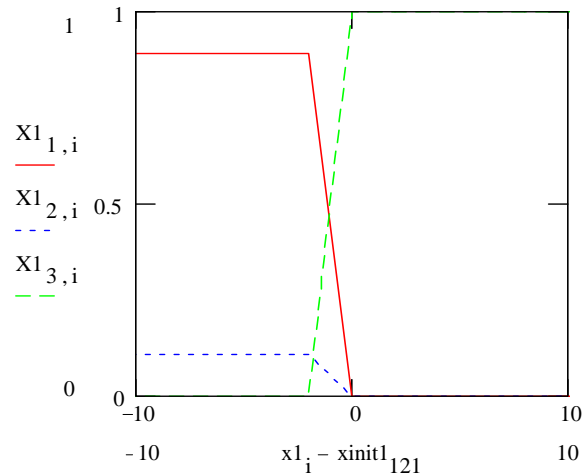
1. Initial concentration distribution for each component
2. Depending upon the formalism, kinetic descriptors as a function of composition, temperature or other variables
3. Thermodynamics of phase, if needed
4. Molar volume as a function of composition

*C. Iswaran, Ph.D. Thesis, Univ. of Florida, 1993*  
*Kulkarni & DeHoff, Acta Mat 2005*



- **Simple** yet effective algorithm
- Handles **variable molar volumes**
- Developed in MathCad – **user-friendly**
- **Efficient** – practical output for a single diffusion couple in less than a minute
- **Versatile** – adaptable to various formalisms

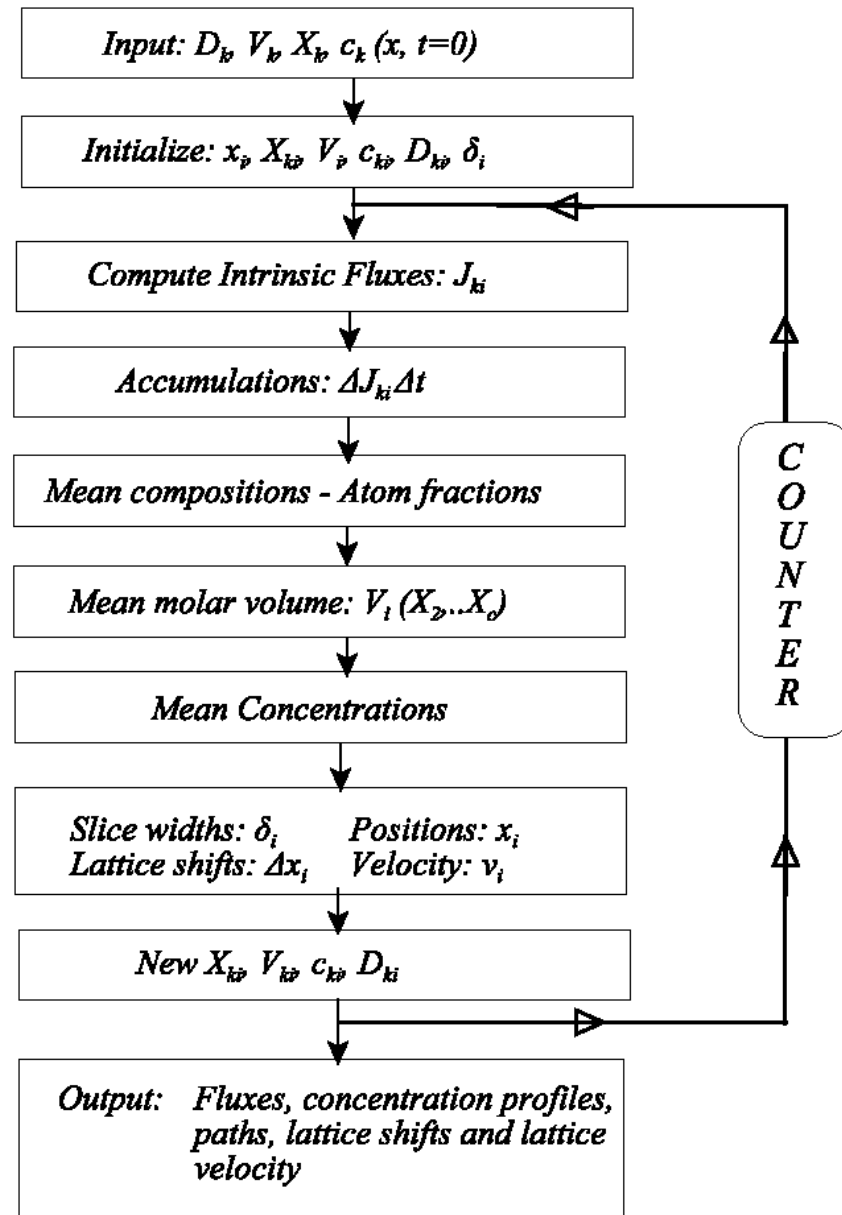
# Simulation Algorithm



Initial concentrations ( $c_{k,i} = X_{k,i} / V$ )

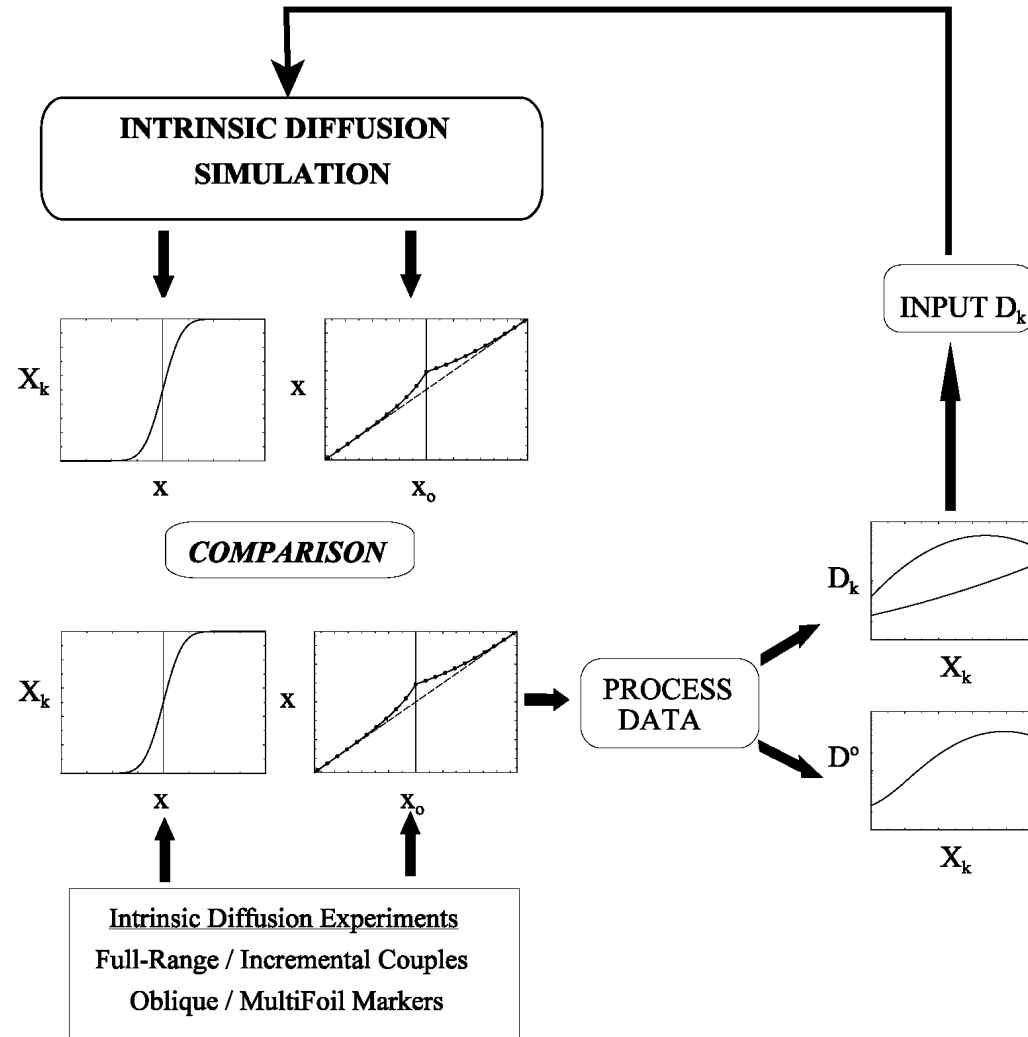
$$J_{k,i}^K = -D_{k,i}^K \frac{c_{k,i+1} - c_{k,i-1}}{x_{k,i+1} - x_{k,i-1}}$$

Fluxes computed using finite difference form



# Procedure for Assessing Darken (Mobility) and Manning (Phenom.)

## A. Establishing consistency of experimental measurements and procedures



## B. Procedure for testing the D-M relations with aid of the simulation

$$D_A = D_A^* \left( 1 + \frac{\partial \ln \gamma_A}{\partial \ln X_A} \right) = D_A^* \Phi$$

$$D_B = D_B^* \left( 1 + \frac{\partial \ln \gamma_B}{\partial \ln X_B} \right) = D_B^* \Phi$$

$$D^o = (X_B D_A^* + X_A D_B^*) \Phi$$

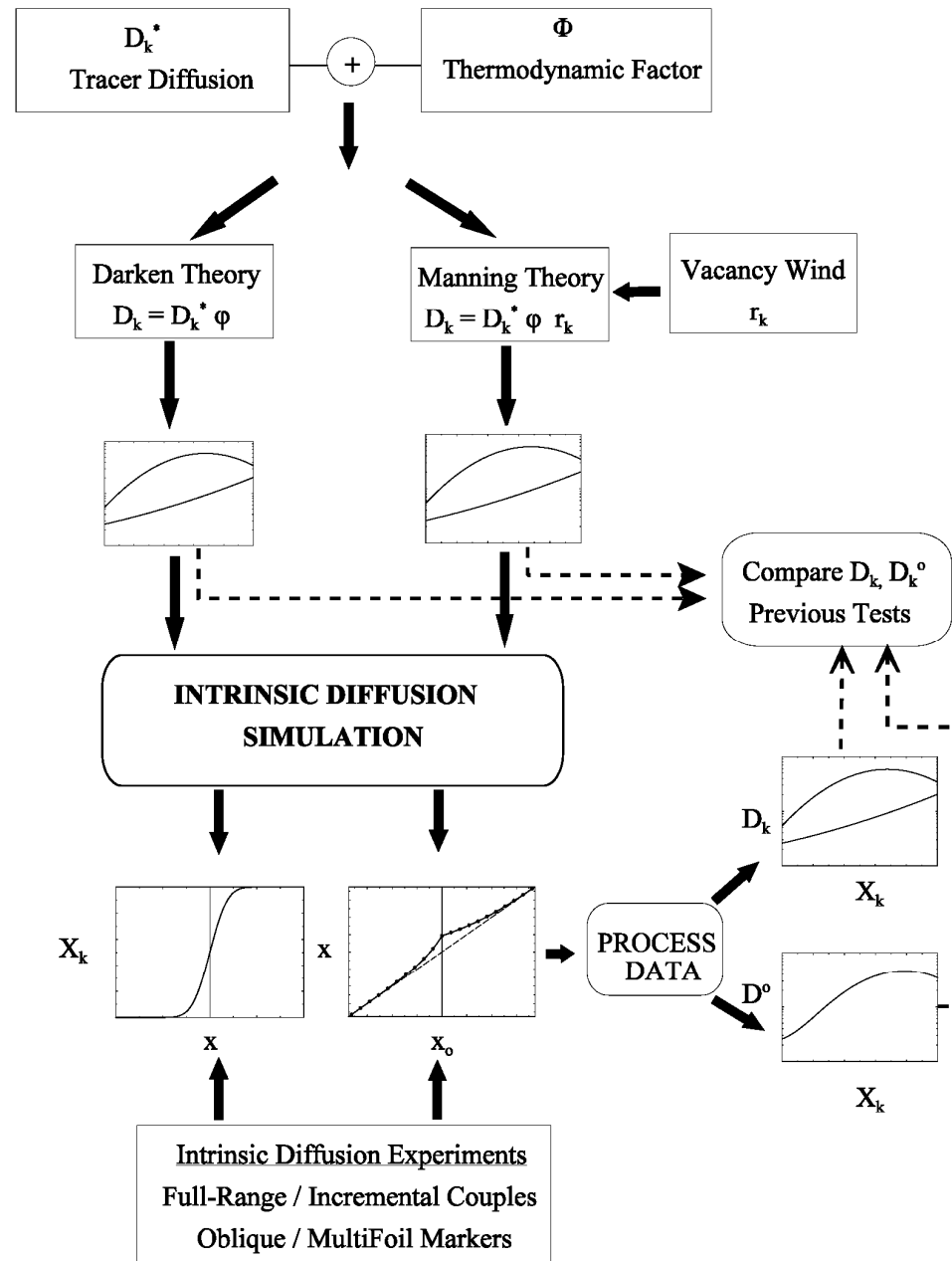
Darken relations

$$D_A = D_A^* \Phi (1 + V_A)$$

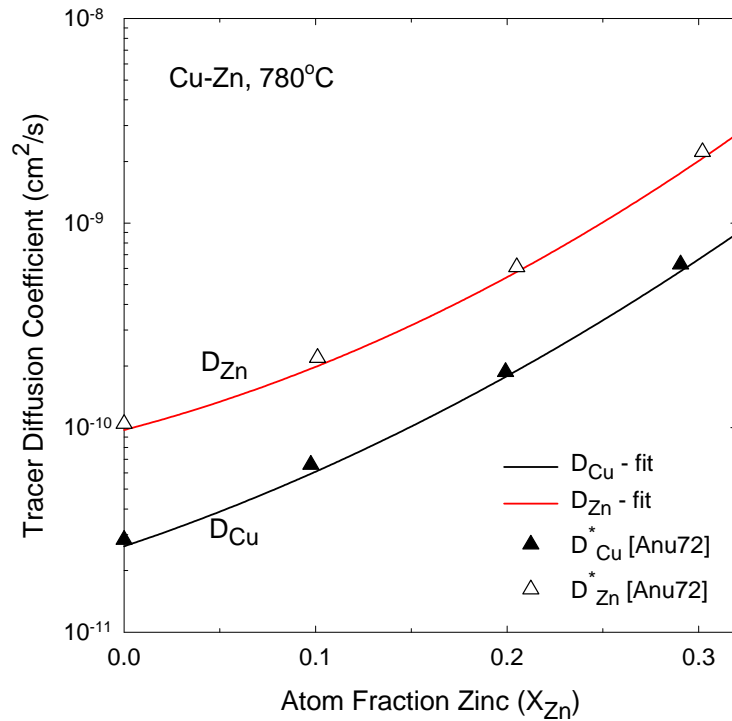
$$D_B = D_B^* \Phi (1 - V_B)$$

$$D^o = (X_B D_A^* + X_A D_B^*) \Phi S$$

Manning relations

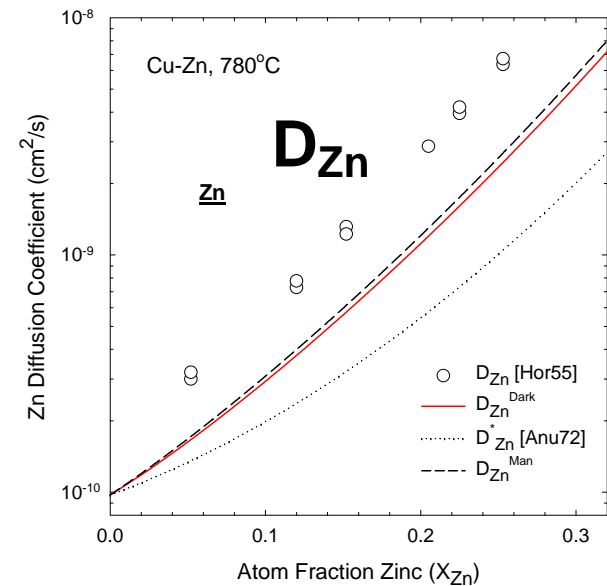
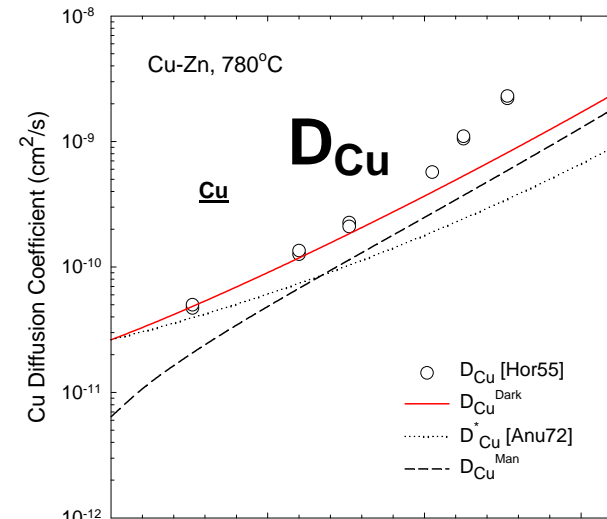


# Assessing D-M Relations for Cu-Zn



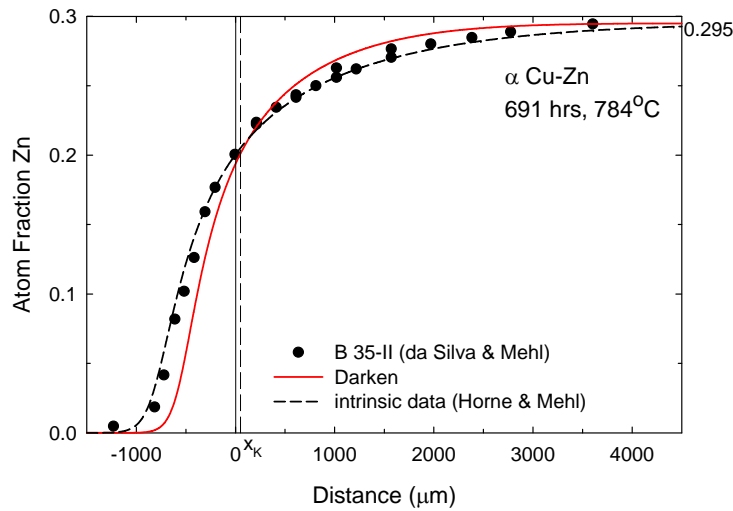
Tracer diffusion data

[Anusavice et al., Met. Trans., 1972]

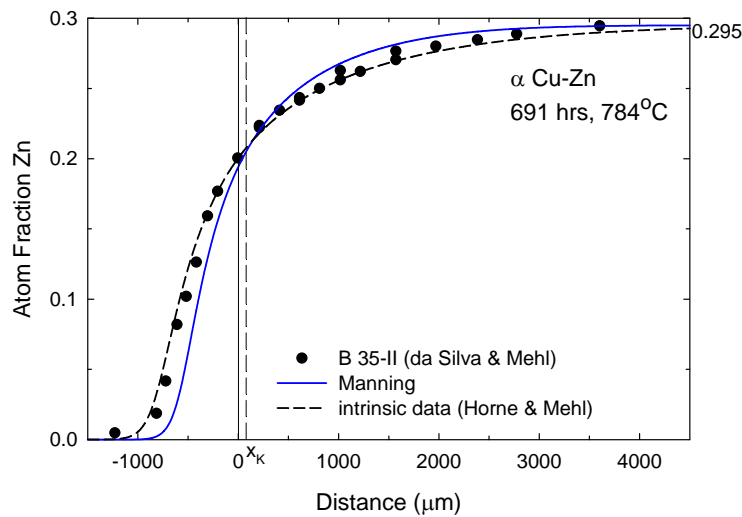
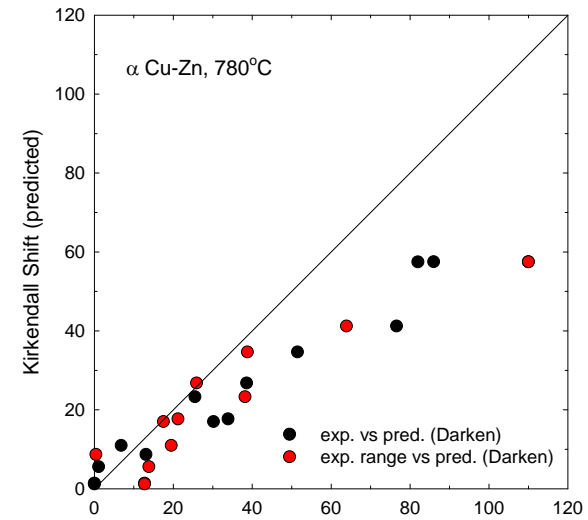


Managed by UT-Battelle  
 Problem with predicted intrinsic coefficients at high Zn compositions

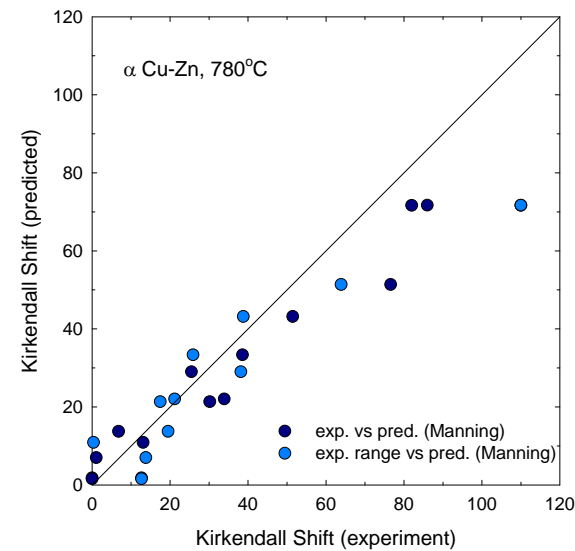
# D-M Relations for Cu-Zn contd.



**Darken**



**Manning**



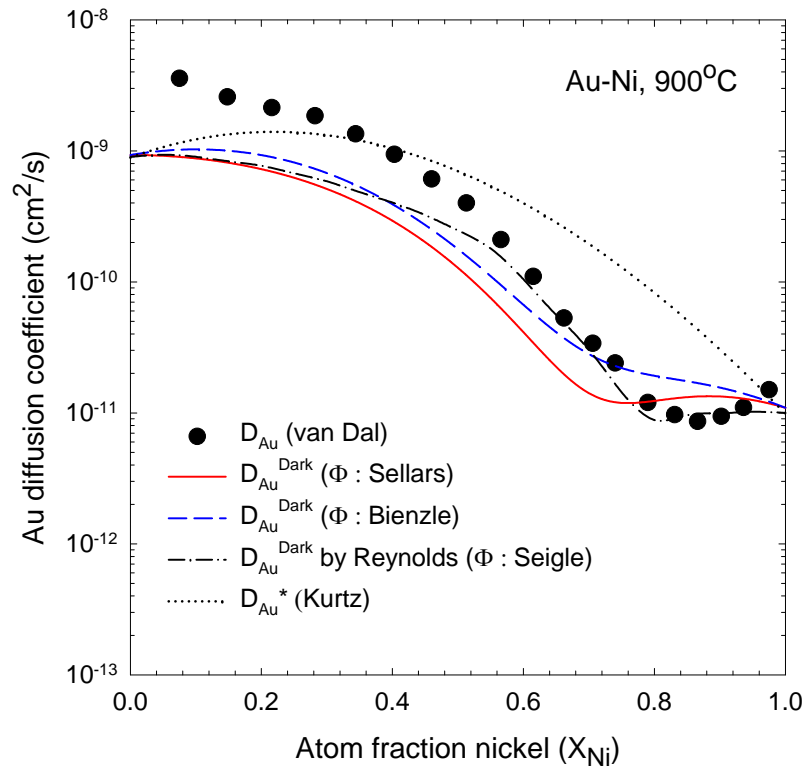
**Concentration profiles**

**Kirkendall shifts**

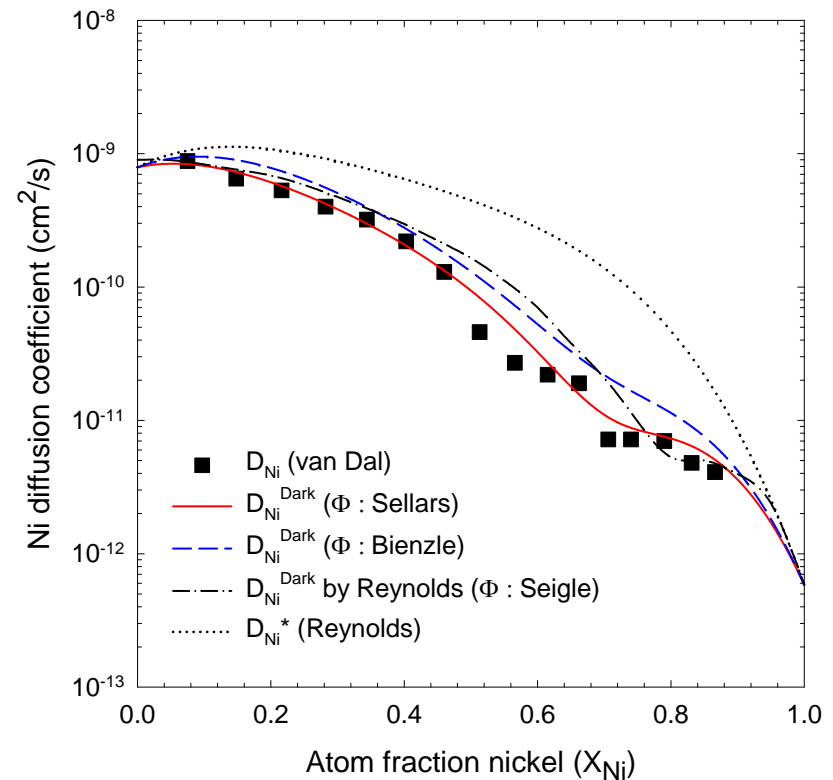
15 **Minor differences between Darken (mobility approach) and Manning**



# Darken Relations for Au-Ni: Predicted Intrinsic Diffusion Coefficients



**Darken:  $D_{\text{Au}}$**

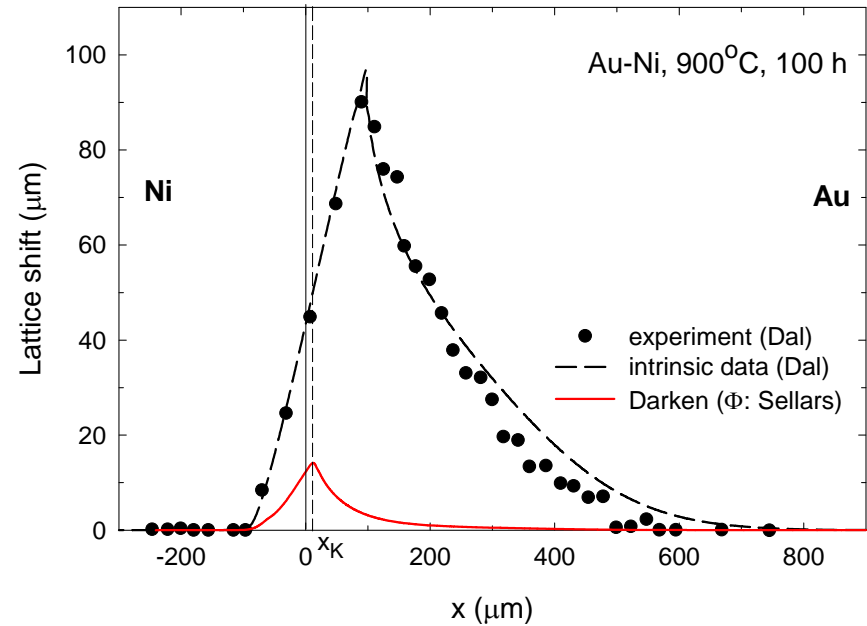
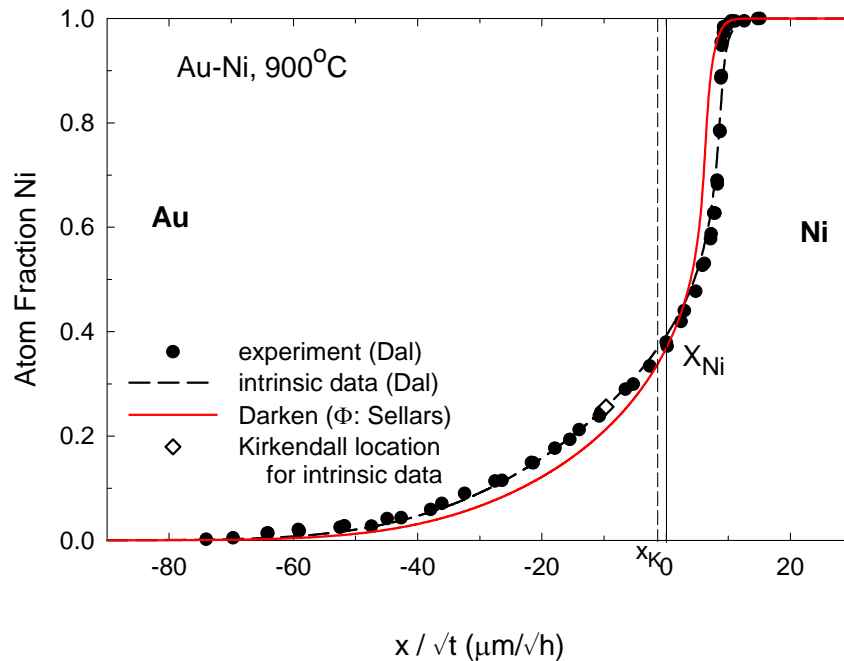


**Darken:  $D_{\text{Ni}}$**

- **Problem with predicted Au intrinsic diffusion coefficient**



# Assessing Darken Relations for Au-Ni with Simulation



Lattice shift profile

- Differences between predicted and experimental  $D_{\text{Au}}$  results in large differences in lattice shift profiles
- Manning correction outside limits (need to check Moleko et al. formalism)

# Mobility Formalism: Cu-Ni-Zn

$$\log(Dt_{\text{Cu}}) = -3.53 \cdot X_{\text{Ni}}^{1.16} + 3.6 \cdot X_{\text{Zn}}^{1.02} - 9.46$$

$$\log(Dt_{\text{Ni}}) = -4.05 \cdot X_{\text{Ni}}^{1.3} + 3.28 \cdot X_{\text{Zn}}^{1.07} - 9.96$$

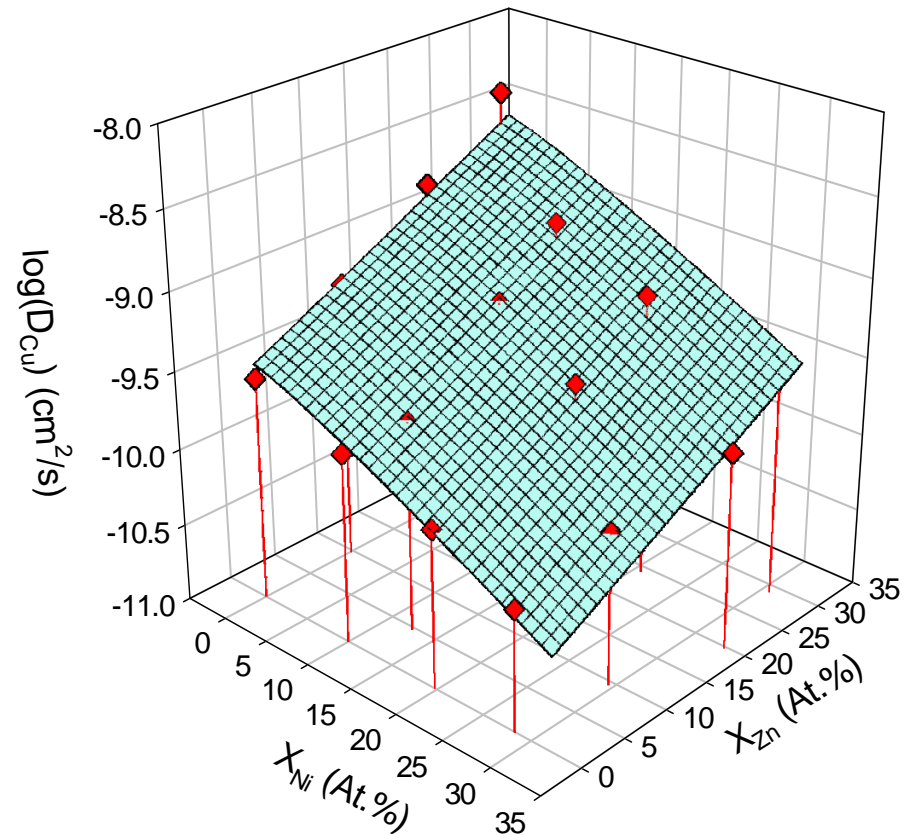
$$\log(Dt_{\text{Zn}}) = -3.2 \cdot X_{\text{Ni}} + 5.21 \cdot X_{\text{Zn}}^{1.25} - 9$$

$$D_{\text{Zn}}^* > D_{\text{Cu}}^* > D_{\text{Ni}}^*$$

Similar composition dependence

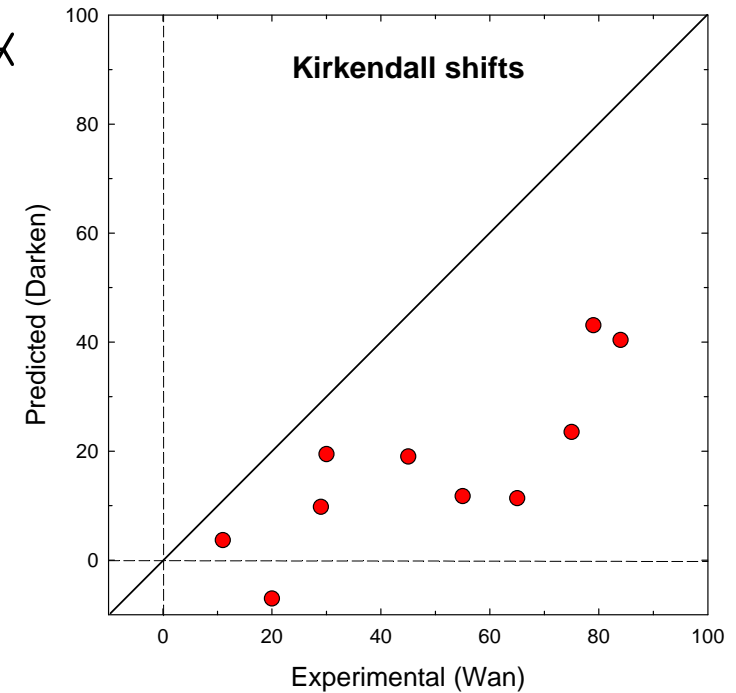
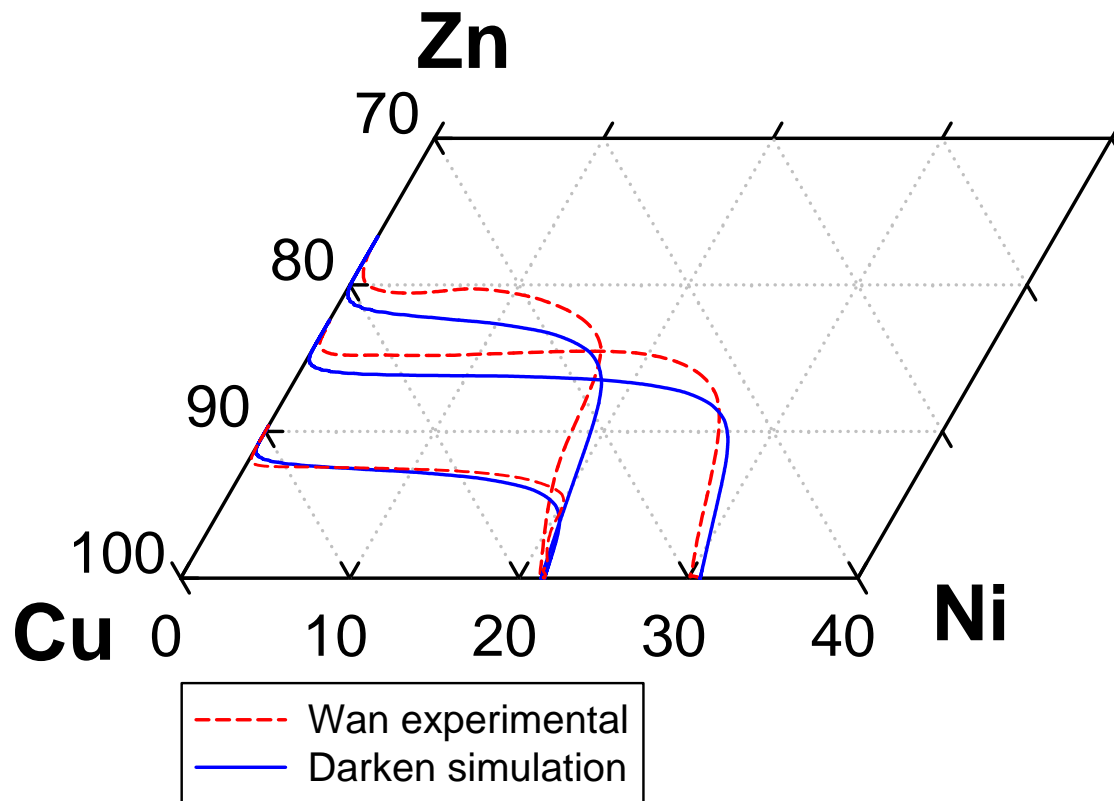
Thermodynamics from Jiang,  
Ishida *et al.*, *J. Phys. Chem.*  
*Sol.*, 2004.

## Tracer diffusion coefficients



Anusavice & DeHoff, *Met. Trans. A.*, 1972

# Mobility Formalism: Cu-Ni-Zn contd.



- **Mobility formalism provides reasonable composition paths**
- **Underestimates Kirkendall shifts**

# Manning Relations in Cu-Ni-Zn: Fluxes

$$J_i = -L_{ii} \cdot \frac{d}{dx} \mu_i - \sum_j L_{ij} \cdot \frac{d}{dx} \mu_j$$

$$J_1 = R \cdot T \cdot \left[ -L_{11} \left( \frac{\Phi_{11}}{X_1} \cdot \frac{d}{dx} X_1 + \frac{\Phi_{12}}{X_2} \cdot \frac{d}{dx} X_2 \right) - L_{12} \left( \frac{\Phi_{22}}{X_2} \cdot \frac{d}{dx} X_2 + \frac{\Phi_{21}}{X_1} \cdot \frac{d}{dx} X_1 \right) - \frac{L_{13}}{X_3} \cdot (-1) \cdot \left[ X_1 \cdot \left( \frac{\Phi_{11}}{X_1} \cdot \frac{d}{dx} X_1 + \frac{\Phi_{12}}{X_2} \cdot \frac{d}{dx} X_2 \right) + X_2 \cdot \left( \frac{\Phi_{22}}{X_2} \cdot \frac{d}{dx} X_2 + \frac{\Phi_{21}}{X_1} \cdot \frac{d}{dx} X_1 \right) \right] \right]$$

$$J_2 = R \cdot T \cdot \left[ -L_{21} \left( \frac{\Phi_{11}}{X_1} \cdot \frac{d}{dx} X_1 + \frac{\Phi_{12}}{X_2} \cdot \frac{d}{dx} X_2 \right) - L_{22} \left( \frac{\Phi_{22}}{X_2} \cdot \frac{d}{dx} X_2 + \frac{\Phi_{21}}{X_1} \cdot \frac{d}{dx} X_1 \right) - \frac{L_{23}}{X_3} \cdot (-1) \cdot \left[ X_1 \cdot \left( \frac{\Phi_{11}}{X_1} \cdot \frac{d}{dx} X_1 + \frac{\Phi_{12}}{X_2} \cdot \frac{d}{dx} X_2 \right) + X_2 \cdot \left( \frac{\Phi_{22}}{X_2} \cdot \frac{d}{dx} X_2 + \frac{\Phi_{21}}{X_1} \cdot \frac{d}{dx} X_1 \right) \right] \right]$$

$$J_3 = R \cdot T \cdot \left[ -L_{31} \left( \frac{\Phi_{11}}{X_1} \cdot \frac{d}{dx} X_1 + \frac{\Phi_{12}}{X_2} \cdot \frac{d}{dx} X_2 \right) - L_{32} \left( \frac{\Phi_{22}}{X_2} \cdot \frac{d}{dx} X_2 + \frac{\Phi_{21}}{X_1} \cdot \frac{d}{dx} X_1 \right) - \frac{L_{33}}{X_3} \cdot (-1) \cdot \left[ X_1 \cdot \left( \frac{\Phi_{11}}{X_1} \cdot \frac{d}{dx} X_1 + \frac{\Phi_{12}}{X_2} \cdot \frac{d}{dx} X_2 \right) + X_2 \cdot \left( \frac{\Phi_{22}}{X_2} \cdot \frac{d}{dx} X_2 + \frac{\Phi_{21}}{X_1} \cdot \frac{d}{dx} X_1 \right) \right] \right]$$

# Manning Relations in Cu-Ni-Zn: Lij's

$$L_{11} = \frac{X_1}{V} \cdot \frac{Dt_1}{R \cdot T} \cdot \left[ 1 + \frac{2 \cdot X_1 \cdot Dt_1}{M_o \cdot (X_1 \cdot Dt_1 + X_2 \cdot Dt_2 + X_3 \cdot Dt_3)} \right]$$

$$L_{12} = \frac{2 \cdot X_1 \cdot Dt_1 \cdot X_2 \cdot Dt_2}{V \cdot R \cdot T \cdot M_o \cdot (X_1 \cdot Dt_1 + X_2 \cdot Dt_2 + X_3 \cdot Dt_3)}$$

$$L_{13} = \frac{2 \cdot X_1 \cdot Dt_1 \cdot X_3 \cdot Dt_3}{V \cdot R \cdot T \cdot M_o \cdot (X_1 \cdot Dt_1 + X_2 \cdot Dt_2 + X_3 \cdot Dt_3)}$$

$$L_{22} = \frac{X_2}{V} \cdot \frac{Dt_2}{R \cdot T} \cdot \left[ 1 + \frac{2 \cdot X_2 \cdot Dt_2}{M_o \cdot (X_1 \cdot Dt_1 + X_2 \cdot Dt_2 + X_3 \cdot Dt_3)} \right]$$

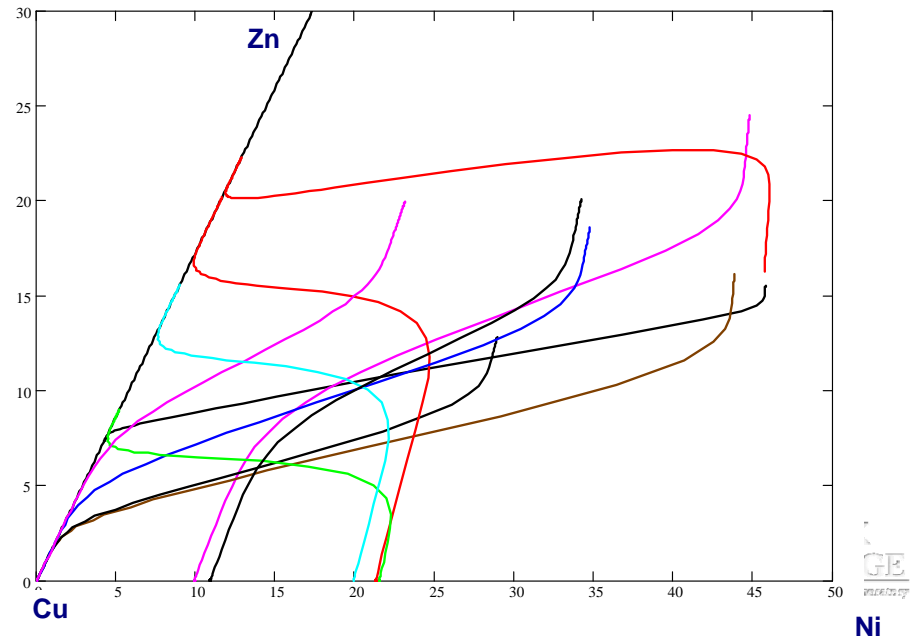
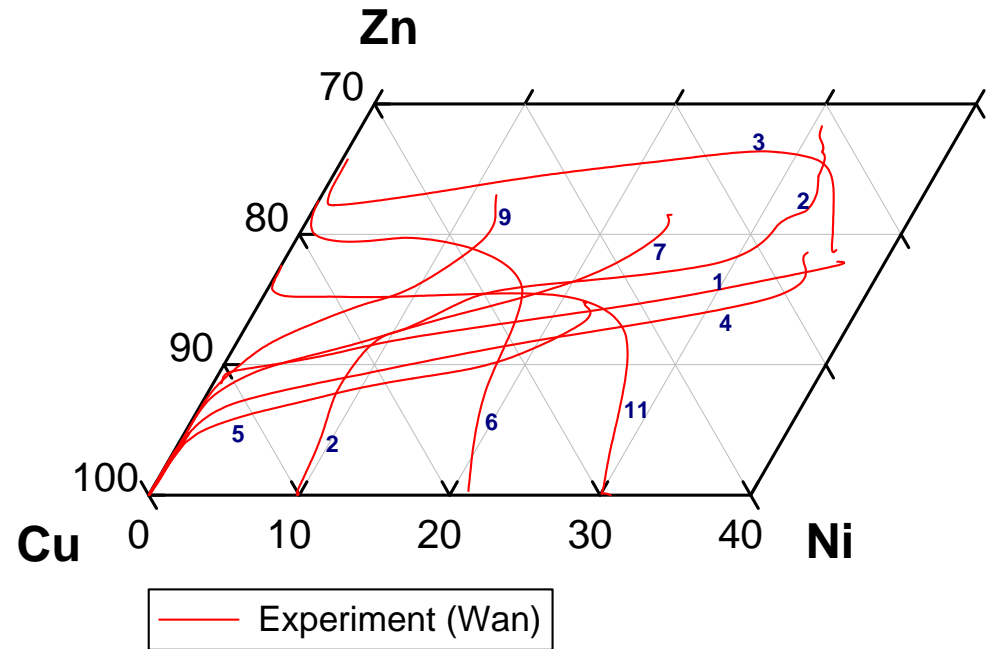
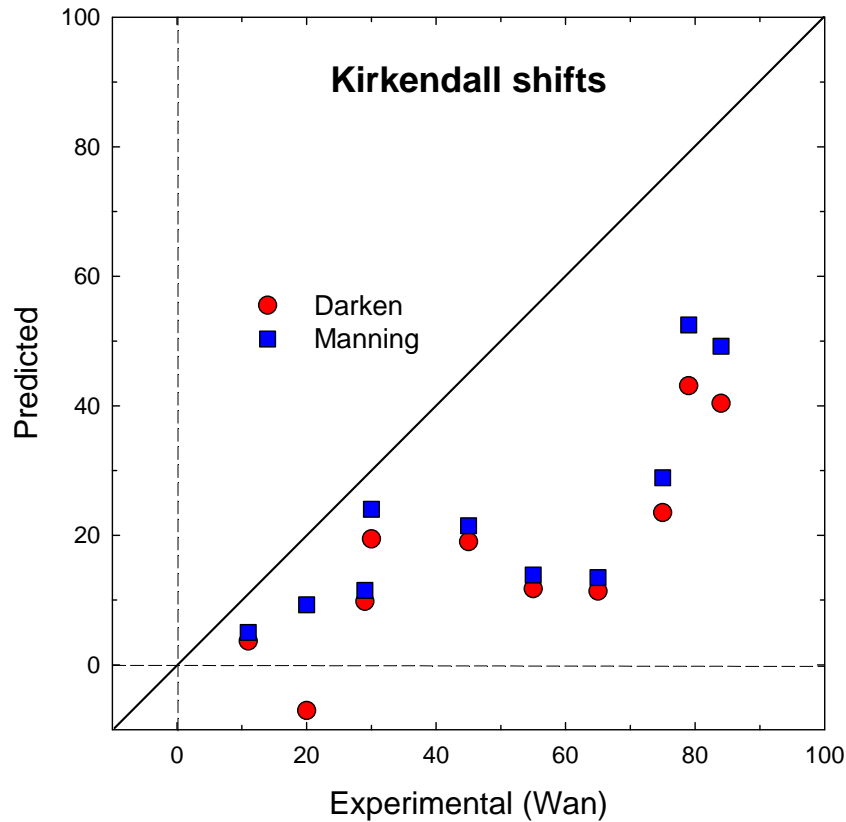
$$L_{23} = \frac{2 \cdot X_2 \cdot Dt_2 \cdot X_3 \cdot Dt_3}{V \cdot R \cdot T \cdot M_o \cdot (X_1 \cdot Dt_1 + X_2 \cdot Dt_2 + X_3 \cdot Dt_3)}$$

$$L_{33} = \frac{X_3}{V} \cdot \frac{Dt_3}{R \cdot T} \cdot \left[ 1 + \frac{2 \cdot X_3 \cdot Dt_3}{M_o \cdot (X_1 \cdot Dt_1 + X_2 \cdot Dt_2 + X_3 \cdot Dt_3)} \right]$$

$$L_{ij} = L_{ji}$$

# Manning: Cu-Ni-Zn

## Diffusion Composition Paths in Cu-Ni-Zn at 900°C



➤ **Manning formalism slightly better for Kirkendall shifts**

# So Which Formalism to Use?

- Mobility or Phenomenological Formalism or Others?
  - Phenomenological formalism slightly better for systems studied, so far...
    - Fewer assumptions
  - **Better** to have software capable of handling different formalisms, e.g., Phenomenological can handle Mobility formalism as a limiting case but not vice versa.
  - **Better** to keep diffusion database independent of thermodynamic database.
  - Tracer diffusion database that feeds into Lij's has diffusivity *units of cm<sup>2</sup>/s* that provides more physical meaning to user.

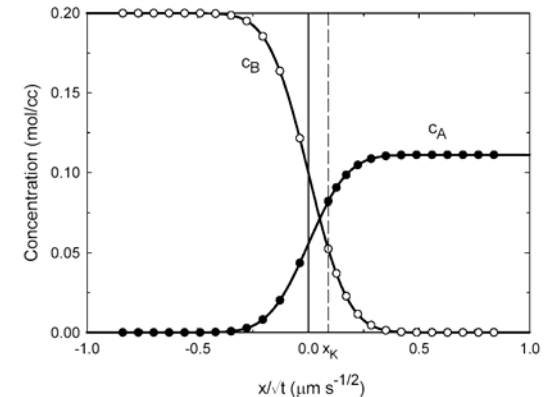
➤ **Ultimately, choice of the individual user!**

# Data for Diffusion Databases

## Experimental data

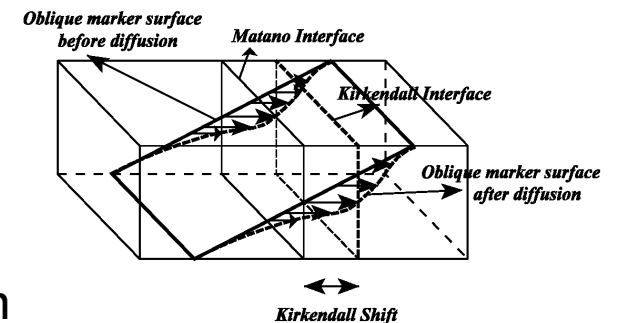
### • Interdiffusion Data

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- Very long annealing times may be needed for improved accuracy if kinetics are slow
  - **Very difficult in compounds unless solubility range is extended**



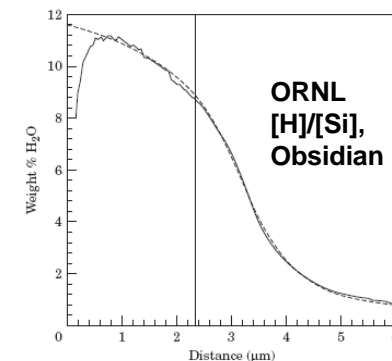
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- Require suitable “inert” markers throughout diffusion zone
  - Multiple markers rarely employed except at original “Kirkendall Interface” due to experimental difficulties
- Vacancy super-saturation (porosity) or under-saturation can cause errors in both analysis



### • Tracer Diffusion Data

- Most reliable but use of radioactive tracers is time-consuming and expensive



24 **Tracer data using non-radioactive (stable) isotopes not established but promising**



# Data for Databases contd.

## First-principles data

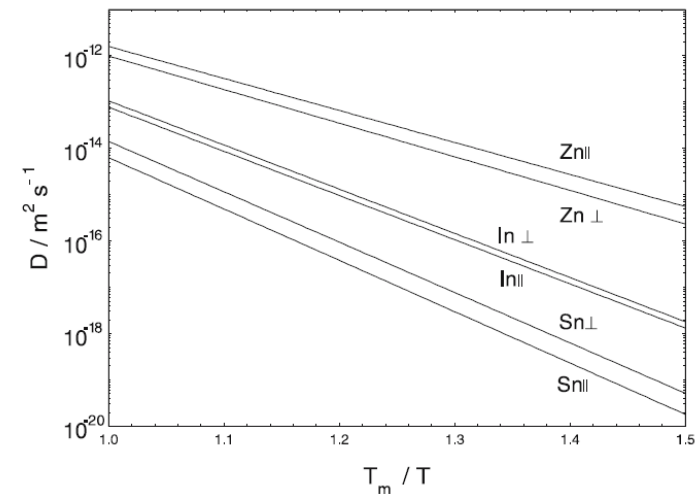
- Mg data/mechanisms (Z.K. Liu., Wolverton et al.)
- NiAl intermetallic data/mechanisms (A. Van der Ven, ...)
- Other pure and compound systems
- Oxides (Ågren et al.), Nitrides, ?

## Empirical data

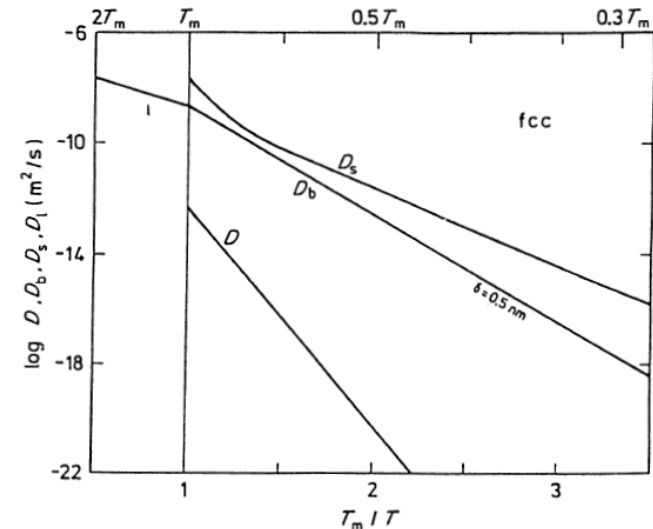
- CIGS system: Empirical approach by Ashby & Brown
  - Utilized by Campbell, et al. for reference pure element diffusivities
- Interdiffusivities: Birchenall & Mehl, others

# Diffusion Databases: What should they contain?

- Volume diffusivities
  - Mostly
- Orientation dependent diffusivities
  - Important for non-isotropic elements (Mg, Zn) and compounds
- Grain boundary diffusivities: No systematic experimental effort (?)
  - Bicrystals, tricrystals
  - Modeling (Mishin et al.)
  - Directly using **EBSD + SIMS integrated system** (the future...)
- Surface/Interface diffusivities
  - Cu/SiN interfacial diffusion dominates electromigration flux in damascene interconnects



Self-diffusion in single crystals of Zn (hex.), In and Sn (tetrag.) parallel and perpendicular to their unique axis (Mehrer. Diffusion in Solids)



Self-diffusion in fcc metals in lattice ( $D$ ), along grain boundaries ( $D_g$ ), on surface ( $D_s$ ) and liquid phase (Herzig and Mishin).

# Approach for Constructing Diffusion Databases

## Calphad Approach (Volume diffusivities)

- Based on constructing models for multicomponent systems using assessed models from relevant binary systems
- Need pure element reference tracer diffusivities
  - Use first principles or empirical approaches if data not available
  - Conduct difficult experiments (CVD, high pressure, creative experiments)
- Optimization of various types of data (tracer, interdiffusion, intrinsic diffusion, first principles, etc.) from various sources
  - Employ desired weighting
- Composition dependence using Redlich-Kister type polynomial functions
- Temperature dependence using Arrhenius expressions

# Approach for Diffusion Dbs. Contd.

However ...

- Calphad approach is convenient but ...
  - Diffusivities are absolute quantities and not relative like Gibbs energies that require reference state values.
    - Hence standard element reference diffusivities need not be used if not available, e.g., Al hcp, Mg fcc.
    - Because kinetic coefficients may vary by several orders in magnitude, small errors in non-measurable reference element values may cause large errors in unknown coefficients
  - Some may prefer to keep diffusion database independent of thermodynamic database.
    - Use only tracer diffusion or first principles data
      - Hence, optimization efforts may be simplified
  - Impurity diffusion, other diffusion mechanisms (aided with first principles analysis) may require more than a single polynomial model or non-polynomial models (?).

# Tracer Data Fit for Cu-Ni-Zn

$$\log(Dt_{\text{Cu}}) = -3.53 \cdot X_{\text{Ni}}^{1.16} + 3.6 \cdot X_{\text{Zn}}^{1.02} - 9.46$$

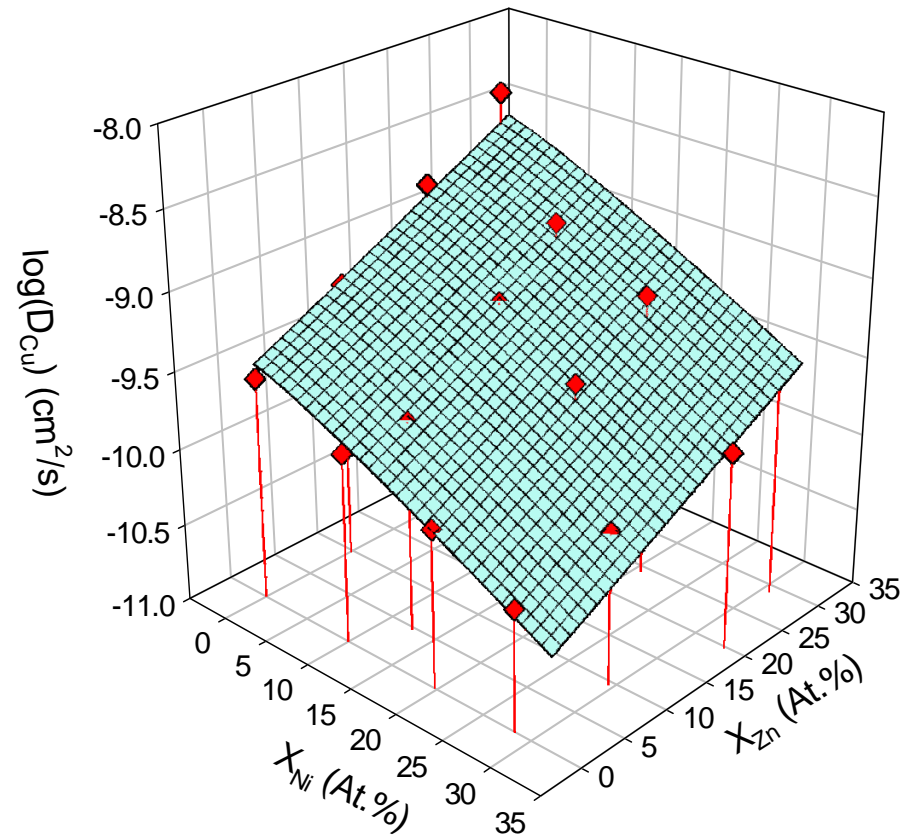
$$\log(Dt_{\text{Ni}}) = -4.05 \cdot X_{\text{Ni}}^{1.3} + 3.28 \cdot X_{\text{Zn}}^{1.07} - 9.96$$

$$\log(Dt_{\text{Zn}}) = -3.2 \cdot X_{\text{Ni}} + 5.21 \cdot X_{\text{Zn}}^{1.25} - 9$$

$$D_{\text{Zn}}^* > D_{\text{Cu}}^* > D_{\text{Ni}}^*$$

Similar composition dependence

## Tracer diffusion coefficients



Anusavice & DeHoff, *Met. Trans. A.*, 1972

# Diffusion Modeling Software

- **Type of diffusion database**
  - Integrated with thermodynamic db
  - Independent of thermodynamic db
- 1D vs 3D
- **Thin film vs Bulk**
  - Grain boundary, orientation, nucleation, texture, stress, etc.
- Phase Field / Crystal Phase Field
  - Special cases only?
- Input information
  - Molar volume, temperature, composition, crystal structure, different boundary conditions, etc.
- **Ease of interface** with other software and db's
  - Properties

# Tracer Diffusion Database

## Radioactive Isotopes

- Tracer diffusion coefficient in a homogeneous single-phase system from the thin film solution

### Tracer flux

$$J_k^{U,Fick} = - D_k^* \frac{\partial c_k}{\partial x}$$

### Thin film solution for $D_k^*$

$$c^*(x,t) = \frac{S}{2\sqrt{\pi D^* t}} \exp\left(-\frac{x^2}{4D^* t}\right)$$

- Measure  $D_k^*$  at each composition for samples annealed for different times; Repeat procedure at different temperatures; Plot  $D_k^*$  vs  $1/T$  to obtain Arrhenius parameters for each sample composition within various phases; Fit tracer diffusivities in a phase as a function of temperature and composition for binaries using polynomial functions for composition dependence.
- Tracer is an isotope of one of the elements in the homogeneous alloy that is present in extremely dilute amounts (ppm) so that
  - Thin film solution for diffusion coefficient is valid and
  - Initial composition of the alloy is unchanged
- Previously, only with a radioactive isotope could trace amounts of the isotope (tracer) be detected due to the high intensity of radiation (beta, gamma):
  - **Time, Money and Safety Issues**

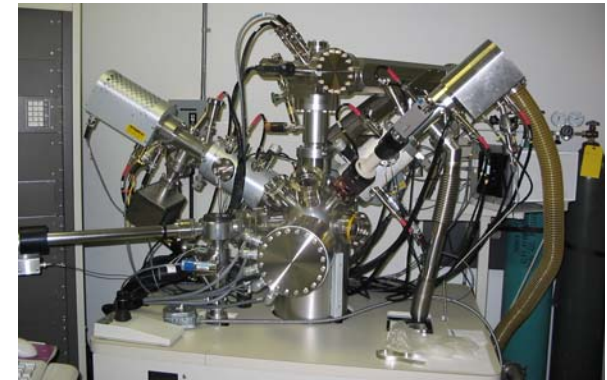
# Tracer Diffusion Database

## Stable Isotopes and SIMS

- Use of stable isotopes has a dramatic effect on safety and reduced costs.
- Advancements in Secondary Ion Mass Spectrometry (SIMS) for the accurate detection of trace amounts of stable isotopes permits thin film solution to be utilized, i.e., essentially the same-simple analytical treatment as before.
- SIMS systems at ORNL and UCF measure isotopic ratio of concentrations as a function of depth or at any point in sample
- We can map elements, isotopes over an area of about 1 cm<sup>2</sup>, and with a lateral resolution of about 1-2 μm, and depth resolution of about 10 nm.
- Future nano-SIMS integration with EBSD capability may enable measurement of:
  - *Diffusivities as a function of orientation in micro/nano grained materials*
  - *Grain boundary diffusivities*



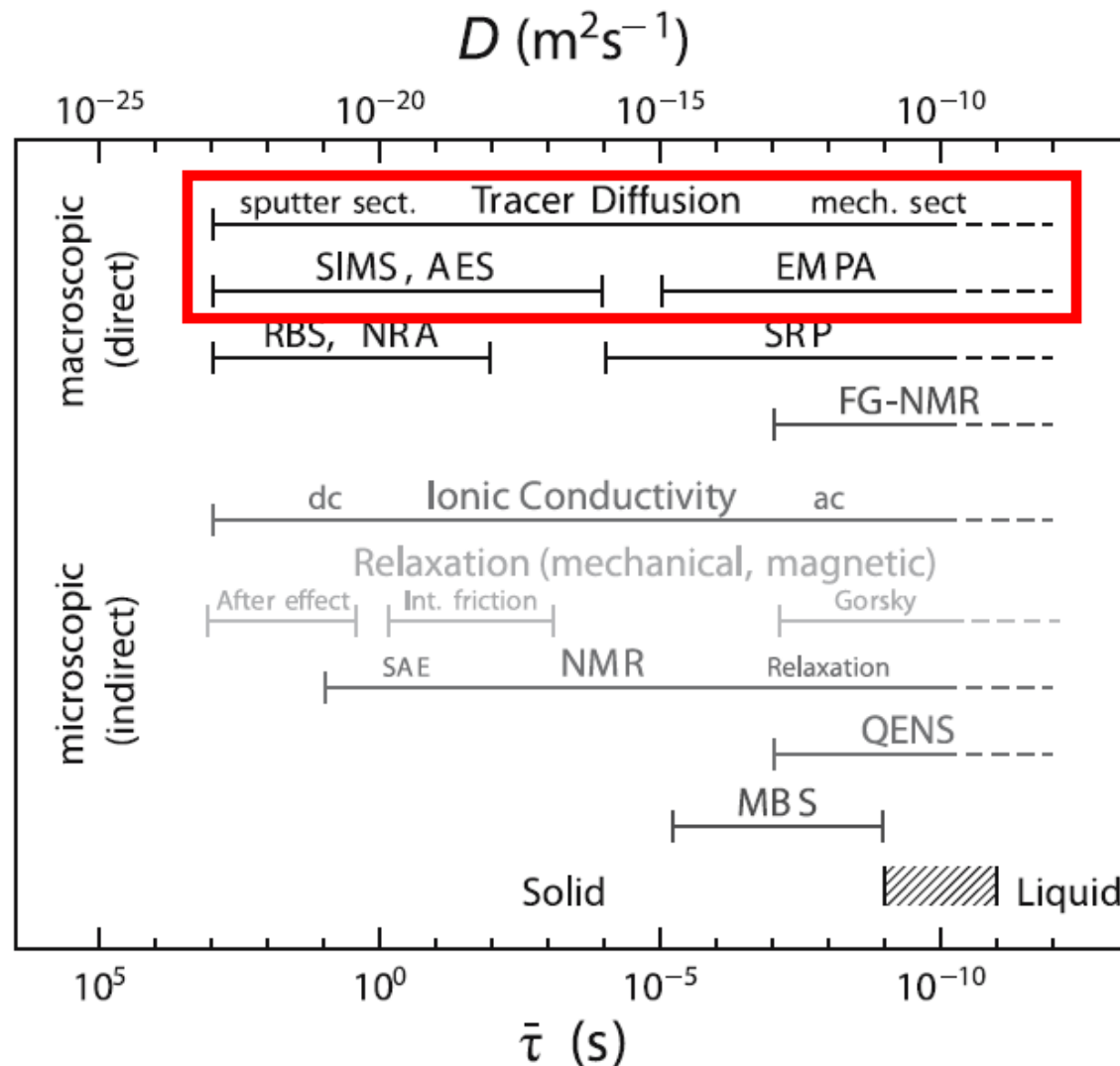
**Cameca IMS 4F at ORNL**



**Cameca IMS 3F at UCF**

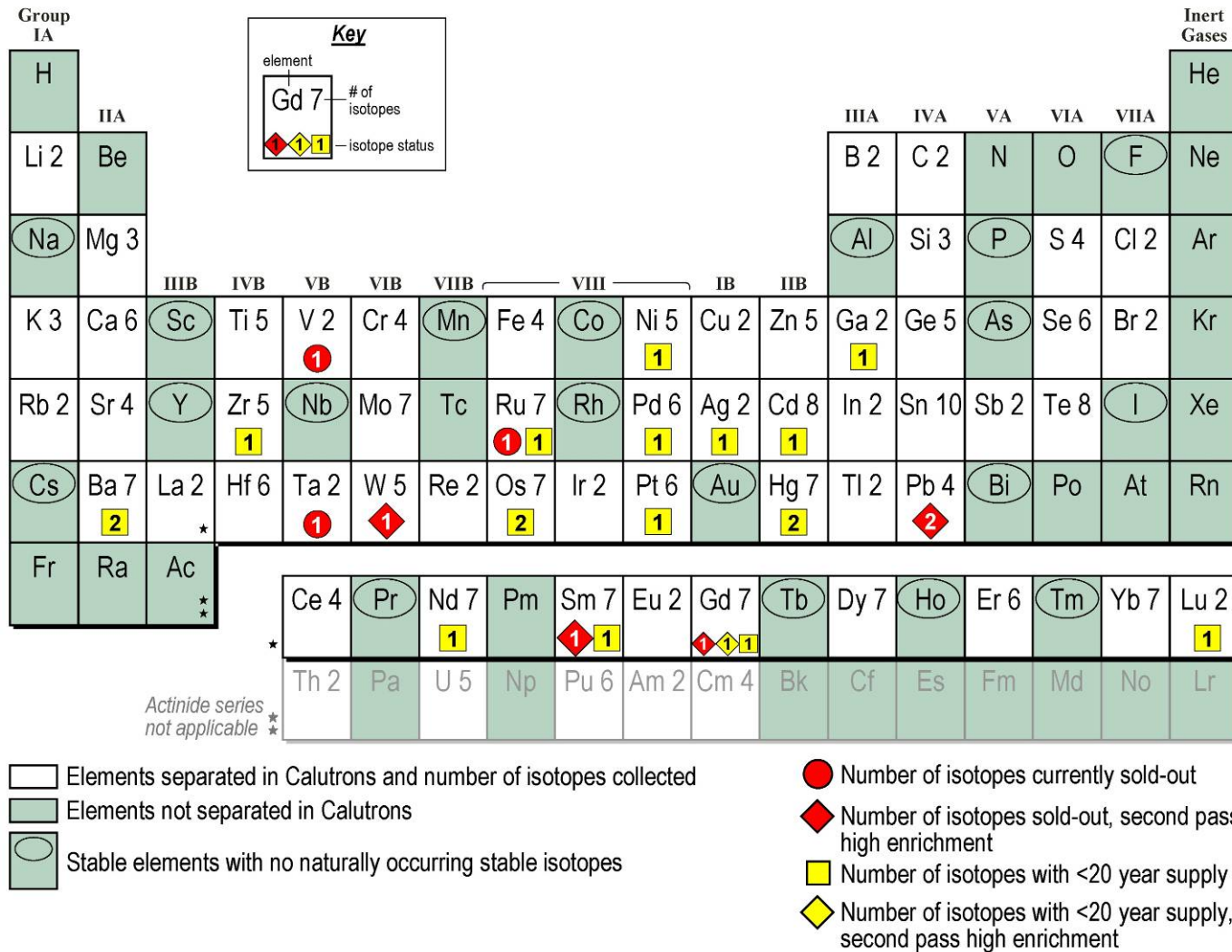


# Tracer Diffusion contd.



**Typical ranges of diffusivity (Mehrner, Diffusion in Solids)**

# ORNL Isotopes Enriched by the Calutrons



➤ Cannot avoid working with radioactive isotopes in some cases, e.g., Al, Mn, etc., but can still use SIMS

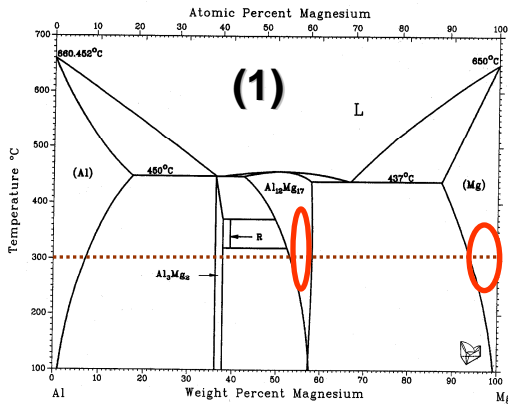
# Inventory ORNL Isotopes

\$360M\*  
Worth of  
Stable  
Isotopes

(\* list price)

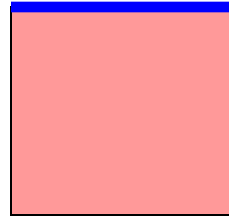


# Procedure for Tracer Diffusion Measurements (Review by Rothman)



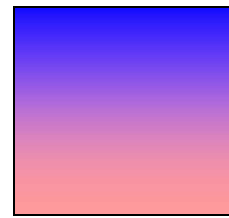
(1) Prepare single phase alloy sample (e.g., Mg-5%Al) at  $T_0$

(2)

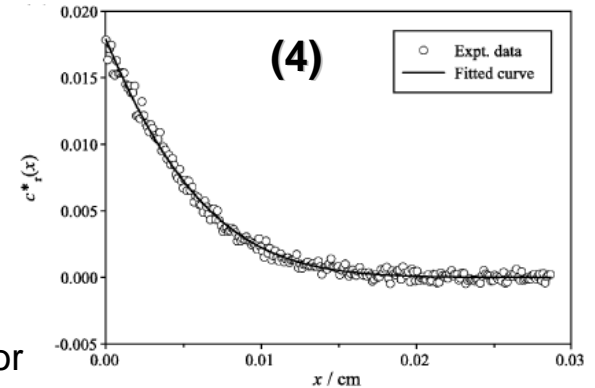


(2) Deposit thin film (100 nm) of stable isotope of an alloy element (e.g.,  $Mg^{26}$ ) on sample surface

(3)



(3) Anneal at  $T_0$  for desired times (mins to hrs) to cause isotope to diffuse inwards

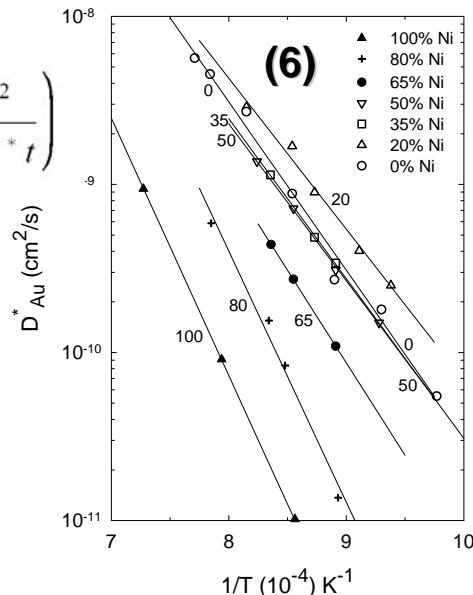


(4) Measure depth profile of isotope or isotope ratio with SIMS (e.g.,  $O^{18}$  with Time of Flight technique, *De Souza et al., Sol. State Ionics '05*)

(5)

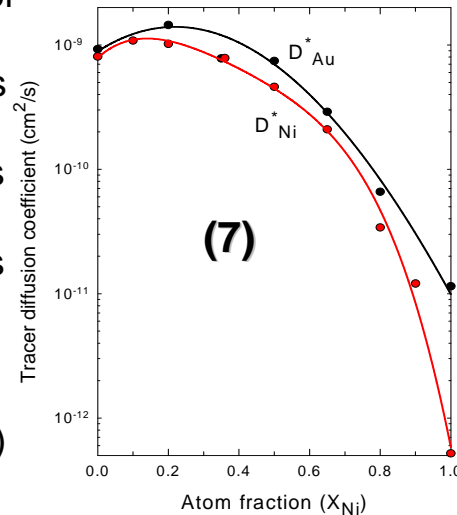
$$c^*(x,t) = \frac{S}{2\sqrt{\pi D^* t}} \exp\left(-\frac{x^2}{4D^* t}\right)$$

(5) Fit depth profile data for isotope in (4) with above thin film solution to extract tracer diffusivity  $D^*$ .



(6) Repeat for different temperatures and compositions to check for Arrhenius fits (e.g. Au in Au-Ni alloys, *Kurtz et al., Acta Met. '55*)

(7)

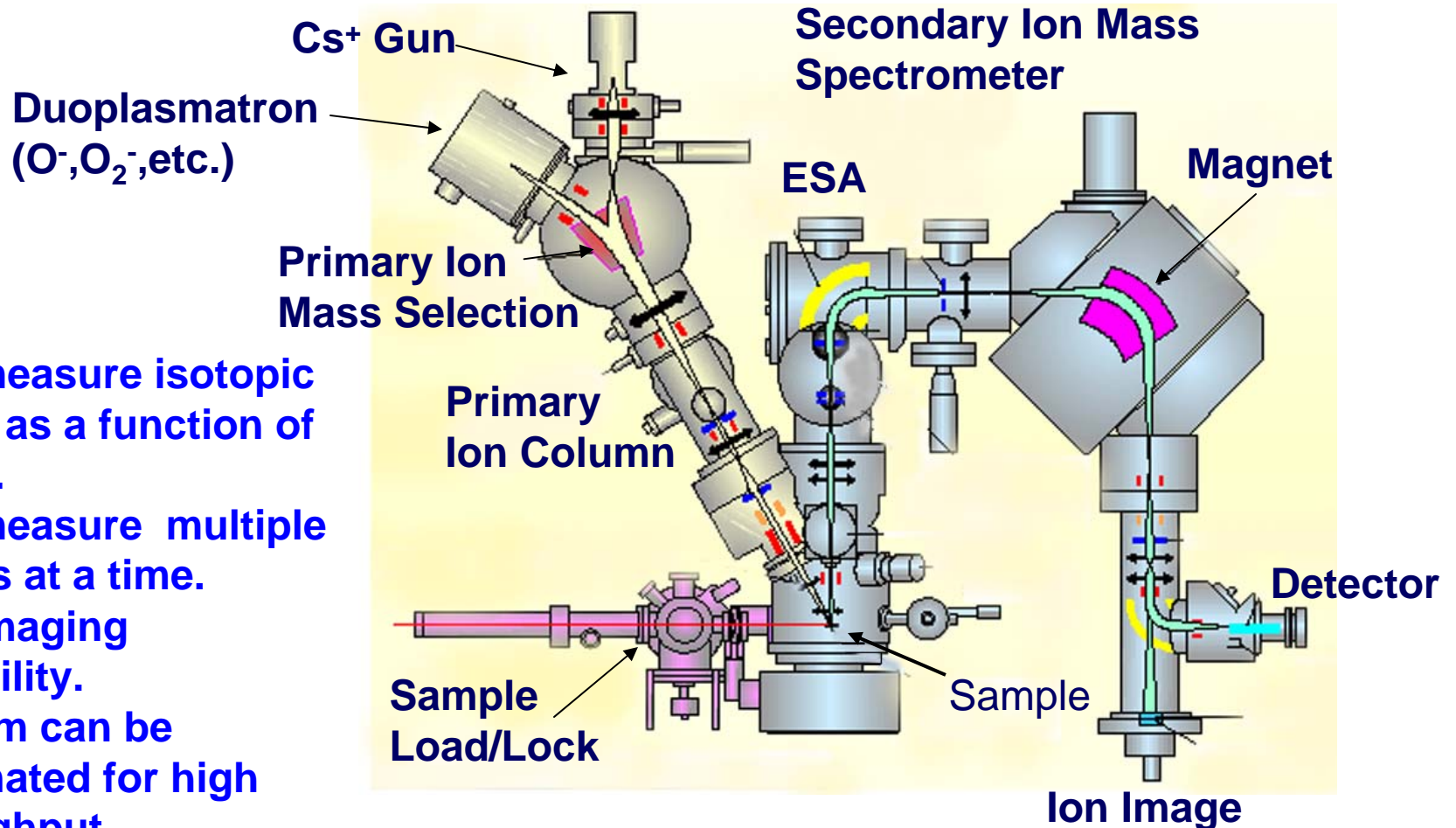


(7) Fit using suitable polynomials for functional form of isotopic diffusivity  $D_k^*(X_1, X_2, \dots, T)$  (e.g. Au-Ni tracer diffusion at 900°C, *Reynolds et al. Acta Met. '57*)

# SIMS: ORNL (CAMECA IMS-4F) & UCF (IMS-3F) \$2-3M

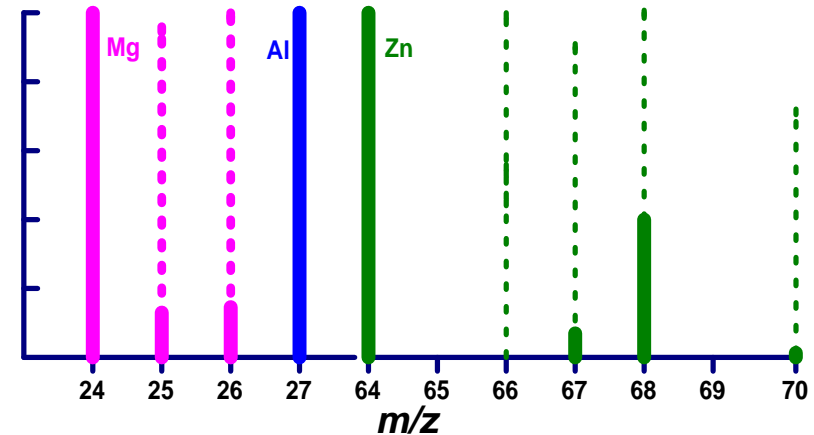
**Cameca ims-4f Ideally Suited for Isotope Ratio Depth Profiles  
High Spatial Resolution (1 $\mu$ m), High Mass Resolution, High Sensitivity**

- ✓ Can measure isotopic ratios as a function of depth.
- ✓ Can measure multiple beams at a time.
- ✓ Has imaging capability.
- ✓ System can be automated for high throughput measurements of samples on a wafer.



**Our Modifications – Increase Flexibility, Compatibility  
with SEM, Optical Microscopes, Reliability**

# Stable Isotopes Available [Not Radioactive]



Isotopically Labeled Alloy



Isotope Ratio

$\Delta$  Isotope Ratio Measured

Headroom

Ratios, e.g.  $[^{26}\text{Mg}]/[^{24}\text{Mg}] = 14.04\%$

Nat. Ab., e.g.,  $[^{25}\text{Mg}]/[^{24}\text{Mg}] = 13.90\%$

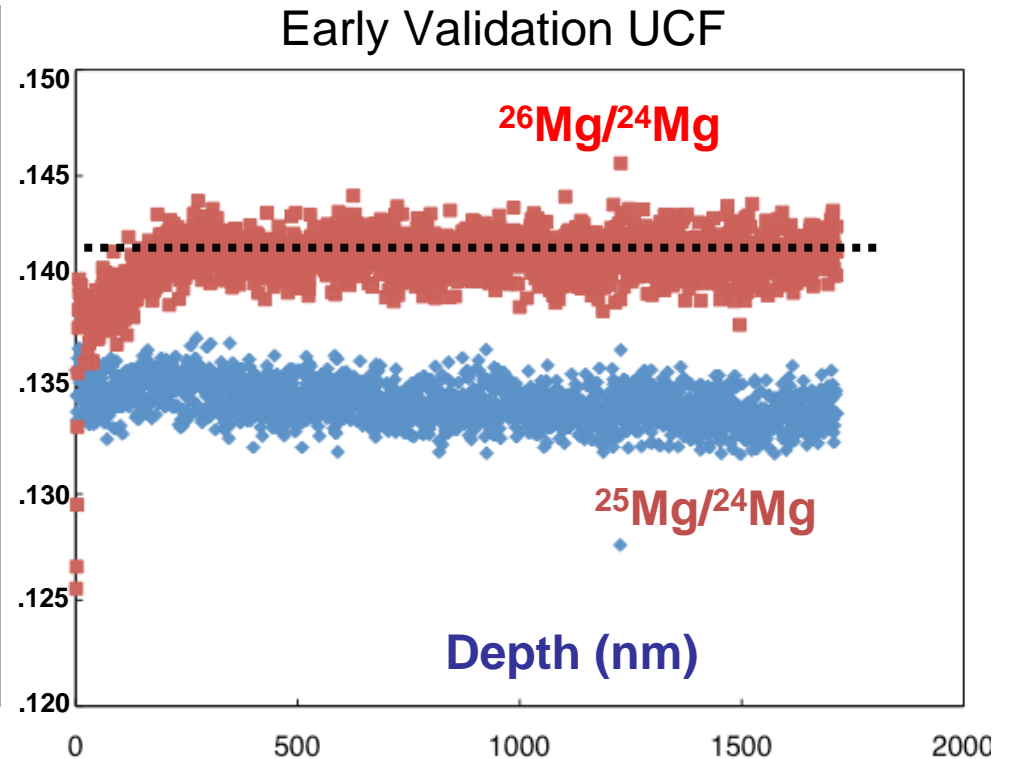
...1% difference readily detected.

100% Available: ca.  $10^4$  Headroom



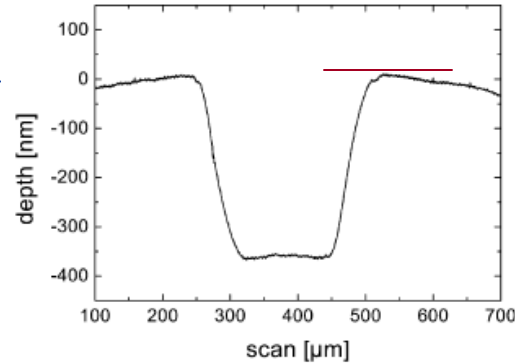
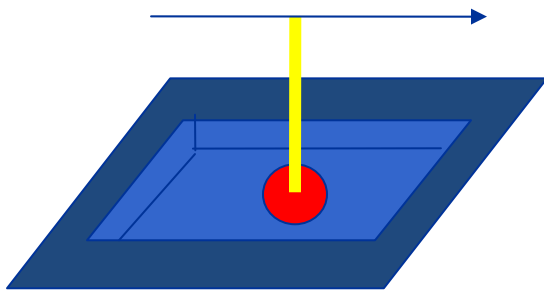
# Isotope Ratios Readily Measured...

Cameca 3F UCF	$^{25}\text{Mg}/^{24}\text{Mg}$ (RSD)	$^{26}\text{Mg}/^{24}\text{Mg}$ (RSD)
Reference value	0.127	0.139
Mg	0.129 (<0.001)	0.138 (<0.001)
Mg-Al-Zn	0.130 (<0.001)	0.139 (<0.001)
AZ31B-2	0.129 (<0.001)	0.138 (<0.001)
AM60B-2	0.130 (<0.001)	0.139 (<0.001)



**Measurements independent of depth within 1% Relative Standard Deviation**

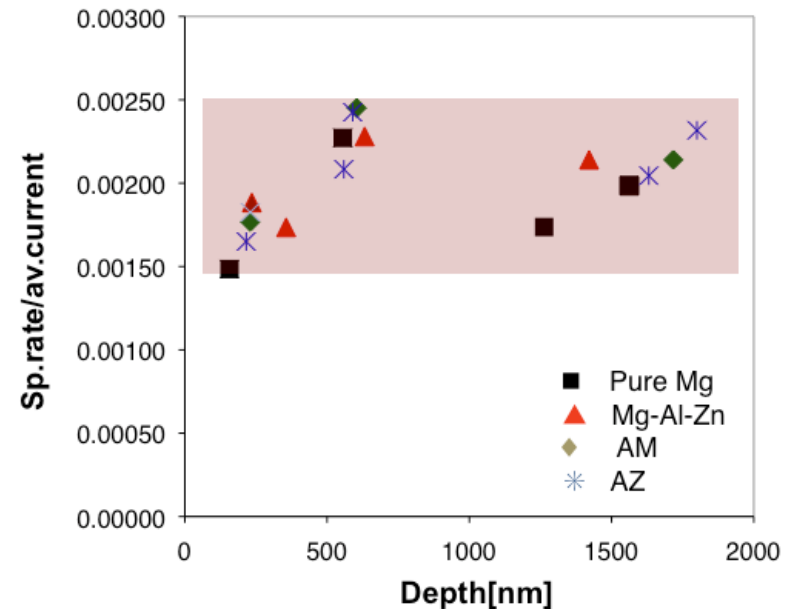
# Sputtering Depth: Precisely Measured



**Profilometer**  
Resolution: < 0.1 nm  
Accuracy: Surface

***Real Data***

- Sputtering Rate Uncertainty (uncertainty Primary Ion Current )
- Measure depth of each crater
- Sputter Rate Only for Scoping



## Assumption

For any Given Crater, given primary ion current, Sputtering Rate Constant ... if Not Known Precisely

**Standard: Si Sputtering**

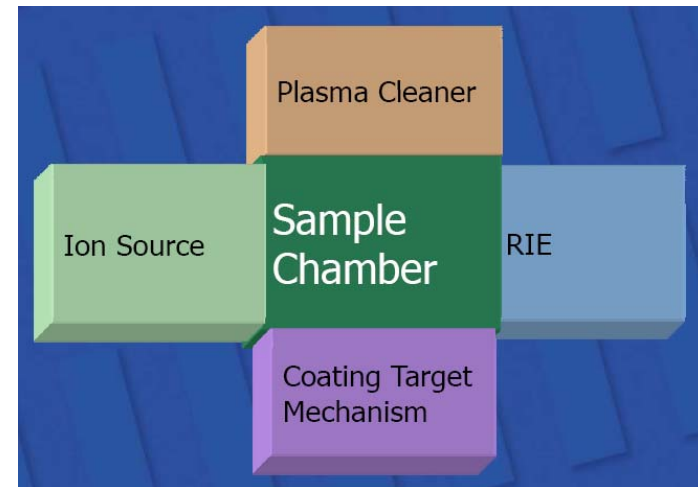
Primary Ion Current:  
ca. 10-100 nA  
Spot Size: 1-10 μm

**Sputter Rate vs. Depth**



# Vapor Deposition of Stable Isotopes – Automated Sample Preparation System (ASAP)

- Clean, planarize sample surface prior to sputter deposition
  - Plasma Clean (PC)
  - Ion Beam Etching (IBE)
  - Reactive Ion Etching (RIE)
  - Ion Beam Sputter Coating (IBSC)
- Pure atmosphere (Ar) during ion beam sputter deposition
  - Attempts to increase deposition rate (Xe?)
  - Metal getter system, in-situ gettering being explored
- Load lock – multiple sample capability
- **Controlled thickness, automation**

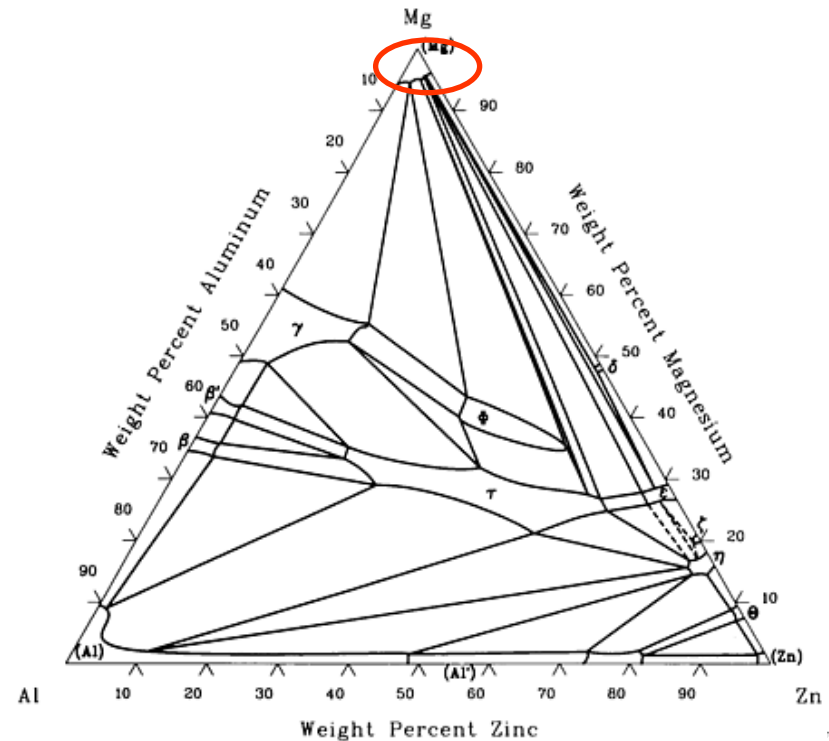
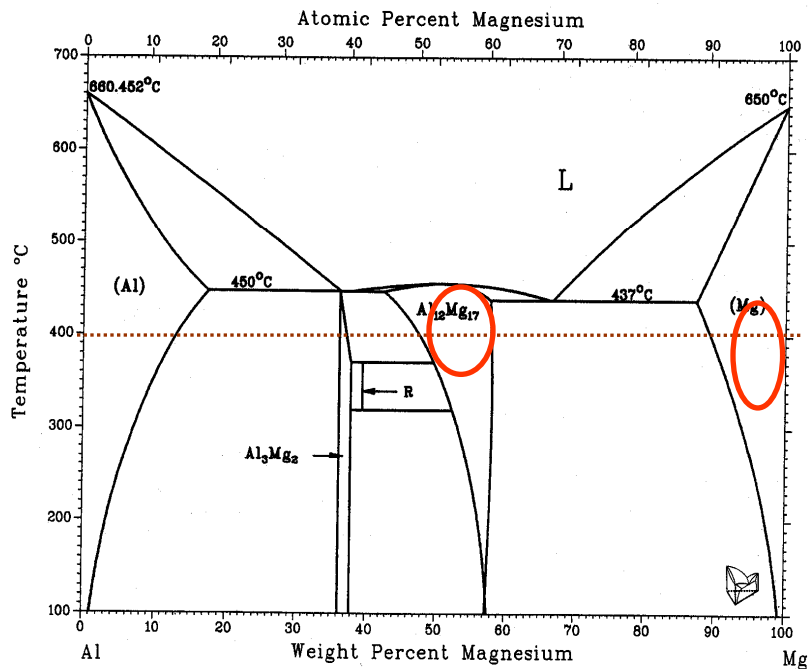


Top  
view



# Current Work in Mg-Al-Zn (Mg rich phase)

- Impurity diffusion (Al, Zn) studies in Mg.
- Improvements in current ion beam sputter tool to minimize oxygen levels in Mg isotope film.
- Future years: Mg-Al-Mn and Mg-Al-Zn-Mn



# Summary

- Justification for effort
    - Clarity and specificity
  - Address technical issues
    - Volume databases alone may not be sufficient
      - Grain boundary, orientation effects
    - 1D Software for bulk diffusion may not be enough
      - Thin films, non-planar interfaces, varied boundary conditions
  - Tracer diffusion databases
    - Stable isotopes to the rescue but not always (Al, Pb, Mn, etc.)
    - Free of major assumptions
    - Independent of thermodynamics
    - Can assess newer/improved formalisms as they develop
    - Amenable to a variety of driving forces
    - Necessary for line compounds, grain boundary measurements, ...
    - Instrumentation/experimentation challenges & costs are significant
- 43 Managed by UT-Battelle for the U.S. Energy Research Office
- National Labs/Centers can play a major role

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Yongho Sohn, Mikhael Klimov, Kevin Coffey: UCF**

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Automotive Lightweight Materials Program  
Oak Ridge National Laboratory**