

Designing a Cross-Slot for Extensional-FlowSANS

Shooting Neutrons at Soap

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Complex Fluids and Flow

Consumer Products



Polymer processing and extrusion



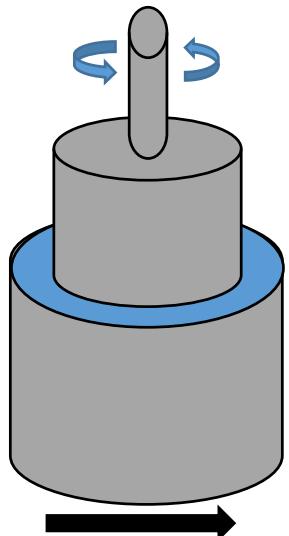
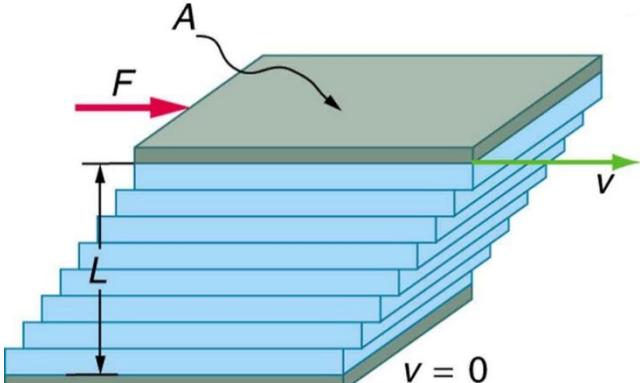
Processing and delivery of pharmaceuticals



Shear and Extensional Flow



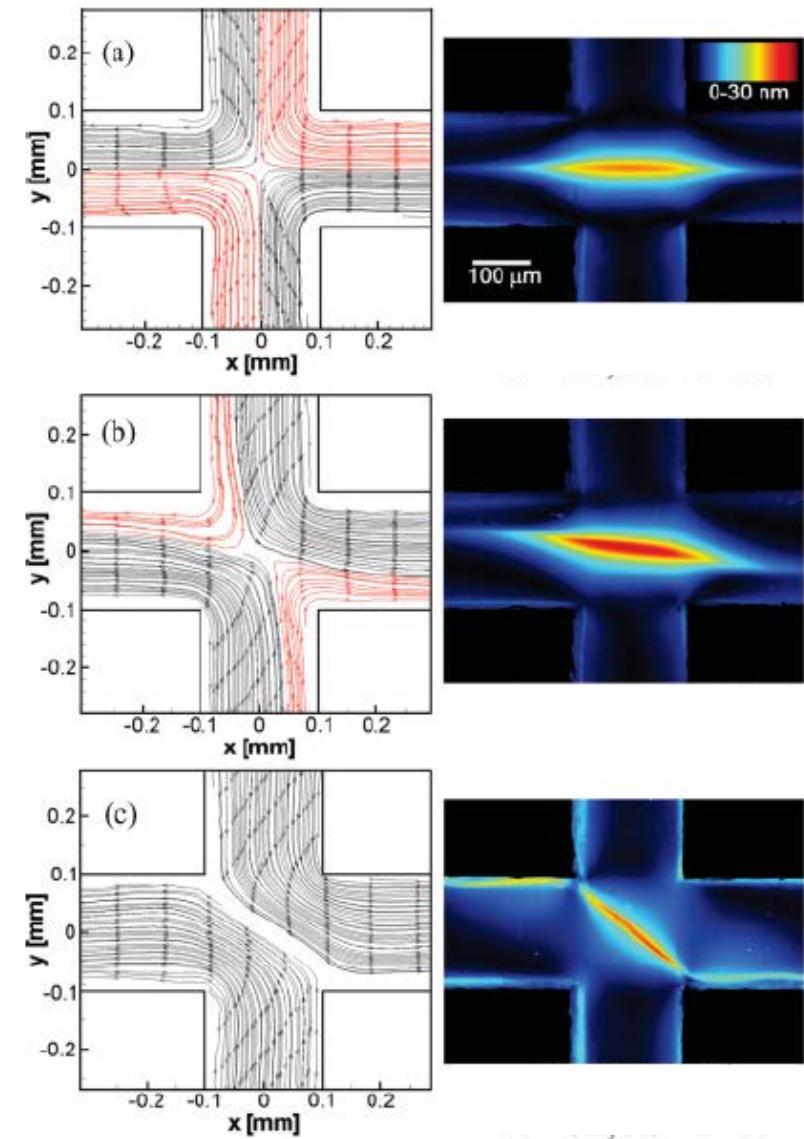
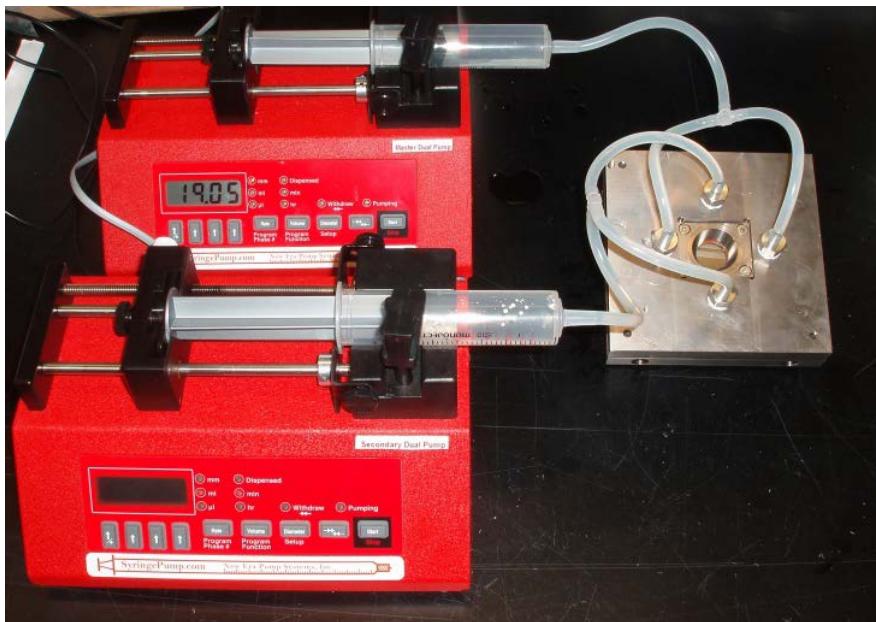
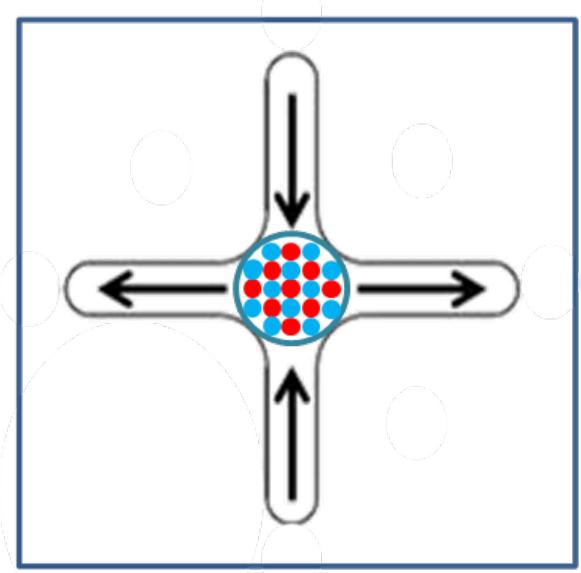
Shear Strain



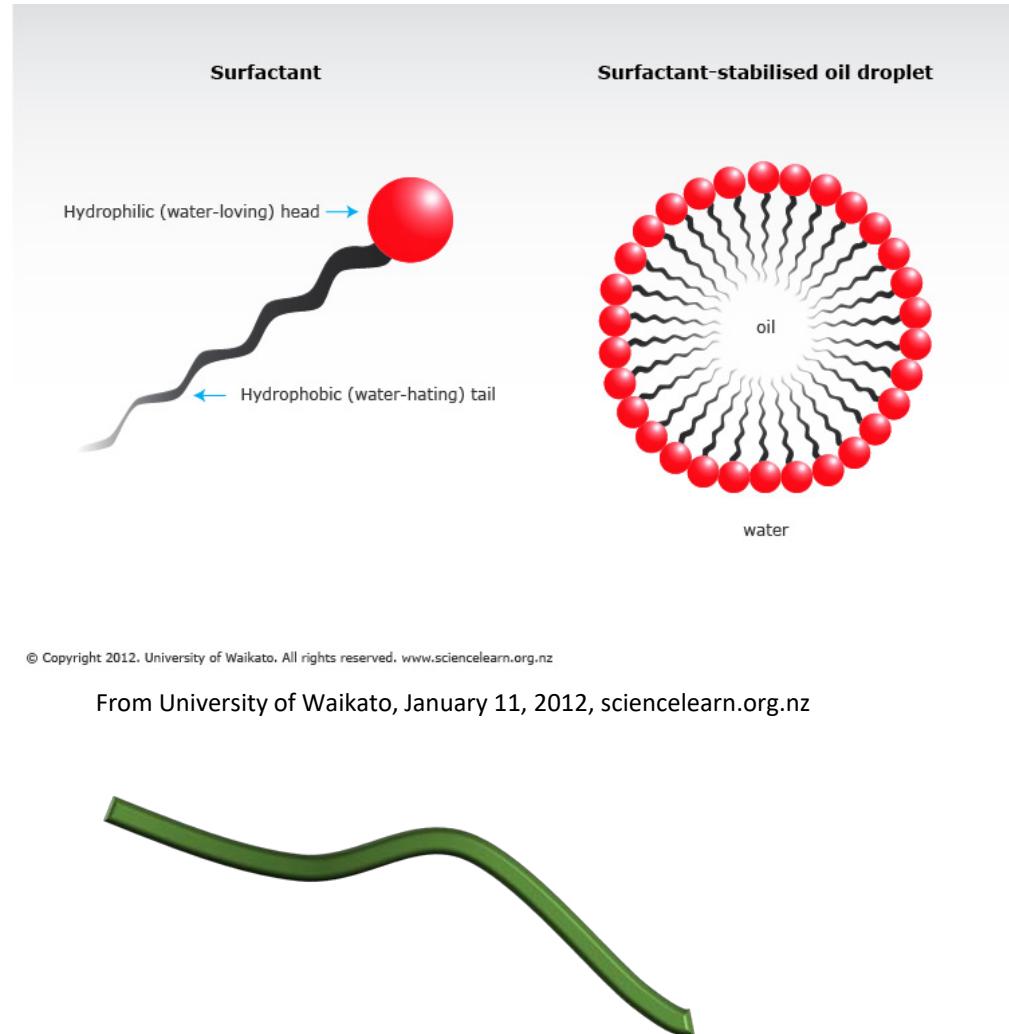
Extensional Strain



Cross-Slot Flow Cell



Wormlike Micelles (WLM)



$75\text{mM CPyCl}/45\text{ mM NaSal in D}_2\text{O}$
 $\tau_r \approx 7\text{ sec}$

Personal care products

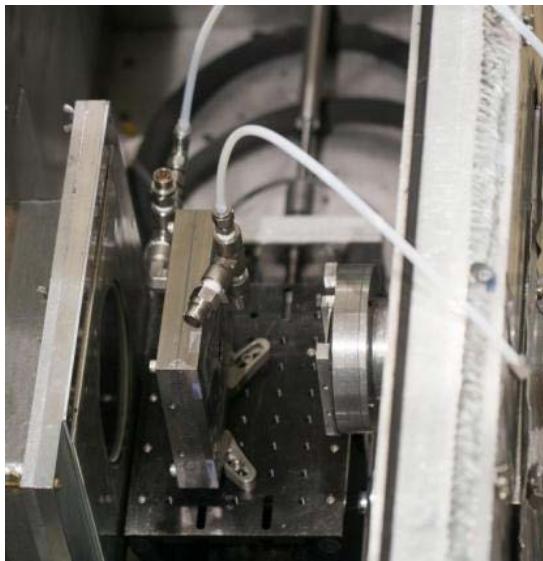
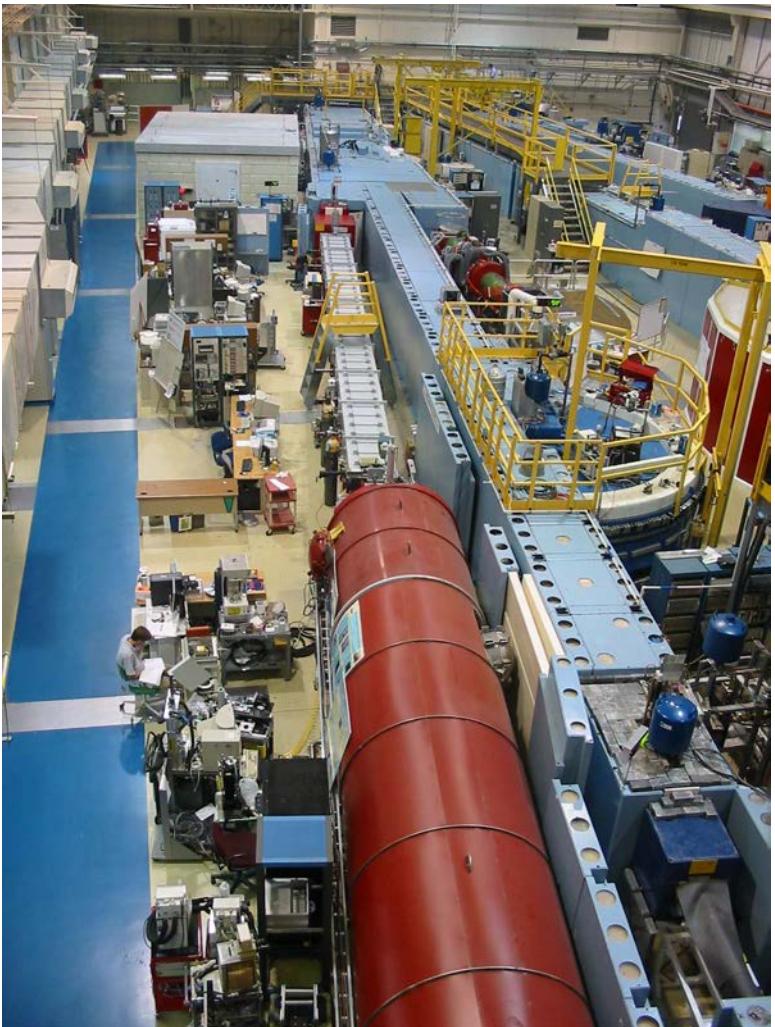


Home care products



Oil recovery and fracking
Drag reducers

Small Angle Neutron Scattering



NCNR."NG7."www.ncnr.nist.gov

Why Small Angle Neutron Scattering?

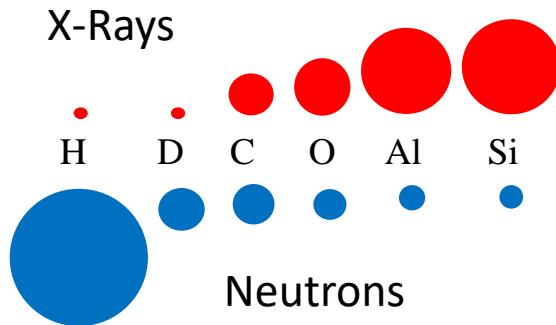
Characterize structures from 1 nm – 500 nm



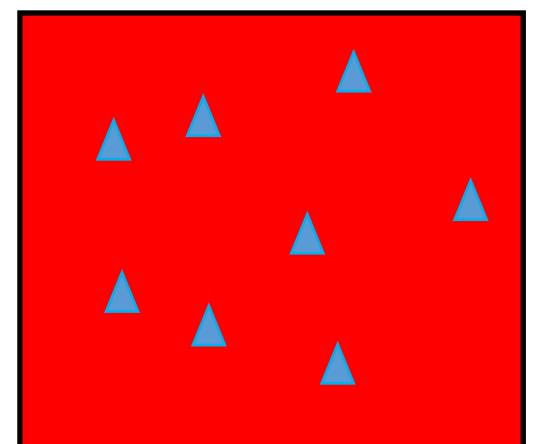
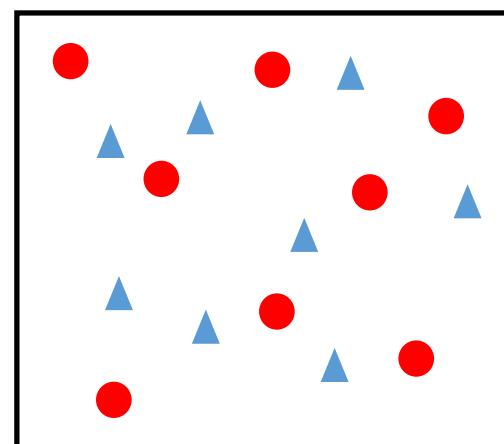
Transparency



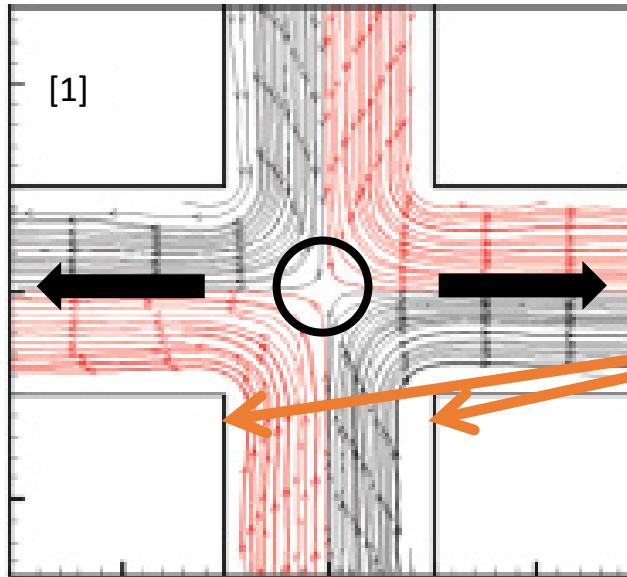
Scattering Cross-Sections



Contrast Variation



Extensional Flow within a Cross Slot



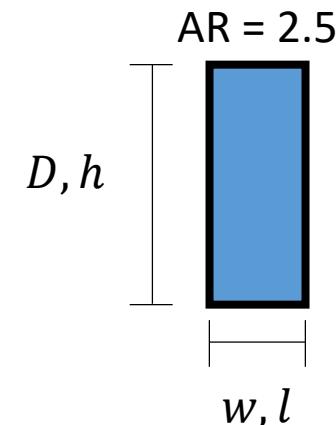
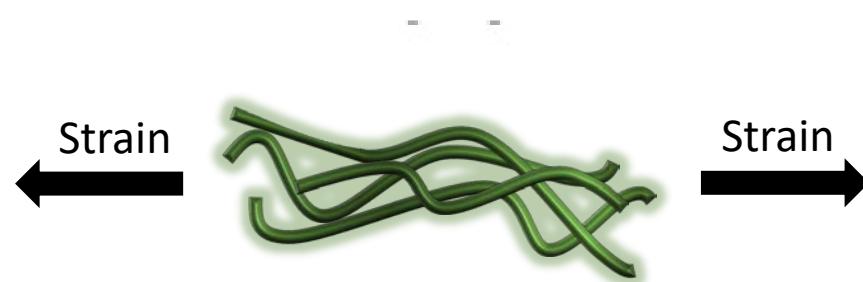
Plug-like flow:

$$\dot{\epsilon}_{nom} = \frac{Q}{w^2 D} [1]$$

$$\dot{\gamma}_{wall} = \frac{6Q}{l^2 h}; l < h \text{ (Newtonian Fluid)}$$

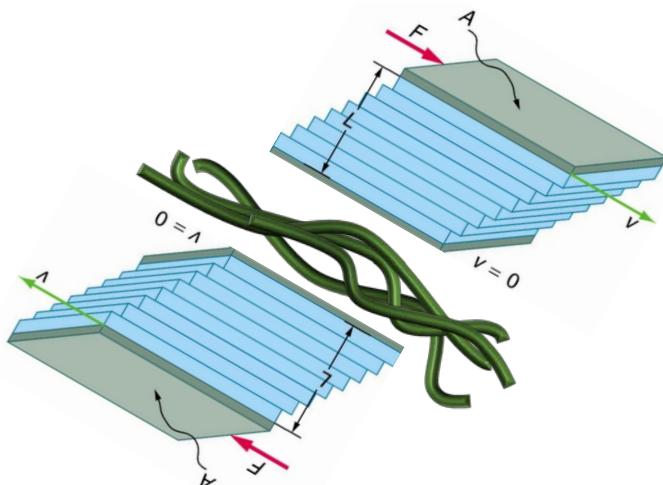
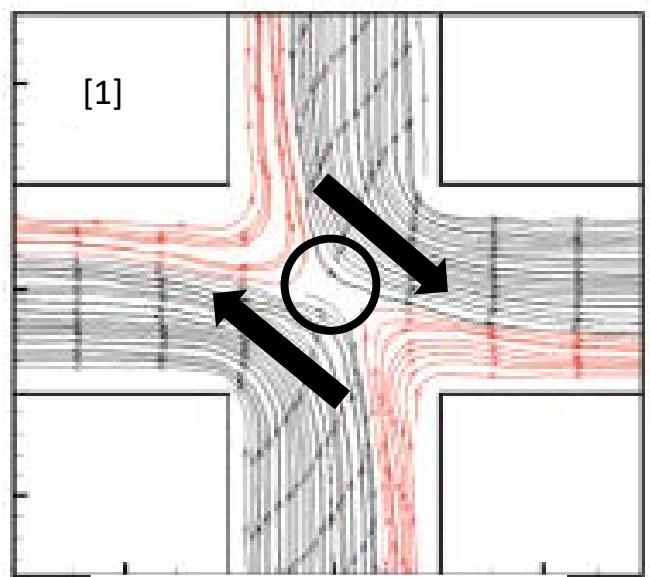
$$AR = \frac{D}{W}$$

$$AR = .1$$

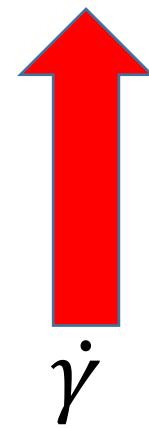
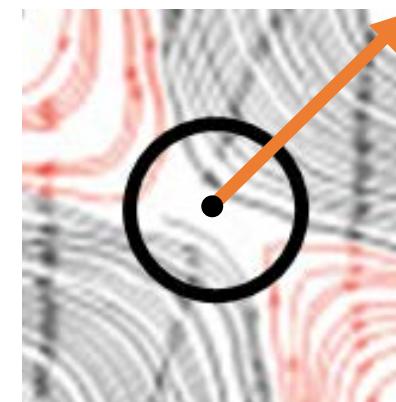


Aspect ratios of 2.5, 1.7, 1, 0.7, 0.1

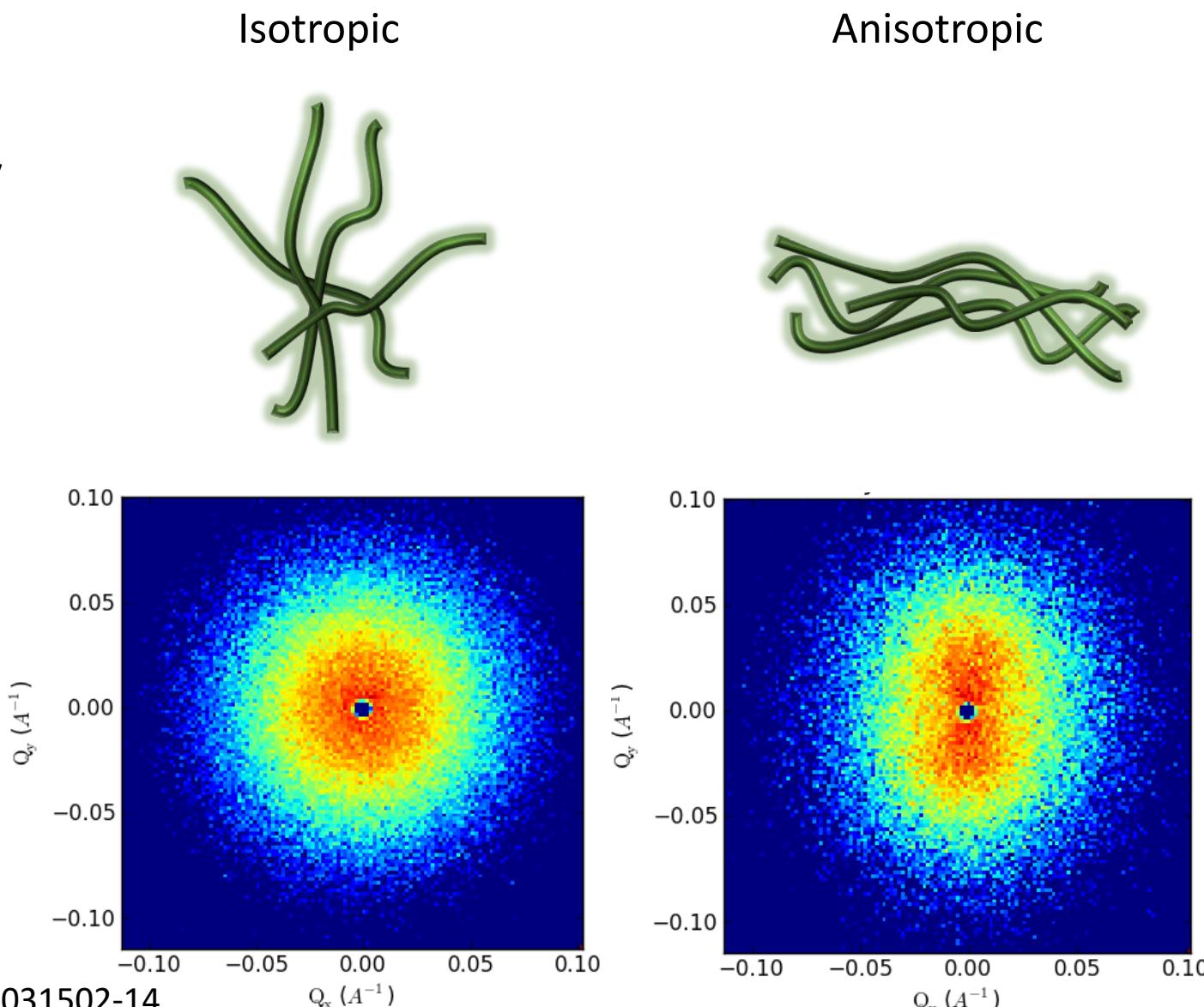
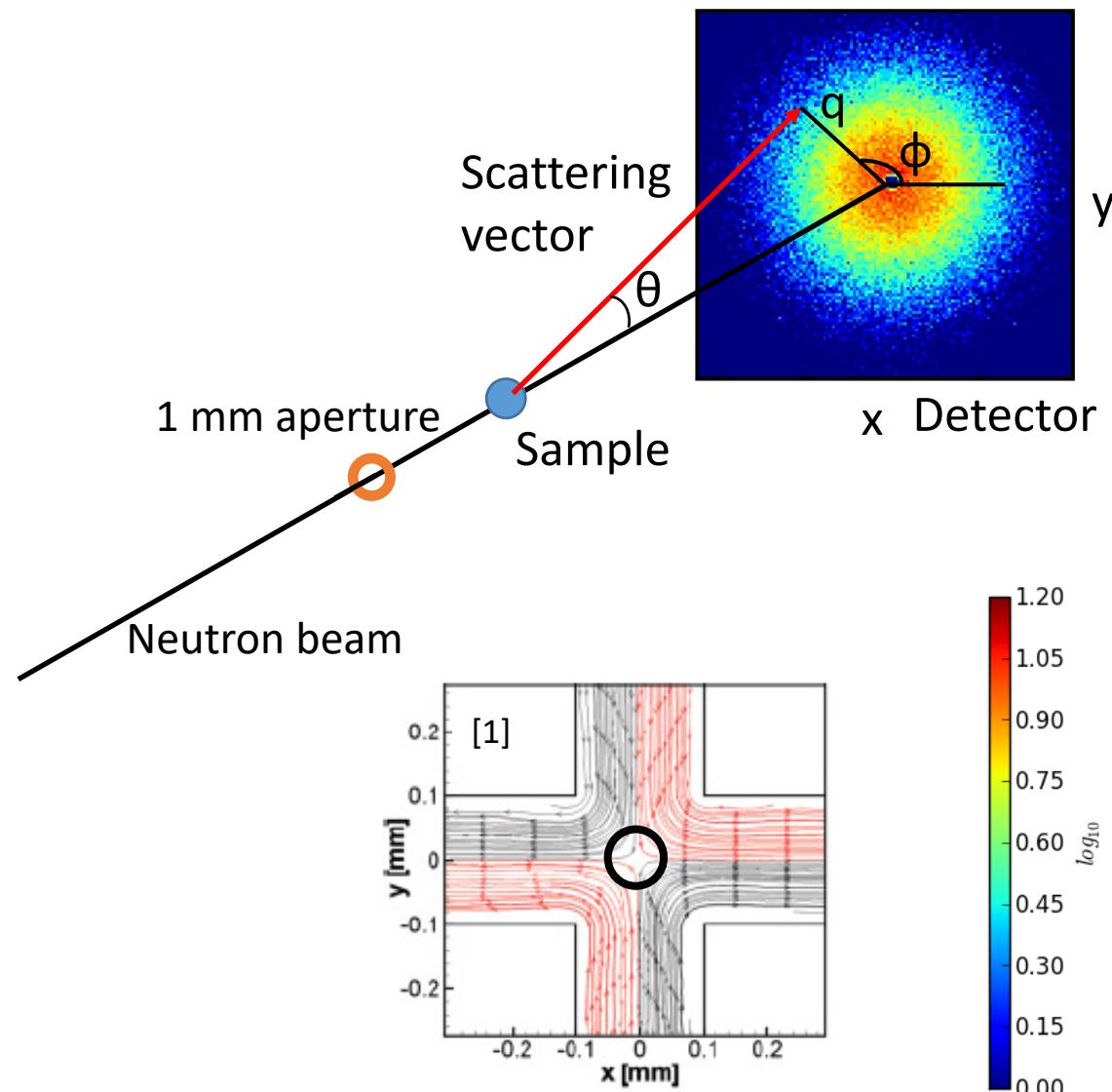
Asymmetric Flow within a Cross Slot



Occurs when $\dot{\epsilon} > \dot{\epsilon}_c$



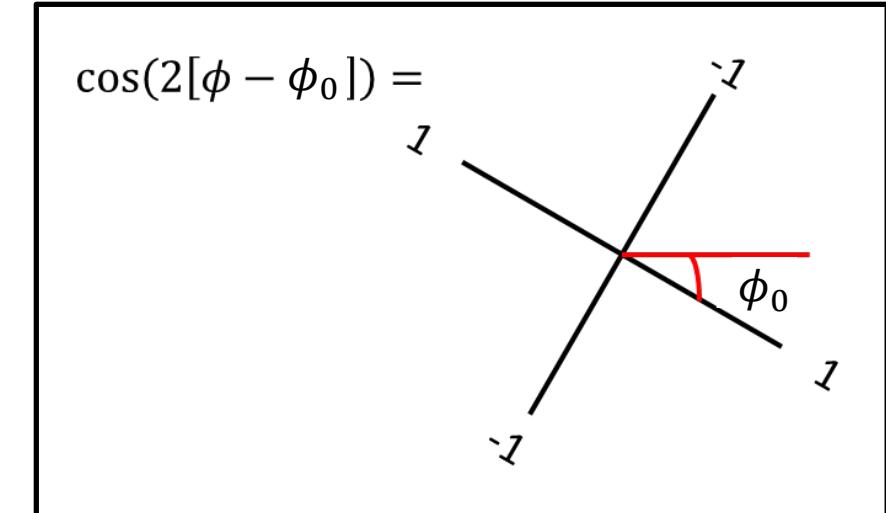
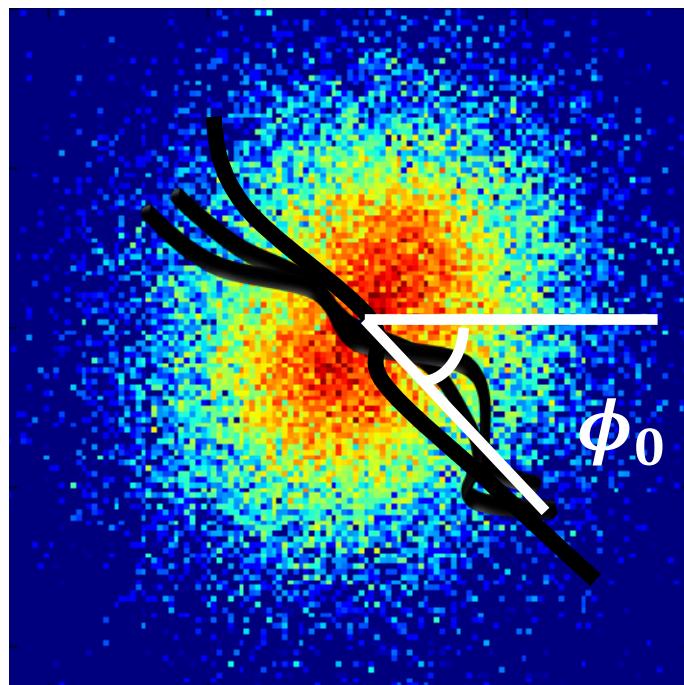
Small Angle Neutron Scattering (SANS)



Alignment Factor

$$A_f(q) = \frac{\int_0^{2\pi} I(q, \phi) \cos(2[\phi - \phi_0]) d\phi}{\int_0^{2\pi} I(q, \phi) d\phi}$$

$$-A_f(q \geq 0.03 \text{ } A^{-1}) \approx S_m$$
^[2]



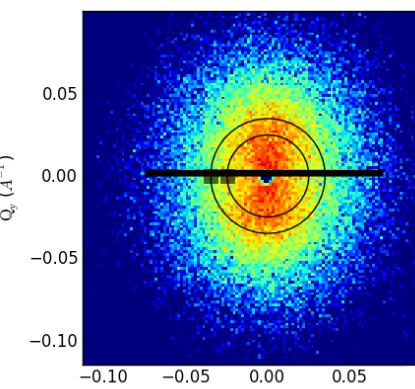
Nematic Orientation Parameter

$$I(\phi) = \sum_{n=0}^{\infty} \left\{ \frac{(-1)^n (2n)!}{4^n n! n!} a_n P_{2n}(\cos(\phi - \phi_0)) \right\}$$

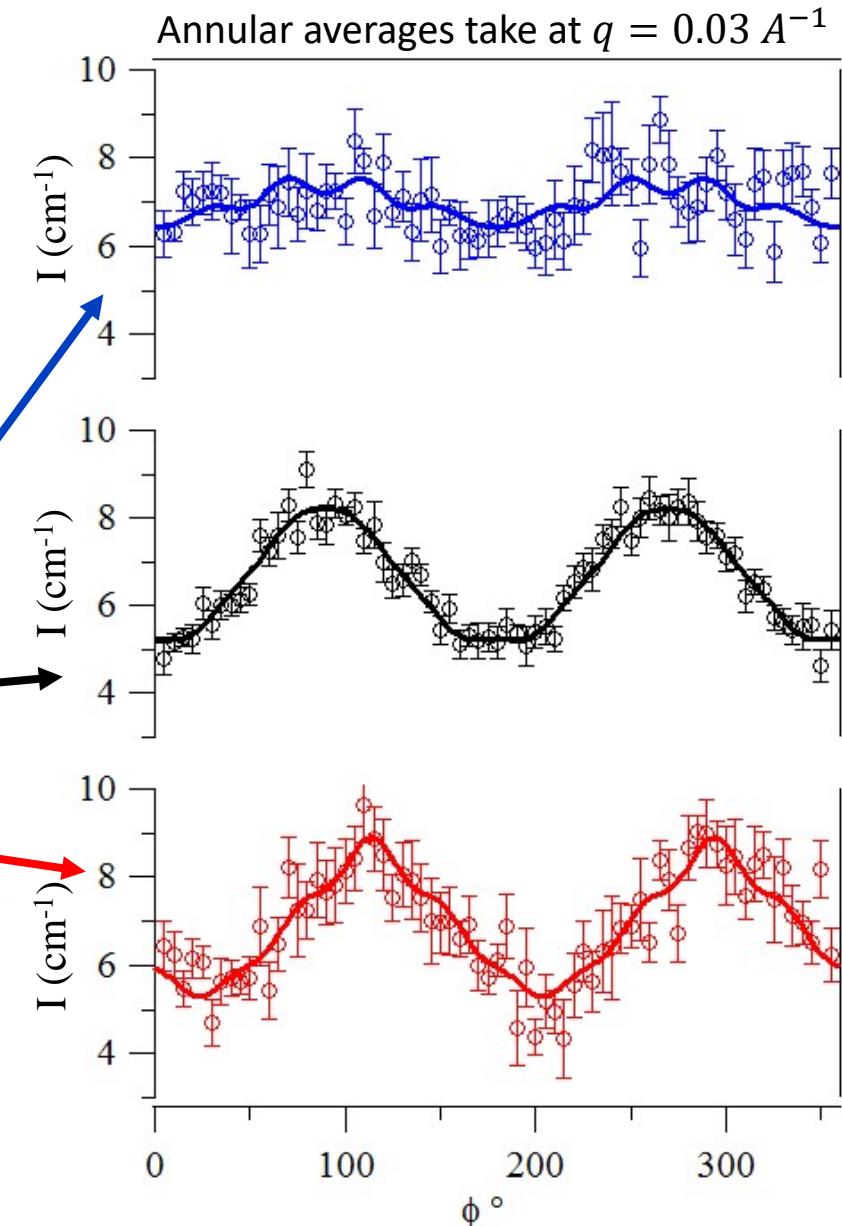
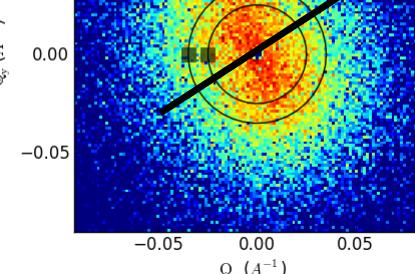
$$\bar{P}_2 = \frac{a_1}{5a_0}$$

$$\begin{aligned}\bar{P}_2 &= 0.0321 \\ \phi_0 &= N/A\end{aligned}$$

$$\begin{aligned}\bar{P}_2 &= 0.1224 \\ \phi_0 &= -0.4^\circ\end{aligned}$$



$$\begin{aligned}\bar{P}_2 &= 0.1127 \\ \phi_0 &= 24^\circ\end{aligned}$$

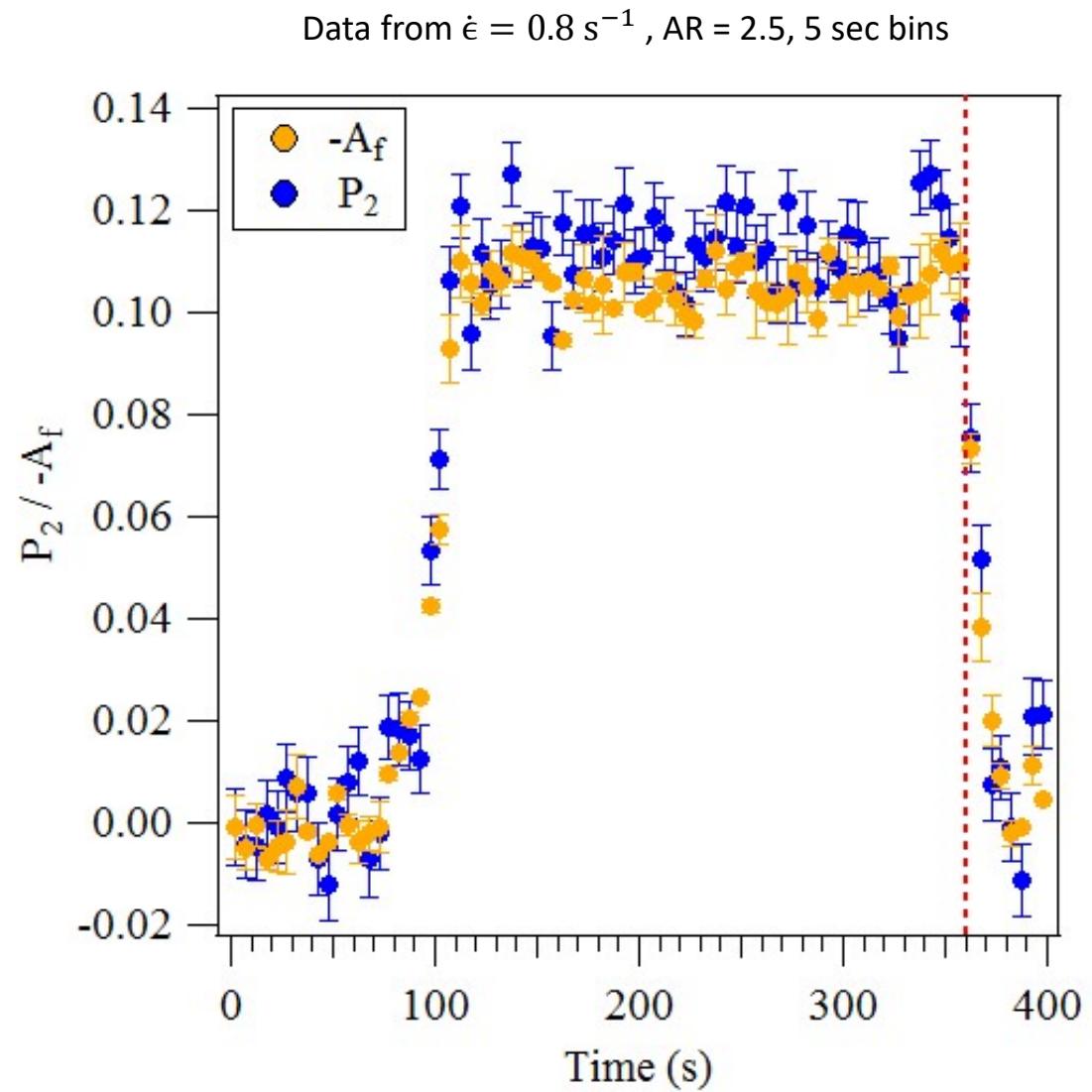


\overline{P}_2 and A_f

ODF: $g(\beta) = \sum_{n=0}^{\infty} a_n P_{2n}(\cos\beta)$

$$\overline{P}_2 = \left\langle \frac{3\cos^2(\beta)-1}{2} \right\rangle = 1 - \frac{3}{2} \overline{\sin^2(\beta)} = S_m^{[3]}$$

Therefore $\overline{P}_2 \approx -A_f$ ($q \geq 0.03 A^{-1}$)

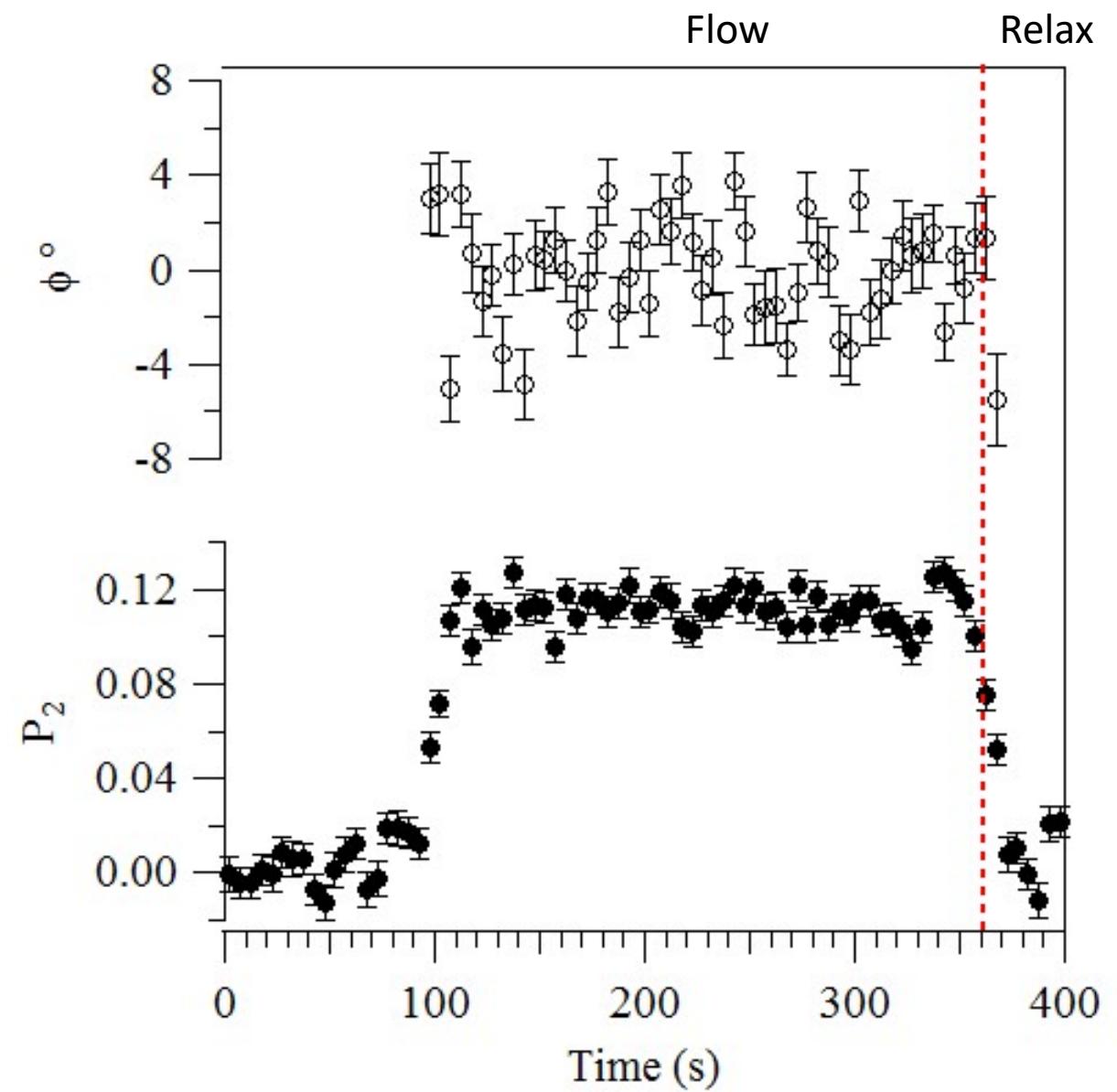
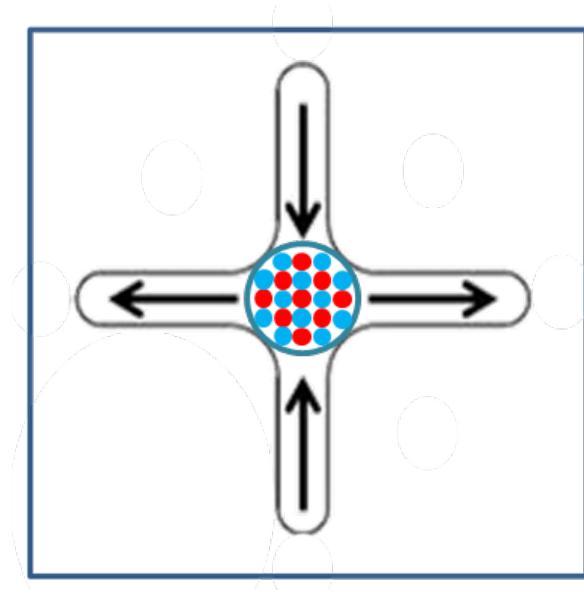


$\dot{\epsilon} = 0.8 \text{ s}^{-1}$ Time Resolved

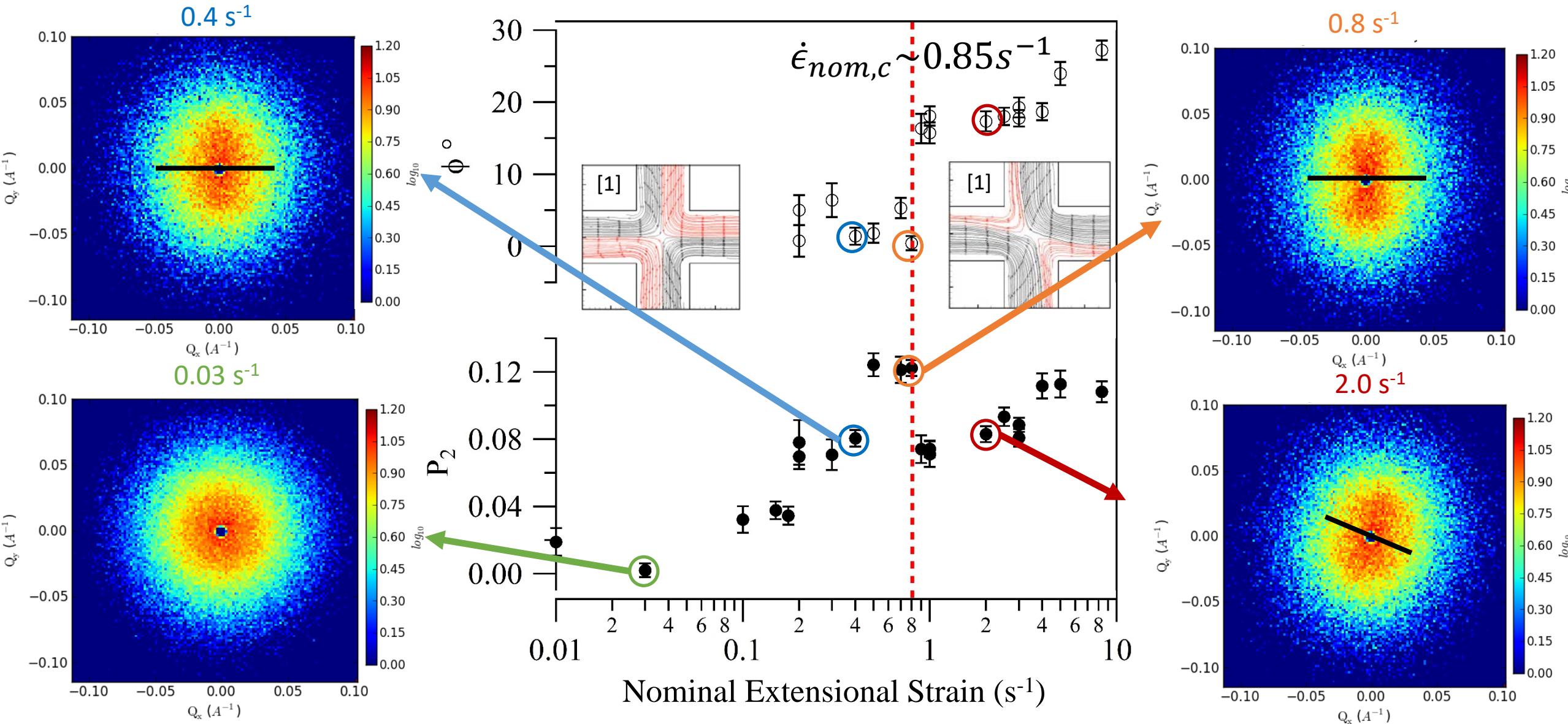
Steady state orientation is reached after $\sim 110\text{s}$

$$\bar{P}_2 = 0.12$$

$$\phi_0 = 0$$



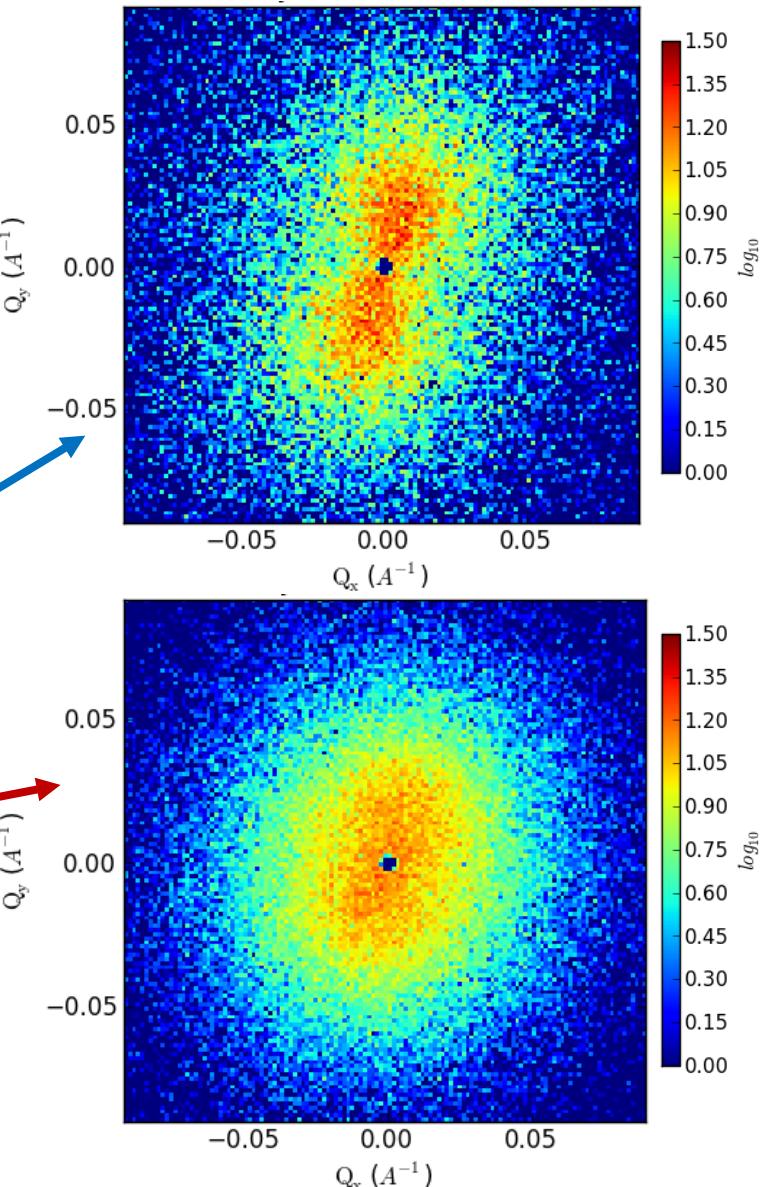
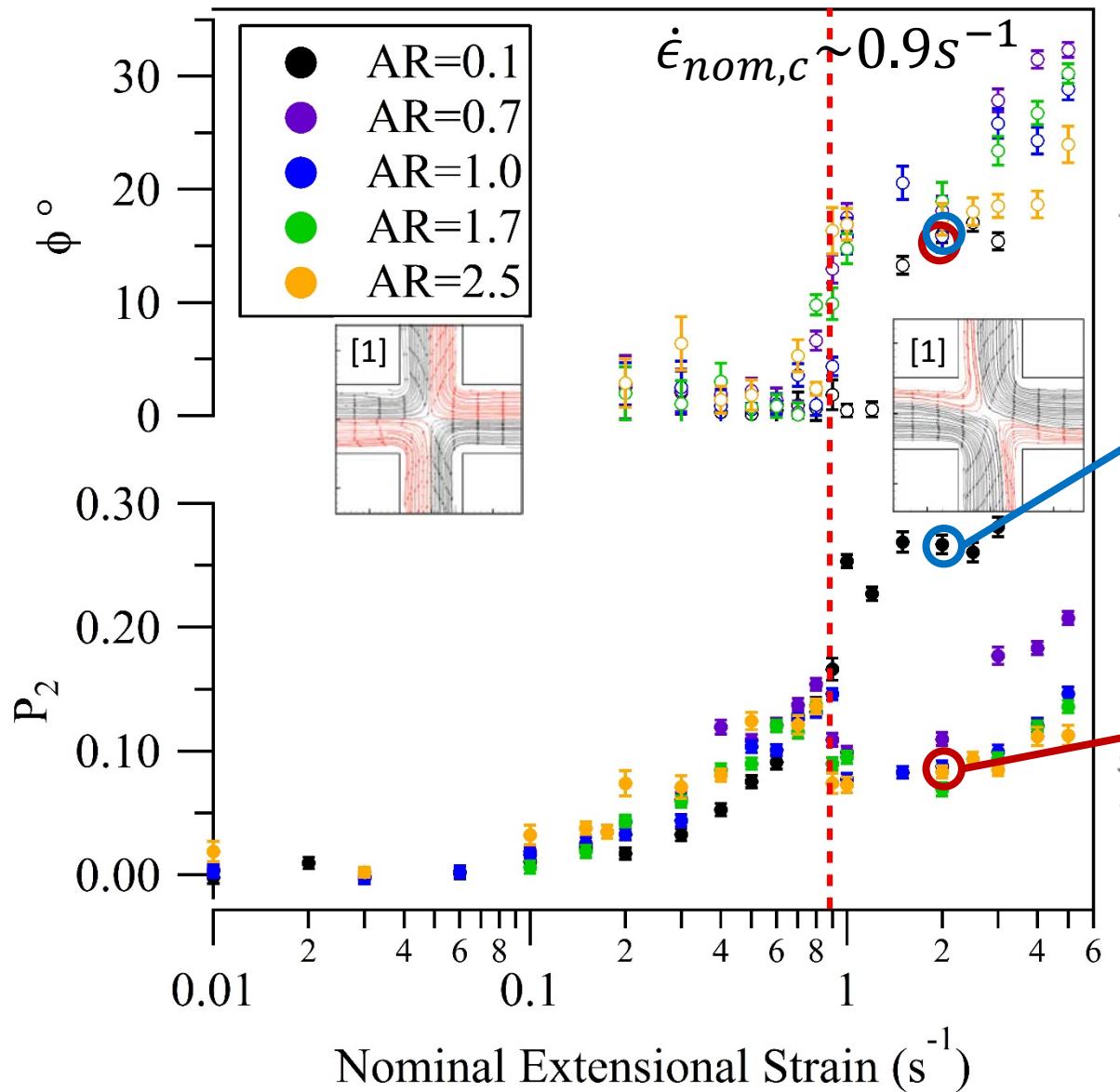
Equilibrium Structure (AR=2.5)



Orientation for Different Aspect Ratios

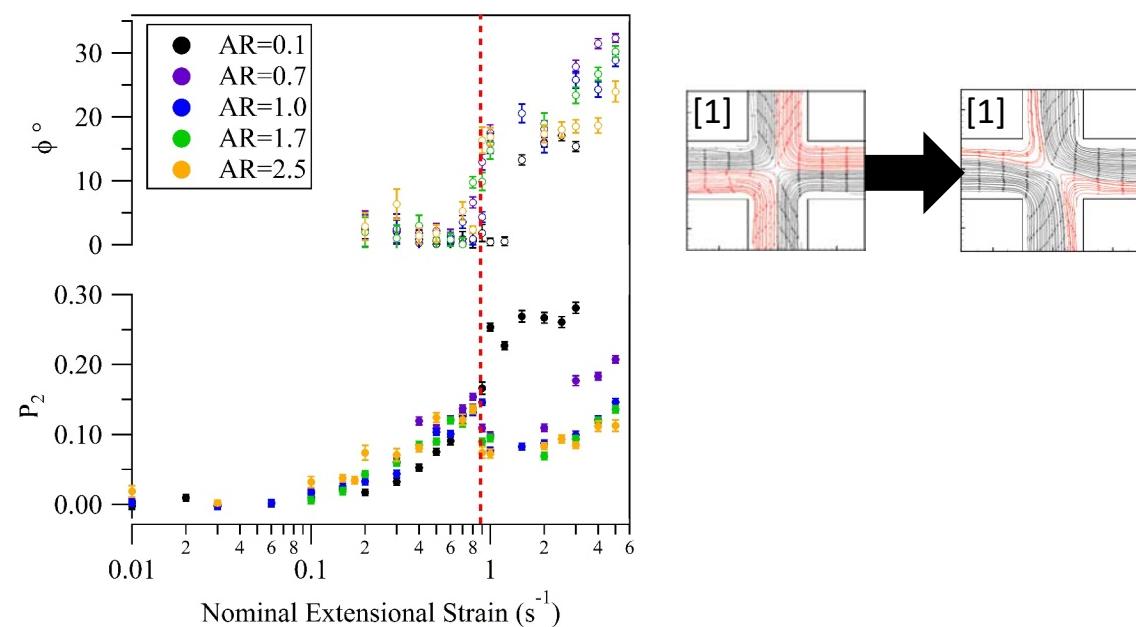
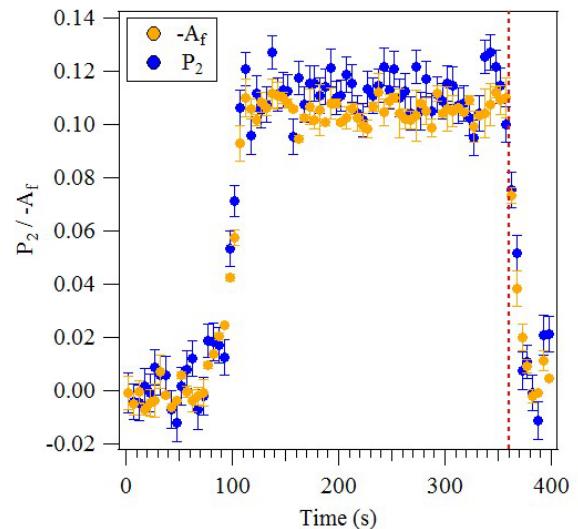
$\dot{\gamma}_{wall}$ is negligible

$$\dot{\epsilon}_{nom} = \frac{Q}{w^2 D}$$

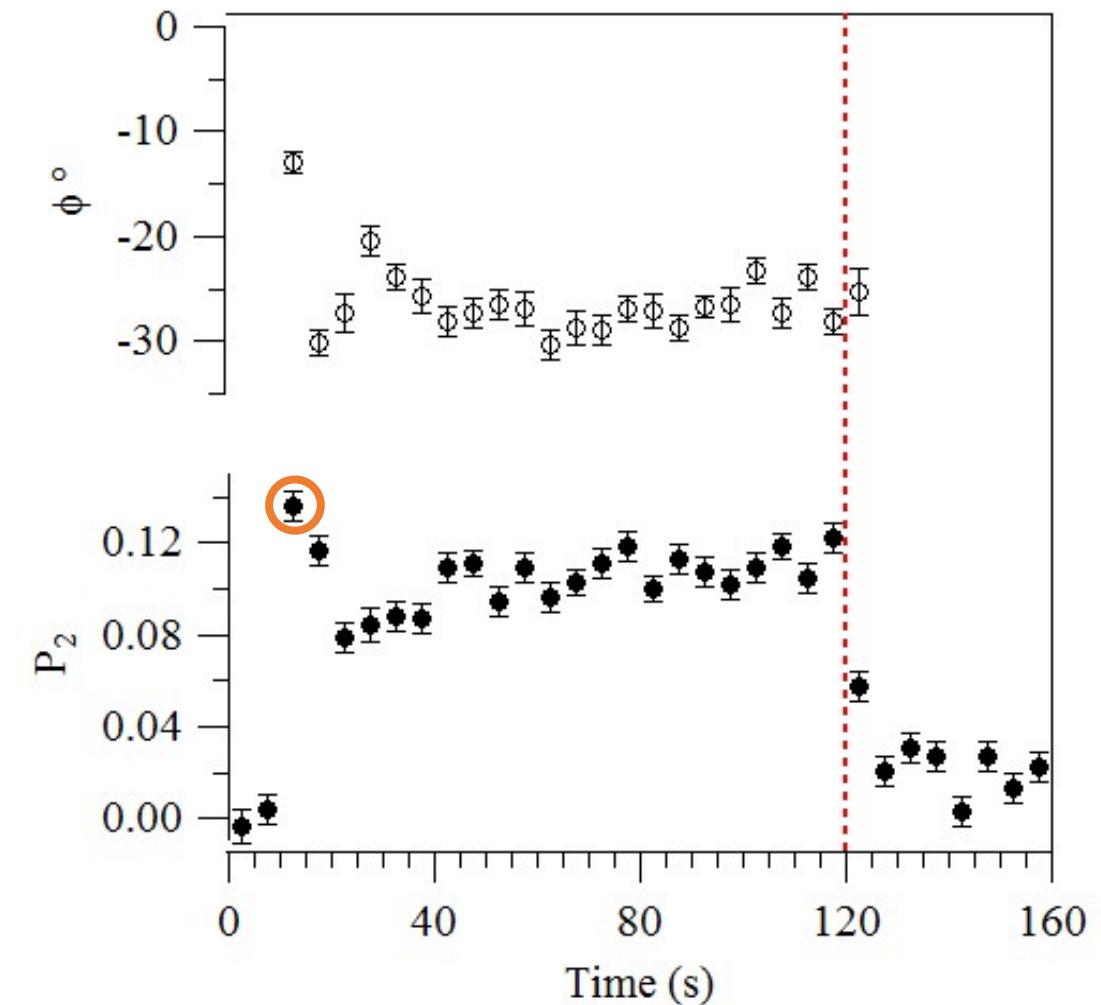
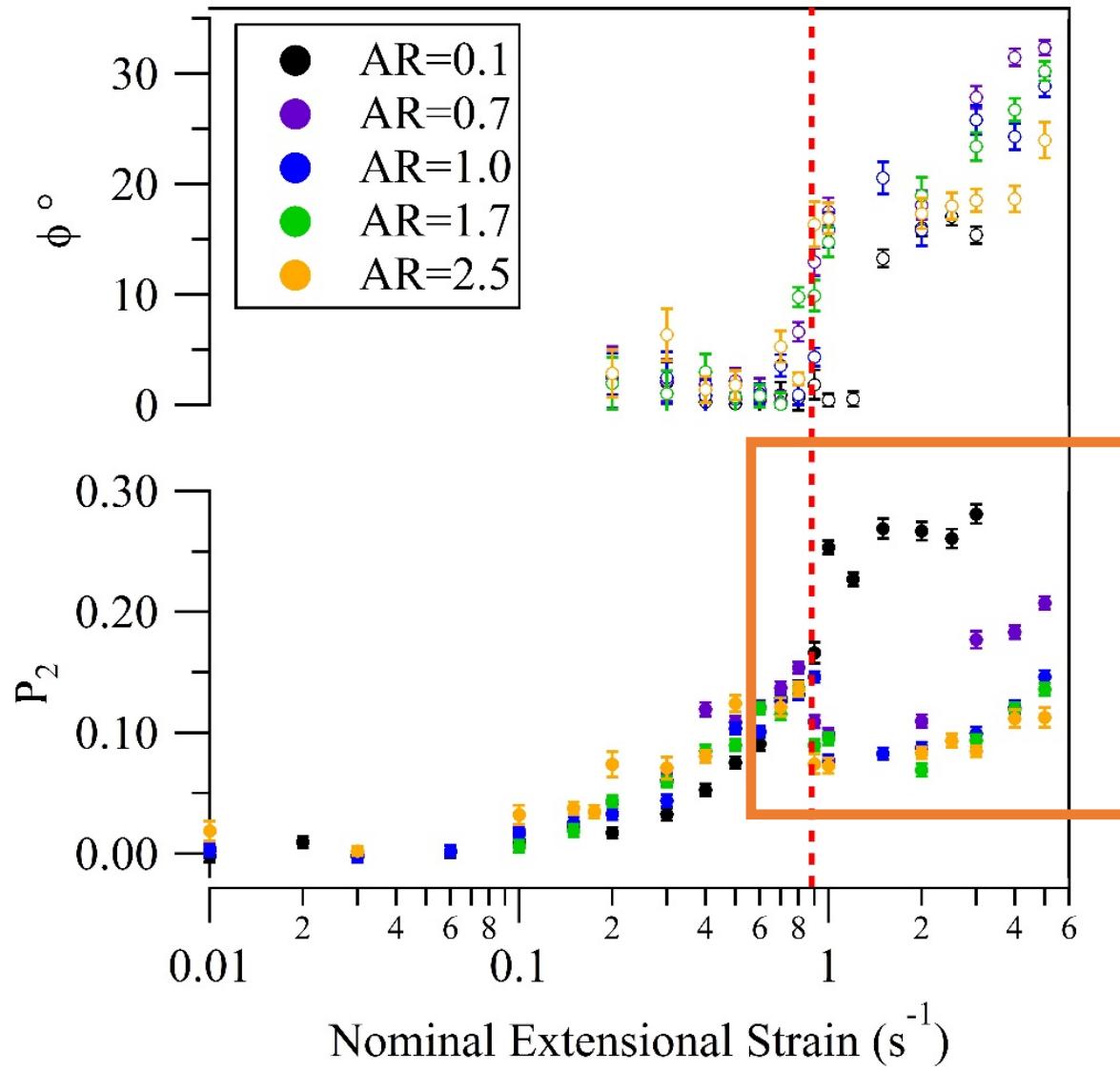


Conclusions

- $\bar{P}_2 \approx -A_f$
- Measured the amount of orientation and the angle of orientation as a function of nominal extensional strain rate
- Characterized the transition between symmetric and asymmetric flow
- Showed that the behavior of the higher aspect ratios is nearly identical



Future Work



Acknowledgements

- Katie Weigandt
- NSF
- NIST- NCNR
- Julie Borchers
- David Hoogerheide, Chirag Parikh, and Frank Hess

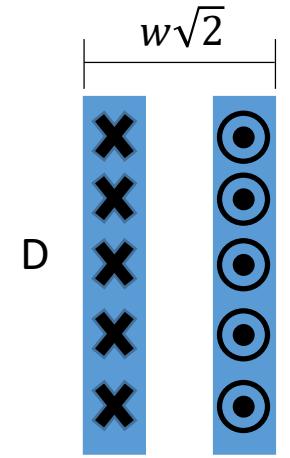
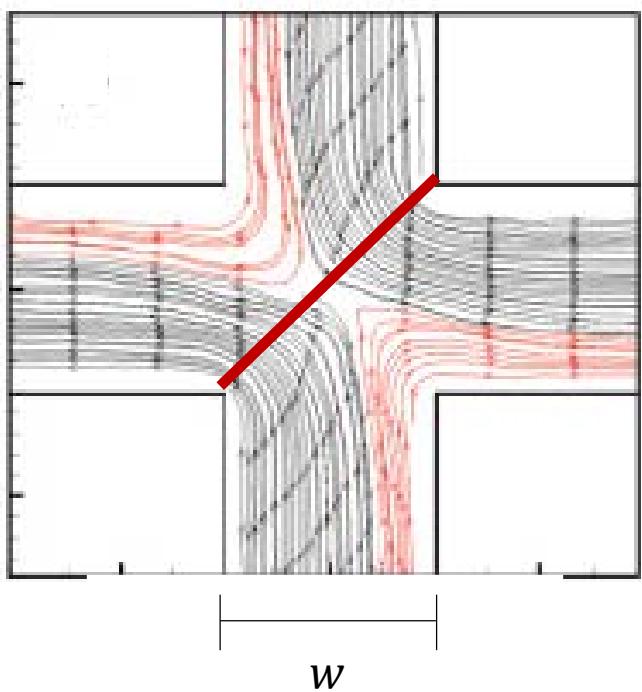


Questions?



Aspect Ratio

$$AR = \frac{D}{w}$$



$$\underline{AR = 2.5}$$

$$\nu = 8.5 \text{ cm/s} \\ (\dot{\epsilon}_{nom} = 1 \text{ s}^{-1})$$



$$\underline{AR = 1}$$

$$\nu = 12 \text{ cm/s} \\ (\dot{\epsilon}_{nom} = 1 \text{ s}^{-1})$$



$$\underline{AR = .1}$$

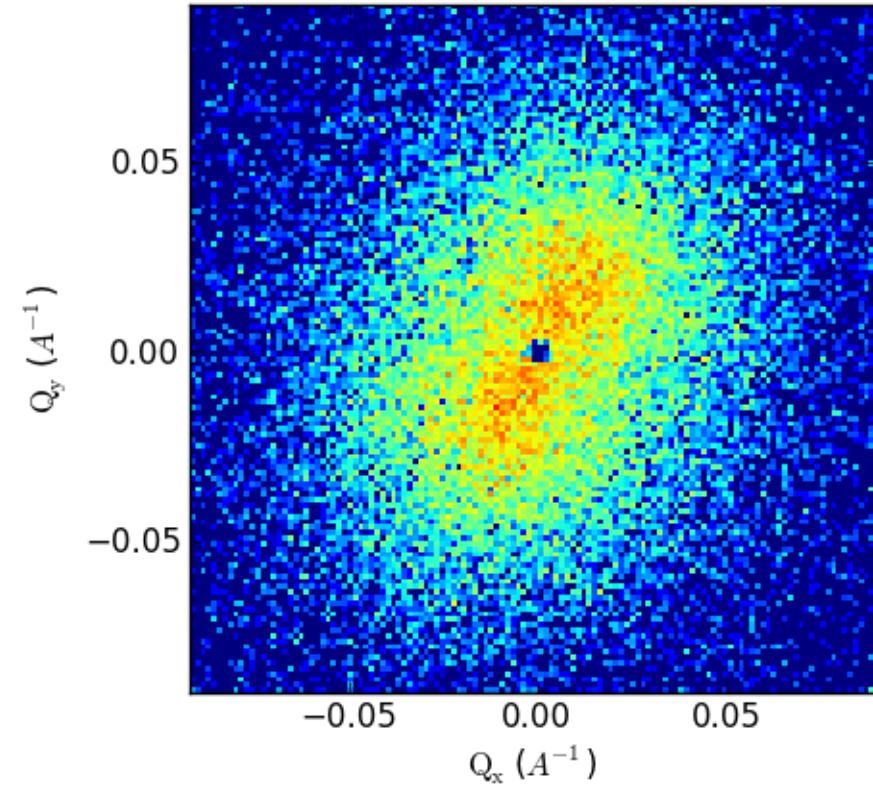
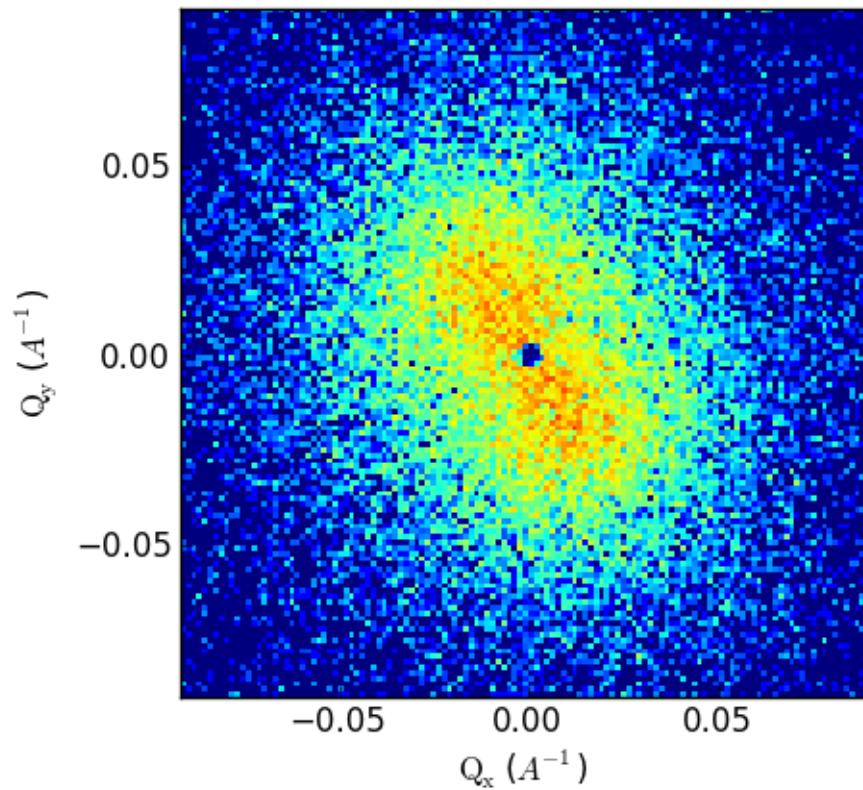
$$\nu = 42 \text{ cm/s} \\ (\dot{\epsilon}_{nom} = 1 \text{ s}^{-1})$$

Plug-like flow:

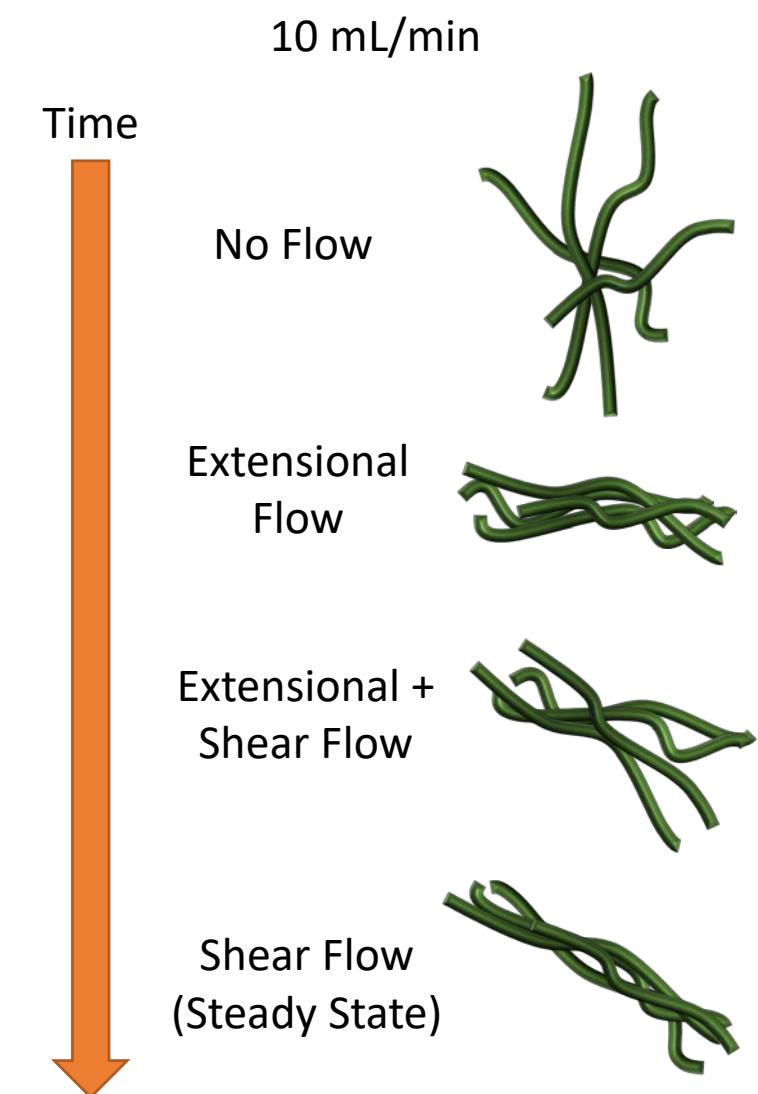
$$\dot{\epsilon}_{nom} = \frac{Q}{w^2 D} [1]$$

Preferential Asymmetry

$\dot{\epsilon} = 3s^{-1}$, AR = 0.7



Stress overshoot

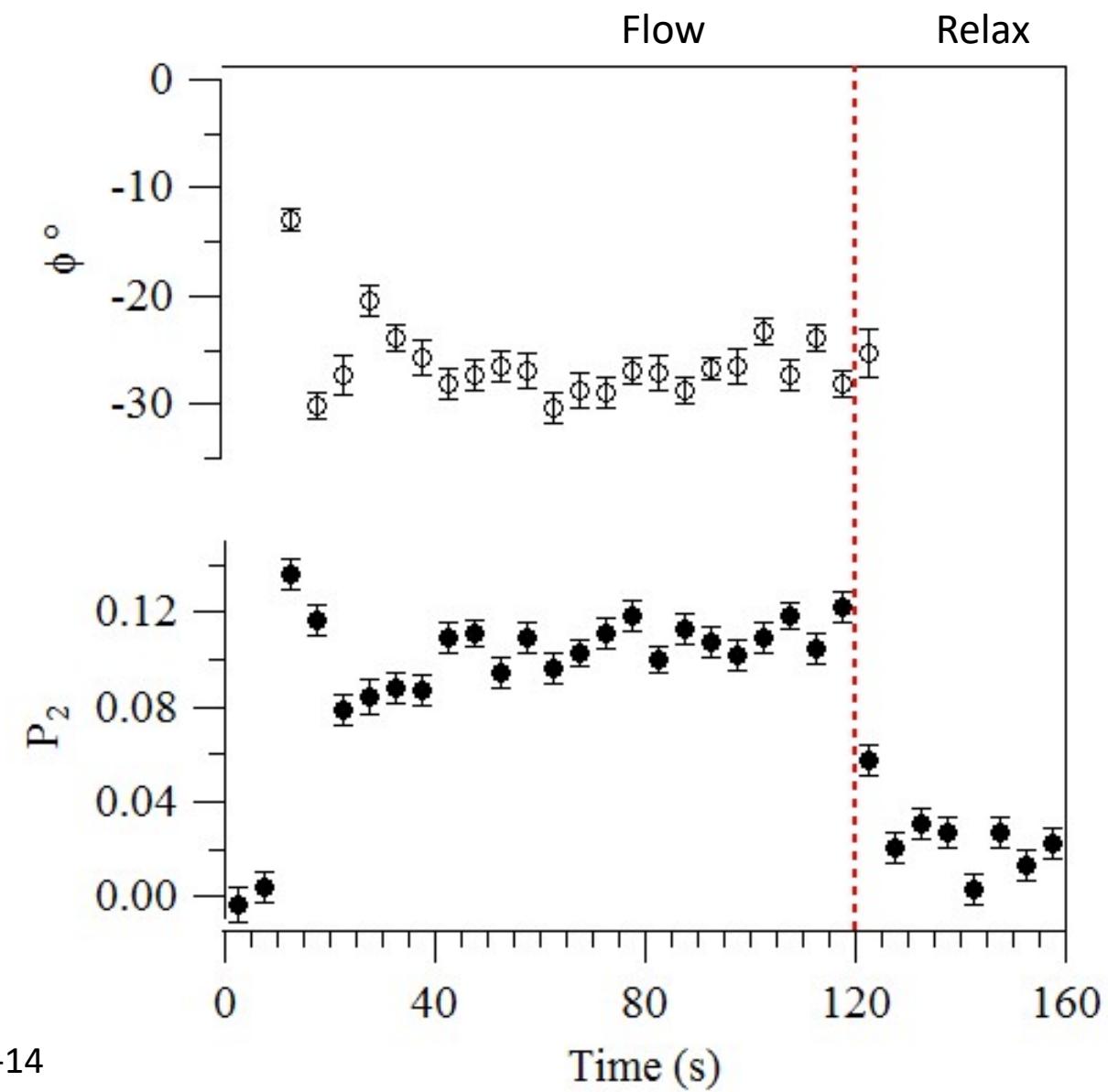
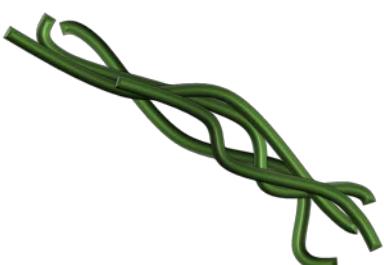
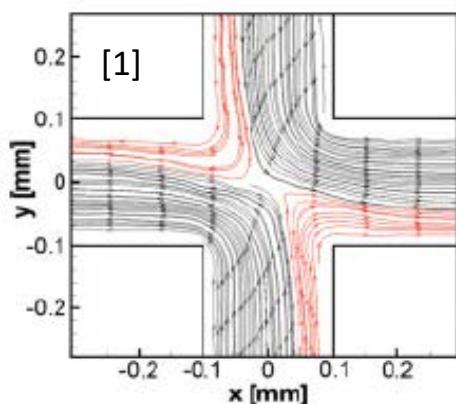


$\dot{\epsilon} = 8.3 \text{ s}^{-1}$ Time Resolved

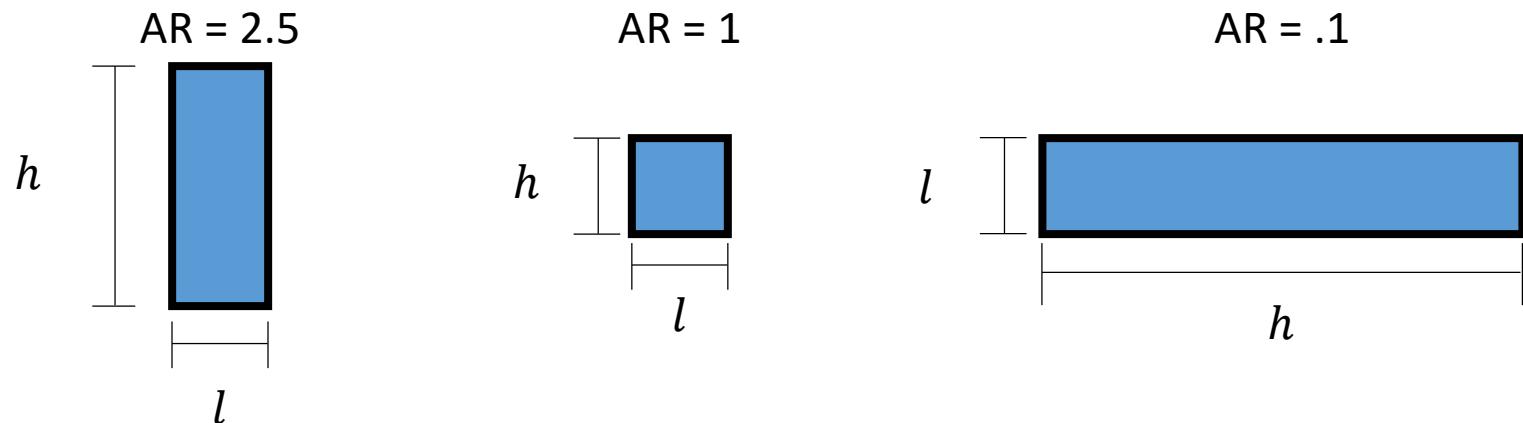
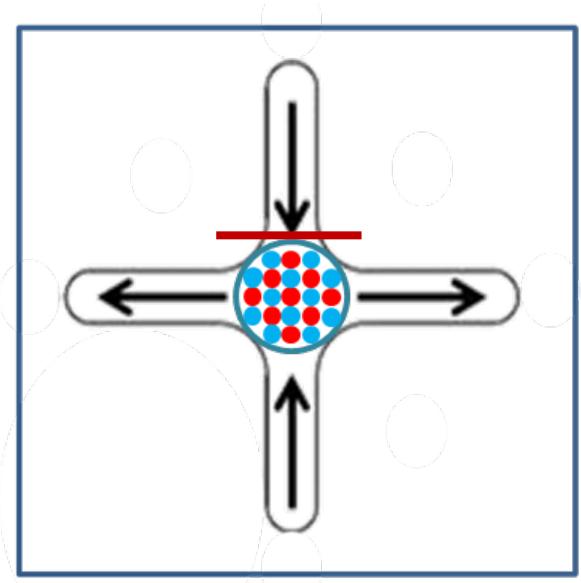
Steady state orientation is reached after
 $\sim 40\text{s}$

$$\bar{P}_2 = 0.10$$

$$\phi_0 = -28^\circ$$



Aspect Ratios and Shear



$$\dot{\gamma}_{wall} = \frac{6Q}{l^2 h}; l < h \text{ (Newtonian Fluid)}$$

$$\dot{\epsilon}_{nom} = \frac{Q}{w^2 D} = 1 \text{ s}^{-1} \rightarrow \dot{\gamma} = 6 \text{ s}^{-1} \quad \dot{\gamma} = 6 \text{ s}^{-1} \quad \dot{\gamma} = 36.8 \text{ s}^{-1}$$

Symmetric Flow

References

1. Haward, S.; McKinley, G. *Physical Review*. **2012**, 85, 031502-1-031502-14
2. W. H. DeJeu, *Mol. Cryst. Liq. Cryst.* **1997**, 292, 13.
3. L.M. Walker, "Rheology and Rheo-optics of liquid crystal polymers under flow." **1995**